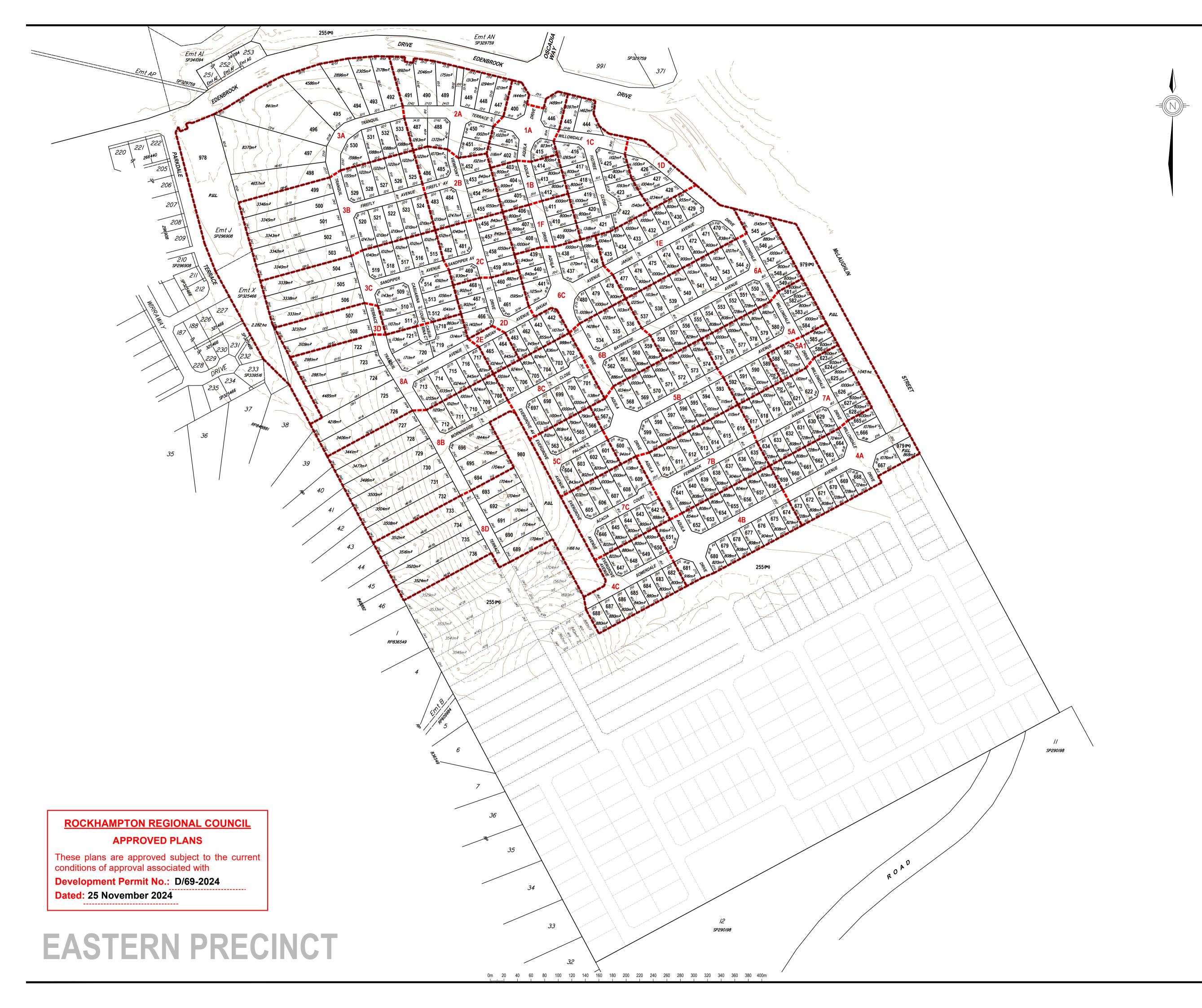


Document Set ID: 40933838 Version: 1, Version Date: 05/11/2024



## Staging

Stage Number	Lots
Stage 1	47
Stage 2	36
Stage 3	42
Stage 4	42
Stage 5	42
Stage 6	38
Stage 7	42
Stage 8	48
Total	337
	•

#### **IMPORTANT NOTE**

This plan was prepared to accompany an application to Rockhampton Regional Council and should not be used for any other purpose.

The dimensions and areas shown hereon are subject to field survey and also to the requirements of council and any other authority which may have requirements under any relevant legislation.

In particular, no reliance should be placed on the information on this plan for any financial dealings involving the land.

This note is an integral part of this plan.

clier

## Edenbrook Land Pty Ltd A.C.N. 112 588 182

proje

## Edenbrook Estate Edenbrook Drive, Parkhurst

plan

## **Concept Plan**

1 Lot into 47 Lots (Stage 1) + 290 Lots + Bal)

rpd

### Lot 255 on SP346283

Rockhampton Regional Council

issue	date	authorised	
Α	18-12-2023	Initial Issue	RJKF
В	29-01-2024	Layout amended, prelim staging added	RJKF
С	13-02-2024	Sub-staging added	RJKF
D	12-06-2024	Stgs 2, 3, 6, 8, Lots 450, 451, 480 amended	RJKF
Ε	25-06-2024	Plan scale changed, Sub-stage 5A1 added	RJKF

created



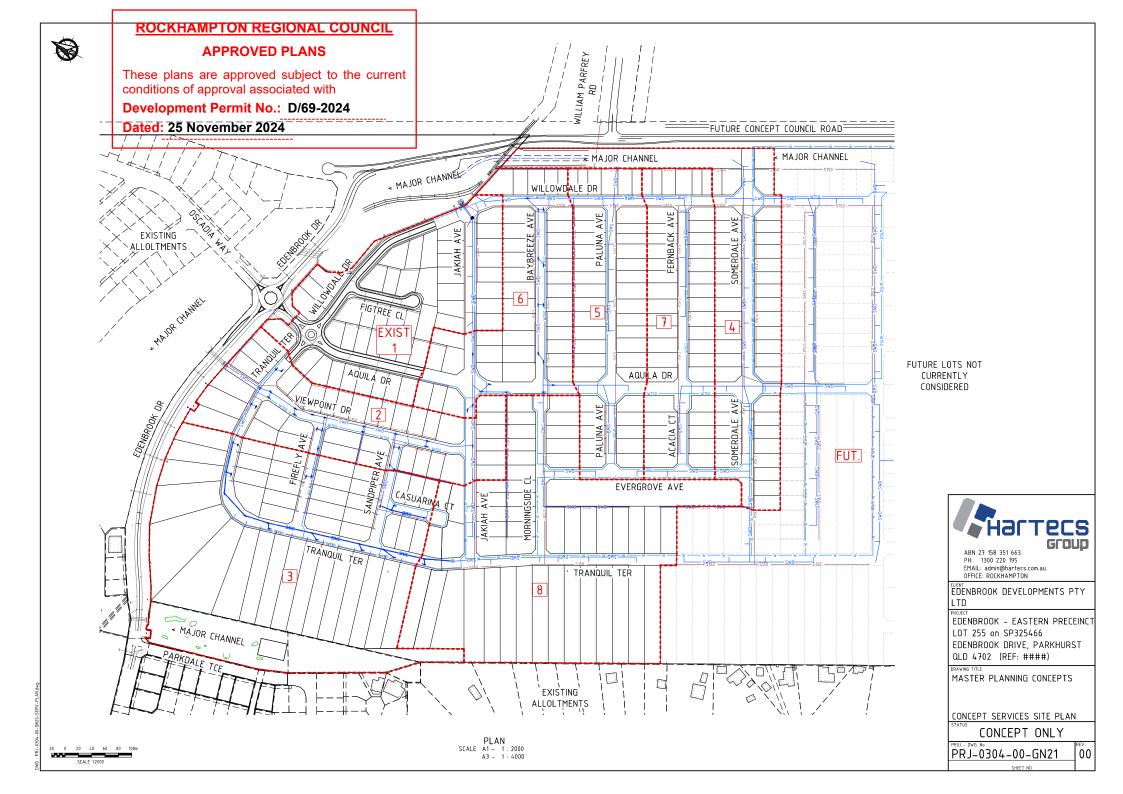
927 5199 | reception@csgcq.com.au | 132 Victoria Parade, Rockhampton QLD 4700

scale datum

1:2000 @ A1 AHD 2.5m Contours
sheet no. cad file

1 of 1 8066-EP-CPT E
plan no. issue

8066-EP-CPT E





## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/69-2024** 

Dated: 25 November 2024

Hartecs Group Pty Ltd ABN: 27 158 351 663

20/5/2022

Development Assessment Section Rockhampton Regional Council PO Box 1860, ROCKHAMPTON QLD 4700

Dear Sir/Madam

## **ROL APPLICATION – STAGE 4 OF 32 RESIDENTIAL LOTS EASTERN PRECINCT AT EDENBROOK DRIVE, PARKHURST**

This engineering report is prepared on behalf of Edenbrook Developments to assist Council with assessment of an ROL application. It refers to the Capricorn Survey Group's proposal plan for Stage 4 on Drawing No 8066-04-ROL Issue C in Appendix A of this report.

The following Hartecs drawings are referenced and included as Appendix B of this report:

- a) Cover Sheet Eastern Precinct Stages 1 6 with the drawing listing
- b) PRJ-0131-ROL1 Issue 3 Site Plan
- c) PRJ-0131-ROL2 Issue 3 Lot Layout & Staging
- d) PRJ-0131-ROL3 Issue 3 and PRJ-0131-ROL4 Issue 3 Finished Surface Profile Post Bulk Earthworks and Finished Surface Depths Post Bulk Earthworks
- e) PRJ-0131-ROL5 Issue 3 Typical Site Sections
- f) PRJ-0131-ROL6 Issue 3 Services Layout Stage 1
- g) PRJ-0131-ROL7 Issue 3 Services Layout Stage 2
- h) PRJ-0131-ROL8 Issue 3 Services Layout Stage 3
- i) PRJ-0131-ROL9 Issue 3 Services Layout Stage 4
- j) PRJ-0131-ROL10 Issue 3 Services Layout Stage 5
- k) PRJ-0131-ROL11 Issue 3 Services Layout Stage 6
- I) PRJ-0131-ROL12 Issue 3 Stormwater Management Flooding
- m) PRJ-0131-ROL13 Issue 3 Stormwater Management Water Quality

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#### 1.0 INTRODUCTION

- 1.1 This development application consists of Stages 4A and 4B in Edenbrook's Eastern Precinct for a total of 32 new residential allotments serviced from both the proposed new southern road connection onto Edenbrook Drive called Aquila Drive and from the new proposed Somerdale Avenue which will connect to McLaughlin Street.
  - A Site Plan is presented on Drawing No PRJ-0131-ROL1 Issue 3 in Appendix B. A Lot Layout & Staging Plan is presented on Drawing No PRJ-0131-ROL2 Issue 3 in Appendix B.
- 1.2 Aquila Drive is proposed to connect to the roundabout intersection of Oscadia Way and Edenbrook Drive which are currently under construction.
  Somerdale Avenue will be a new thoroughfare connection to McLaughlin Street.
- 1.3 The subject site will not be constrained by servicing; all services are available or can be made available and can be conditioned accordingly by Council.

#### 2.0 EARTHWORKS & SLOPE STABILITY

- 2.1 Portions of the subject site of this undeveloped area of the Edenbrook land are captured by the Steep Land Overlay mapping wherein intermittent slopes greater than 15% are identified.
- 2.2 Douglas Partners has prepared an assessment of the site's geotechnical stability in accordance with the Council's Steep Land Overlay Code with the clear understanding that the Applicant proposes major earthworks to generally create lower sloped lots over the site and eliminate as much as possible the need for high retaining walls (> 1m). It will also serve to keep road grades to generally less than 5%.
- 2.3 The proposed cut depths are significant, up to 7 metres in places; similar depths of cut were undertaken on the adjacent Stage 12. Hence the proposed earthworks are a feasible, practical operation that will have benefits for road grades, for drainage and for future allotment development.
- 2.4 The proposed Bulk Earthworks Finished Profile Slopes and Bulk Earthworks Finished Profile Depths are presented on Drawing No's PRJ-0131-ROL3 Issue 3 and ROL4 Issue 3 in Appendix B of this report. Similar plans are incorporated within the Douglas Partners stability assessment report.
- 2.5 In summary the Douglas Partners assessment found that:
  - There are no signs of instability present on this site.
  - Provided the site's development is carried out in accordance with good engineering practice for hillside construction then:
    - 1) The risk to property and to properties adjacent the site is considered to be "Low".
    - 2) And instability failure will be "Unlikely" and/or "Rare".

Council's standard approval conditions and the normal follow up Operational Works application review and its procedures will oversee and ensure compliance with these requirements.

2.6 These findings by Douglas Partners are consistent with similar investigations undertaken on earlier stages of the Edenbrook development site immediately to the west.

2.7 These earlier investigations found no instability and instability was unlikely; and that landslide risk was low. Similar recommendations for future development were also made. Council should be confident there are no issues in this regard for the Eastern Precinct.

#### 3.0 TRUNK INFRASTRUCTURE

- 3.1 The trunk infrastructure nominated for the Priority Infrastructure Area of Parkhurst
  - (or an equivalent RRC approved strategy) that affects immediate servicing of the subject proposal has been incorporated into the approval of the Oscadia development which lies immediately on the northern side of Edenbrook Drive from the subject site.
- 3.2 Council approved the Oscadia residential development with conditions to provide the necessary infrastructure in this locale in accordance with the Planning Scheme's schedule of works and Council policy in this regard. These works are designed, approved and currently under construction and include the extension to Edenbrook Drive and the Trunk Sewerage works to command the subject site. Trunk Water infrastructure has been previously provided by Edenbrook Developments including the VS Booster Pump Station that services Edenbrook and commands adjacent undeveloped residential land to the east.

### 3.3 McLaughlin Street – Trunk Transport Infrastructure & Drainage Structures

- 3.3.1 Council's preliminary interim design titled *ALEXANDRA STREET EXT. BELMONT DR TO EDENBROOK DR (PARKHURST) PROJECT NO 2020-229* includes the proposed construction of the McLaughlin Street link showing the following major culverts on Drawing No 2020-229-09; refer Appendix D for first 10 pages only with a diversion channel (in red) indicated schematically on page 10:
  - DRAIN LINE 4 3/1800x1200 RCBC on McLaughlin Street at Ch 1290 for Catchment A = 28.5 ha
  - DRAIN LINE 3 3/2400x1500 RCBC on William Palfry Road at Ch 75 to cater for Catchments A + B = 80 ha
  - DRAIN LINE 2 4/2400x 1550 RCBC on McLaughlin Street at Ch 1510 to cater for Catchments A+ B + C = 98.2 ha
- 3.3.2 This RRC design and these culverts recognize and are consistent with the flowpaths and flood extents on the Creek Catchment Flood Overlay Map OM-8C-41.
  - The proposed allotments have been kept clear of inundation areas and Public Use Land (PUL) provided where required. The majority of the inundation borders the Eastern Precinct and encroachment (if any) is minor and is mostly within the redundant road reserve of Edenbrook Drive that arose with the redesign of McLaughlin Street. It is these drainage paths that precipitated the re-routing of McLaughlin Street and immediate road connections adjacent.
- 3.3.3 In addition, Edenbrook Developments proposes an offer to Council to re-direct Catchment A i.e., the upstream watercourse within Edenbrook land, before it naturally runs into Drain Line 4 across McLaughlin Street; i.e., to provide a diversion channel entirely on the western side of McLaughlin Street within Edenbrook's Eastern Precinct.

- 3.4 This proposal would have major benefits to Council when completing the proposed Trunk Transport Infrastructure on McLaughlin Street and William Palfry Drive. The proposed redirected flow from an area of 28.5 hectares would eliminate Drain Line 4 from being a cross culvert on McLaughlin Street.
- 3.5 It would also significantly reduce the catchments to DRAIN LINE 3 by some 35% and to DRAIN LINE 2 by around 29% i.e., the 28.5 hectares of Catchment A would be prevented from connecting to Catchment B and then to Catchment C.
- 3.6 This offer is made on the basis that it is then fair and reasonable for the works required for the effective redirection of Catchment A's 28.5 hectares to be deemed Trunk Infrastructure under Council's policy.

These works would include:

- The equivalent hydraulic structure needed for Drain Line 4 relocated to the Edenbrook internal road leg connection immediately adjacent to McLaughlin Street to facilitate the redirected flowpath; plus
- b) The necessary diversion channel and stabilization works of the diversion channel that will run parallel to McLaughlin Street but essentially within Edenbrook.

### 3.7 McLaughlin Street – Trunk Transport Infrastructure & Road Construction

- 3.7.1 Until the McLaughlin Street link connection is constructed, day to day traffic access to and from the Edenbrook's Eastern Precinct will be via Edenbrook Drive and Belmont Road.
  - Assuming the worst case (i.e., full development of the Oscadia precinct plus every lot developed in Stages 1 to 14 of the Edenbrook development), there will be 297 residential lots, both developed with houses and un-developed, that are connected to Edenbrook Drive prior to the release of any lots in Edenbrook's Eastern Precinct.
- 3.7.2 The construction of the McLaughlin Street link (T97) plus its intersection with Birkbeck Drive-Alexandra Street-Belmont Drive (T96) is an enormous undertaking (costing in the order of \$11 million plus dollars) even if interim construction standards or alternative intersection controls reduce the financial impacts to the project funder.
- 3.7.3 To date Council has produced a preliminary design for these works and the estimated timing in the Planning Scheme's Schedule of Works is 2026. This timing is thus in advance and on track to cater for the next six proposed stages of Edenbrook's Eastern Precinct for a total of around 240 allotments.
- 3.7.4 Of the next six Eastern Precinct stages for a total of around 240 allotments, an optimistic projection is that 50 to 60 lots would be released over each of the next 4 years i.e., realistically through to mid to late 2027 allowing for the design, approval and construction processes.
  - Full traffic generation will not occur until several years after 2027 as these lots will only progressively develop with residential housing. Hence, the proposed 2026 timing for construction of the McLaughlin Street link will be in step with if not ahead of the release of lots in the Eastern Precinct .
- 3.7.5 The 600-metre section of Edenbrook Drive immediately connected to Belmont Road was constructed in 2014 and is the main constraining capacity link. It is constructed to a Minor Urban Collector standard with a 7.5m pavement but within a much wider 25m road reserve. The balance of Edenbrook Drive that is currently under construction to Major Urban Collector standard will have a 10m wide pavement within a 31m road reserve.

- 3.7.6 The Capricorn Municipal Development Guidelines nominates a Deemed-to-Comply capacity for traffic generation of 300 allotments for a Minor Urban Collector. This Deemed-to-Comply capacity is based on the *Queensland Streets* guidance for an "Environmental Capacity" of 3,000 vehicles per day for urban collectors. The actual traffic carrying ability will be several factors higher than this environmental capacity figure.
  - The significantly wider road reserve of 25 metres on the initial 600-metre section of Edenbrook Drive results in greater setback distances between houses which can then allow the road to accommodate higher traffic numbers for the same level of amenity.
- 3.7.7 Therefore, in the short term at the very least, a tolerance above 300 lots should be acceptable to Council given that the take up to 100% occupation of all lots in the Eastern Precinct catchment will not occur for some extended time well after 2026 even in the current climate and also given that the road reserve in this constrained section is significantly wider by nearly 40%.
- 3.7.8 It is recommended that the <u>short-term</u> capacity of the constrained section of Edenbrook Drive be tolerated and accepted as in the order of 500 lots i.e., somewhere above a Minor Urban Collector and less than a Major Urban Collector's environmental capacity. Then, the sequential release of an additional 240 lots plus the existing 297 (a total of around 537 allotments) can be allowed in the short term as within the capacity of the constrained section of Edenbrook Drive on the basis that timing for construction of the alternative route is controlled by Council.

#### 3.8 Trunk Sewer

Currently a 300 dia Trunk Sewer is designed, approved and constructed across Edenbrook Drive to the Eastern Precinct to service the subject development and future stages.

This sewer line will command a majority of the future 500 to 600 allotments of Edenbrook's Eastern Precinct. Based on an area assessment alone, this sewer would also command a not dissimilar number of lots on the eastern side of McLaughlin Street (ie approximately 1,000 lots all up); i.e., just by a simple review of RRC Drawing 2020-229-09 Issue A in Appendix D, the 300 dia trunk sewer would command an area at least similar to the drainage Catchments A, B, C & D.

In other words, the Trunk Sewer could be extended up McLaughlin Street in order to command in the order of 1,000 allotments in the future. The 300 dia sewer is shown extended indicatively to approximately the location of Drain Line 4

#### 4.0 INTERNAL ROADS

4.1 Access to the proposed subject development is via the extension of Edenbrook Drive and McLaughlin Street of which the latter is proposed to be constructed by Rockhampton Regional Council.

The extension of Edenbrook Drive is deemed a Major Collector Road and is designated Transport Trunk Infrastructure. McLaughlin Street is a Sub-Arterial Road and is also designated Transport Trunk Infrastructure.

4.2 The Eastern Precinct, which encompasses the entire balance area of the Edenbrook Estate, is estimated to ultimately yield in the order of 500 to 600 allotments.

Initially the main connection to the subject development will be via the "Oscadia" roundabout on Edenbrook Drive with the connecting proposed Minor Urban Collector of Aguila Drive.

In the short to medium term, until Somerdale Avenue can physically connect to McLaughlin Street, Aquila Drive will cater for around 240 allotments which is within its nominated capacity as a Minor Urban Collector.

As development proceeds and McLaughlin Street is constructed past the site, Somerdale Avenue (and much later a third connection) can join to McLaughlin Street. This will keep traffic numbers on Aquila Drive to well within the traffic loading parameters of a Minor Urban Collector (preferred maximum 300 lots). These future connections are shown on Drawing No PRJ-0131-ROL1 Issue 2 - Site Plan in Appendix B.

- 4.3 The internal roads for Stage 4 of this new development include:
  - Somerdale Avenue; catchment between 70 and 80 lots; an Access Street.
  - Willowdale Drive; catchment between 60 and 70 lots; an Access Street.
  - Aquila Drive; catchment less than 300 lots; a Minor Collector.
- 4.4 The indicative services & road layout Drawing No's PRJ-0131-ROL6 to ROL11 inclusive in Appendix B show all proposed pavement and road reserve widths compliant with or exceeding the Capricorn Municipal Development Guidelines preferences.

These nominated pavement widths and reserve widths including pathway location/routes may be adjusted at final design within the Operational Works application, but all will be compliant with the Capricorn Municipal Development Guidelines.

#### **5.0 DRAINAGE**

5.1 An indicative drainage network and strategy is shown on Drawing No's PRJ-0131-ROL6 to ROL12 inclusive in Appendix B.

All necessary drainage works both piped, road flows and channel flows will be designed and constructed in accordance with Operational Works Permit approved plans, Council's current policies and practices, the Capricorn Municipal Development Guidelines and the Queensland Urban Drainage Manual as relevant.

- 5.2 The proposed lots will be also covered by a Site Based Stormwater Management Plan to meet drainage and runoff quality requirements.
- 5.3 The subject development will address State Planning Policy in a not dissimilar manner to
  - Edenbrook Stage 8;
  - Edenbrook Stage 10; and
  - Oscadia Pocket.

5.4 An indicative proposed water quality management strategy is shown on Drawing No PRJ-0131-ROL13 included in Appendix B.

The detailed final design water quality treatment train submission is not provided with this application for the following reasons:

- a) The final strategy/solutions are determined and finalised in conjunction with discussions with Council and may well be developed on a stage-bystage basis or several stages together depending on Council preferences.
- b) There is an abundance of opportunities to provide treatments downstream and adjacent to the development and therefore there are many permutations of the final design to be determined with Council input.
- c) Regardless of any treatment train presentation and outcomes provided at this time, Council will impose its standard conditions requiring State Planning Policy being addressed and signed off at Operational Works.

The Developer has a record of and demonstrated a willingness to address the water quality in consultation with Council. The Developer has provided high quality works in this regard. Council cannot doubt the Developer's diligence and application in this respect. Council's standard conditions are sufficient to address this matter.

5.5 The increase in runoff from the additional impermeable area from within this development is insignificant in the context of the Ramsey Creek catchment and its proximity to the Fitzroy River flood plain. It will have no impact downstream and will not cause any actionable nuisance.

All stormwater can drain to a legal point of discharge as defined by the Queensland Urban Drainage Manual with the placement of easements/reserves in favour of Council as necessary.

#### 5.6 **Q100 FLOODING**

The peripheral edge of the Eastern Precinct is marginally impacted by the Creek Catchment Flood Overlay Map OM-8C-41. The proximity of inundation extents has been recognized and addressed in the proposed layout.

The flood flows and inundation extents have also been addressed during the approved design of the Edenbrook Drive extension and recognized in the Council's preliminary design of McLaughlin Street with Drain Lines 1, 2, 3 & 4.

A 1% AEP flood analysis has been previously submitted for the Edenbrook Estate and approved for the receiving waters of Ramsey Creek and the Fitzroy River. This provided a similar 1% AEP flooding line as the AURECON study on the Local Creek Catchments and AECOM's flooding line for the Fitzroy River.

5.7 The resulting 1% AEP inundation line with the recommended diversion channel is shown on attached Hartecs Drawing No PRJ-0131-ROL12 included in Appendix B. Inundation is clear of the proposed allotments.

#### **6.0 WATER SUPPLY INFRASTRUCTURE**

- 6.1 An indicative water reticulation layout is shown on attached Drawing No's PRJ-0131-ROL 6 to ROL12 inclusive in Appendix B.
- 6.2 A watermain network in 150mm diameter mains is proposed to connect off the existing Edenbrook Drive watermain, follow along Aquila Drive in 150 dia plus 150 dia mains are shown on the outer roads of the Eastern Precinct with a reconnection to the McLaughlin Street main. The numerous internal crosslinks of the network are all 100mm dia mains and ensure efficiency of the network.

- 6.3 The existing Edenbrook Drive 150mm watermain is connected to the VSD Pump Station system at the reservoir providing a minimum design pressure level equivalent to around RL 85 m AHD.
- 6.4 Given the proposed interconnected network and the subject site's final ground levels after earthworks will be less than RL 45m or 50m AHD, no further analysis is required.

#### 7.0 SEWERAGE INFRASTRUCTURE

- 7.1 Indicative proposed sewer servicing layouts are provided on the Drawing No's PRJ-0131-ROL 6 to ROL12 inclusive in Appendix B.
- 7.2 This is based in part on a suggested extension of the 300mm trunk sewer and cross connections to the eastern side of McLaughlin Street if Council so requires. If Council determines that extending the 300 dia sewer is not warranted, replacement with a 225 or a 150mm dia main is a simple matter.

#### 8.0 TELEPHONE AND ELECTRICITY

- 8.1 Ergon has confirmed that the existing supply has sufficient capability to service the proposed development.
- 8.2 Existing overhead power lines traverse the Eastern Precinct site and will need to be relocated and may impact the staging strategy.
  - This issue needs extensive design works negotiations with the electricity provider over the changeover strategy once an approval is received.
  - It will be resolved prior to Operational Works applications and Council's standard approval conditions are sufficient to address this aspect.
- 8.3 The NBN has accepted the whole development into its network.

#### 9.0 STATE PLANNING POLICY

#### 9.1 Acid Sulphate Soils

The proposed development site is located between RL 15m and RL 60m AHD. Excavation below RL 5 AHD is not required to install services or for construction. Hence acid sulphate soils are not an issue.

#### 9.2 Slope Stability

A slope stability investigation has been undertaken; no instability is present. The report is appended in Appendix C. The recommendations of the report are standard industry practice and will be incorporated into any future Operational Works on the site.

#### 9.3 Bushfire Management

The development site will be serviced with fully constructed sealed roads and an extensive reticulated water supply providing fire-fighting abilities to the statutory regulatory requirements. Therefore, evacuation will be able to be undertaken safely and adequate and accessible water supplies will be available.

#### 9.4 Flood

The site and access to the site will be above the AECOM/AURECON determined 1% AEP flooding level and clear of the inundation area as depicted on the Flood Overlay mapping. Therefore, there are no adverse impacts on people's safety.

#### 10.0 SUMMARY

- 10.1 The engineering submission herewith demonstrates that for Edenbrook's Eastern Precinct:
  - a) There are no engineering impediments to the proposed development and/or the subject stage as presented on the proposal plan.
    - Council's standard ROL development approval conditions modified to be relevant are sufficient to address the engineering aspects of the proposal.
  - b) The Steep Land Overlay code has been addressed. Instability is not present on the site. The subject site can be safely developed with good engineering practice for hillside construction. Council's standard approval conditions and procedures will oversee and ensure compliance with the requirements of the Douglas Partners recommendations.
  - c) The 1% AEP inundation area as depicted on the Flood Overlay mapping has been catered for on the subject proposal plan and a drainage strategy provided.
  - d) The first 600-metre section of Edenbrook Drive connected to Belmont Road has an increased reserve width which allows in the short term an increase in its nominal environmental capacity of 3,000 vehicle per day to be tolerated until the McLaughlin Street link scheduled for 2026 is completed.
  - e) Future detailed Operational Works Submissions are sufficient to address the details of the site works proposed, an acceptable water quality treatment train, road construction, water and sewer connections and drainage provisions for the proposed new allotments.
  - f) In the event Council accepts the Applicant's offer regarding DRAIN LINE 4 culvert and an integrated internal drainage channel, it would be reasonable for Council to adopt changes to its Trunk Infrastructure to address the changes to drainage infrastructure on McLaughlin Street.
  - g) It would be prudent for Council to investigate and review the need to extend the 300 dia Trunk Sewer further south along McLaughlin Street in order to command as much developable land as is possible as presented in this report.

Yours faithfully

**Hartecs Group** 

**Attachments** 

**Appendix A** Capricorn Survey's proposal plan Drawing No 8066-04-ROL

Issue C

**Appendix B** Engineering Report Drawings

Appendix C Douglas Partners Geotechnical Stability Assessment

**Appendix D** RRC Preliminary Design Drawings for McLaughlin Street

# **Appendix A**Reconfiguration Proposal Plan



# **Appendix B**Engineering Report Drawings

CSG

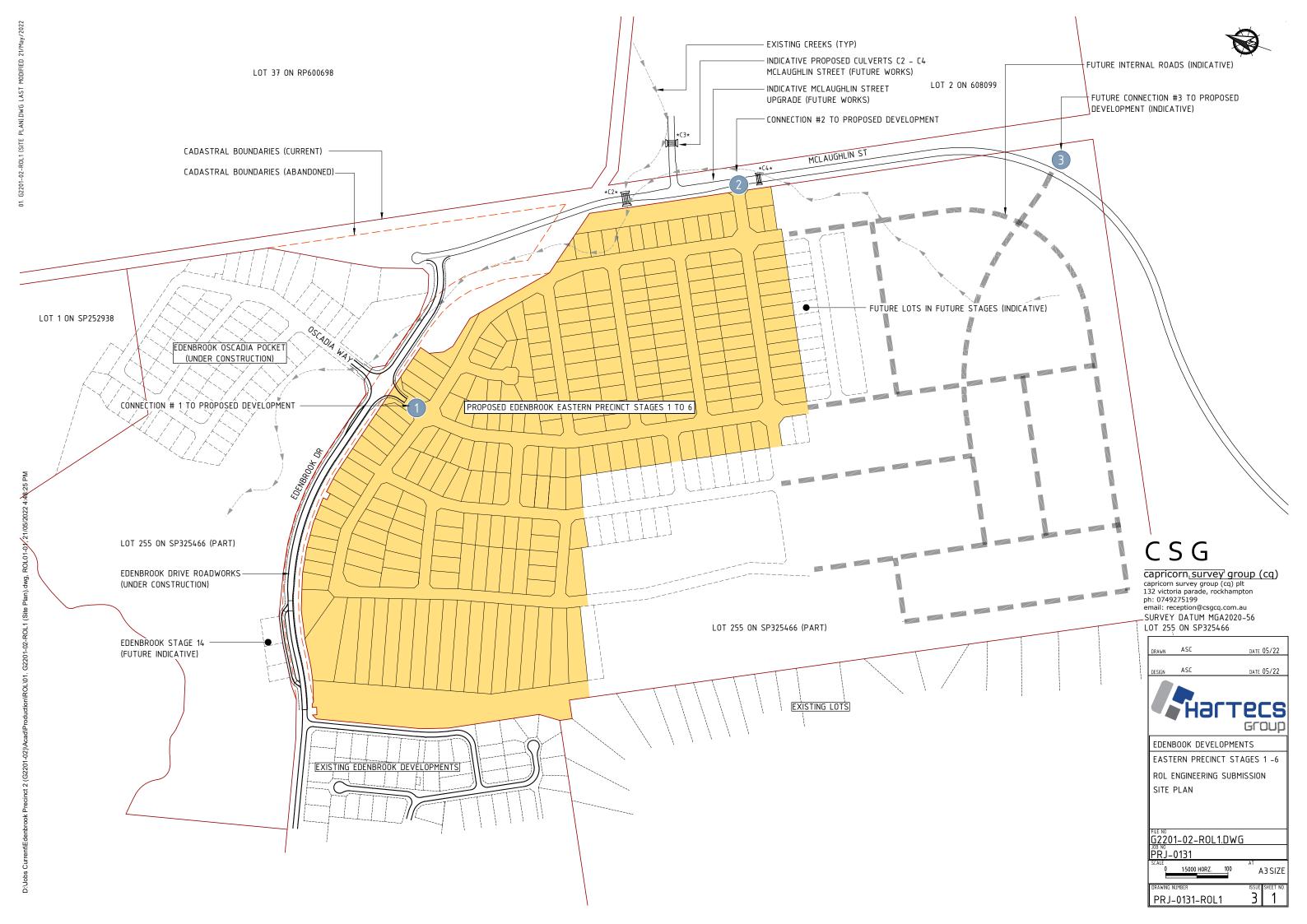
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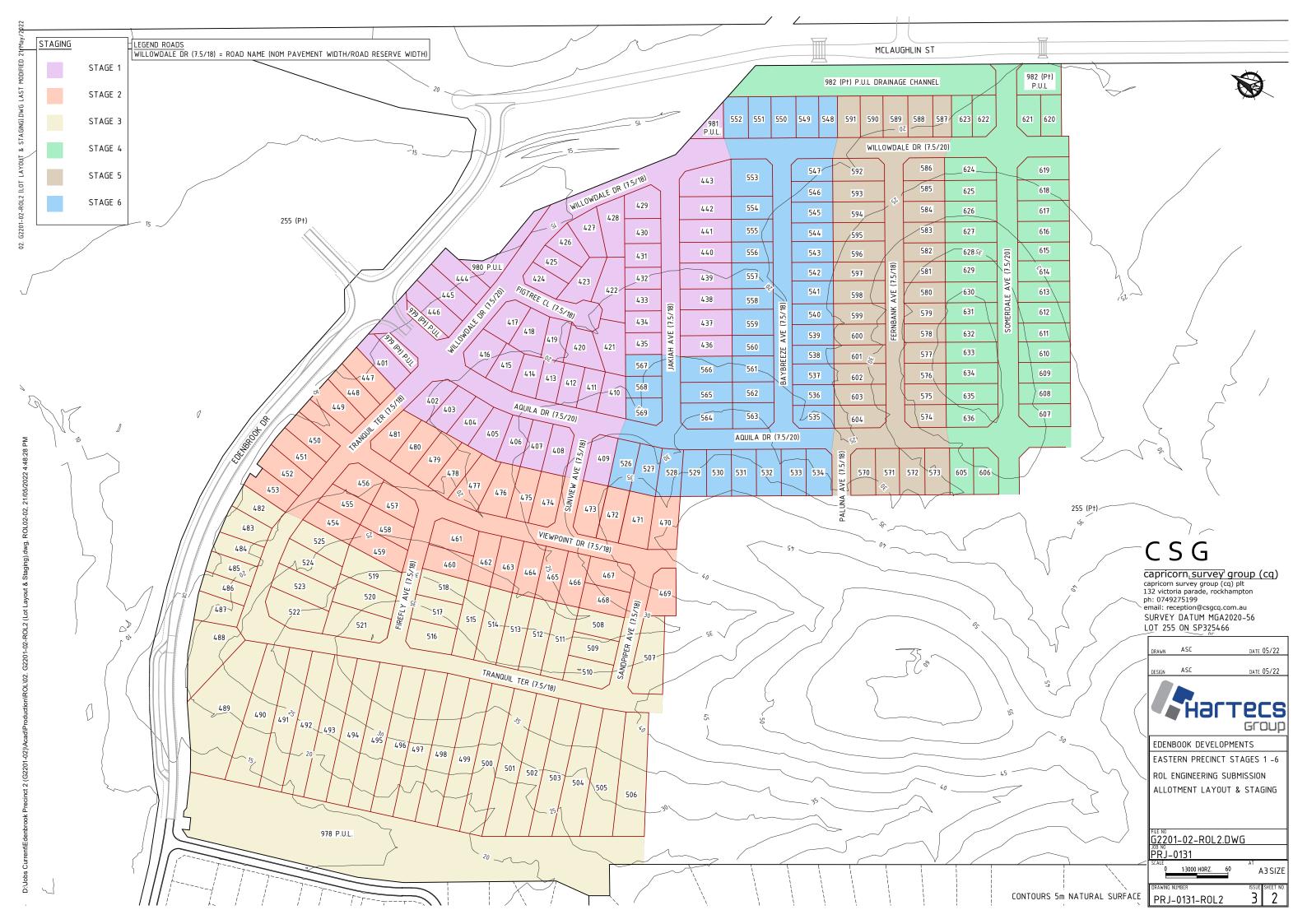


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ROL SUBMISSION 20/05/		SHEET	DWG NO.	REV	DESCRIPTION
ROL SL	SW	1	PRJ-0131-R0L1	3	SITE PLAN
EV 3	1 11	2	PRJ-0131-R0L2	3	LOT LAYOUT AND STAGING
0/05/2022 R	17,000	3	PRJ-0131-R0L3	3	FINISHED SURFACE PROFILE POST BULK EARTHWORKS
ROL SUBMISSION 20/05/	- N	4	PRJ-0131-R0L4	3	FINISHED SURFACE DEPTHS POST BULK EARTHWORKS
ROL SUE		5	PRJ-0131-R0L5	3	TYPICAL SITE SECTIONS
3		6	PRJ-0131-R0L6	3	INDICATIVE SERVICES & ROAD LAYOUT LAYOUT STAGE
//2022 REV		7	PRJ-0131-R0L7	3	INDICATIVE SERVICES & ROAD LAYOUT STAGE 2
ROL SUBMISSION 20/05/2022 REV		8	PRJ-0131-R0L8	3	INDICATIVE SERVICES & ROAD LAYOUT STAGE 3
OL SUBMIS		9	PRJ-0131-R0L9	3	INDICATIVE SERVICES & ROAD LAYOUT STAGE 4
<b>~</b>		10	PRJ-0131-R0L10	3	INDICATIVE SERVICES & ROAD LAYOUT STAGE 5
322 REV 3		11	PRJ-0131-R0L11	3	INDICATIVE SERVICES & ROAD LAYOUT STAGE 6
ION 20/05/2022 REV 3	SKA A	12	PRJ-0131-R0L12	3	STORM WATER MANAGEMENT Q100 FLOOD INUNDATION AREA

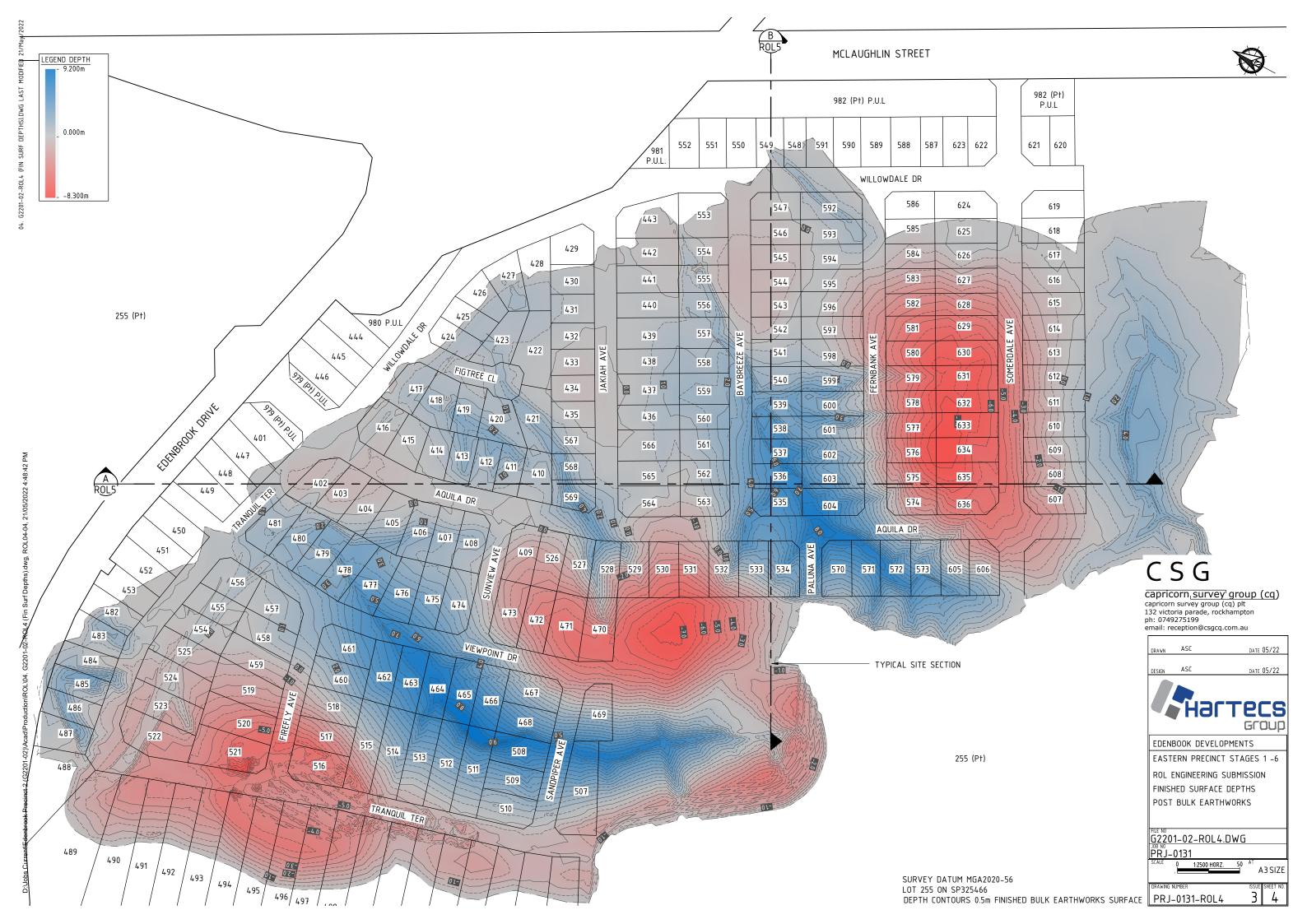
PRJ-0131-ROL13 3 STORM WATER MANAGEMENT WATER QUALITY







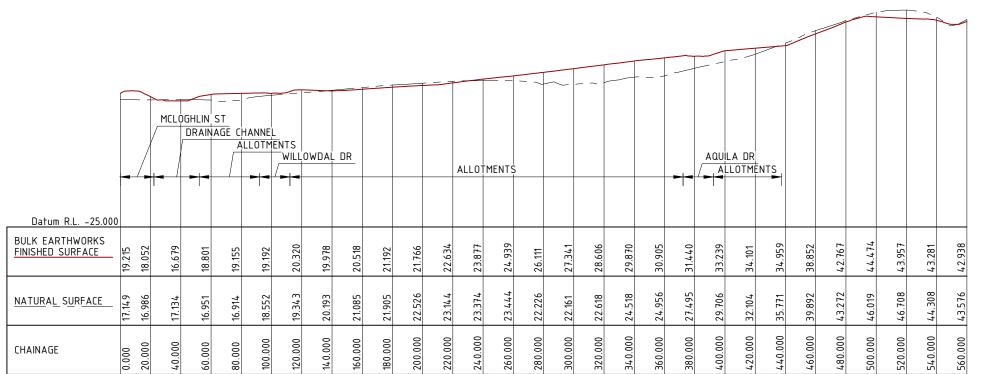




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NATURAL SURFACE	13.757	.58	16.02 <i>7</i> 16.13 <i>7</i>	79	19.940	22.367	23.270	24.484	24.439	24.898	25.861	6.2	23.918	7	70	28.997	28.044	26.339		0.05	28.286	31.693	-	63	40.625	40.542	39.113	35.304	33.102	31.287	29.686	26.995	28.625
CHAINAGE	20.000		100.000	0.00	160.000	200.000	220.000	260.000	280.000	300.000	320.000	40.00	360.000	4 00.000	0.00	7,000.097	4 80.000	500.000	0.0	560.000	580.000	600.000	0.0		680.000	700.000	720.000	740.000	760.000	780.000	800.000	820.000	840.000

Scale Horizontal 1:2500 Vertical 1:1250 SITE SECTION A



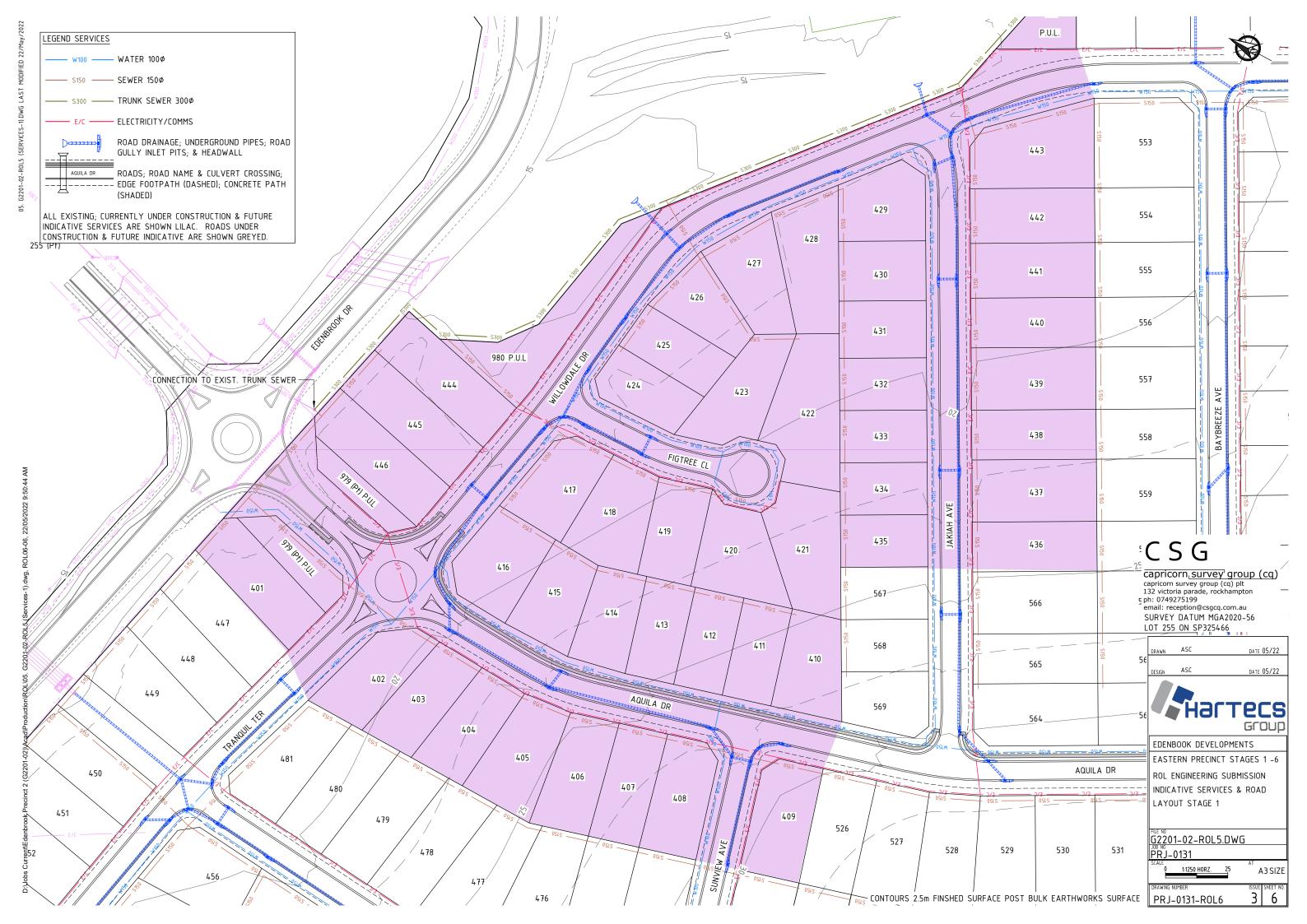
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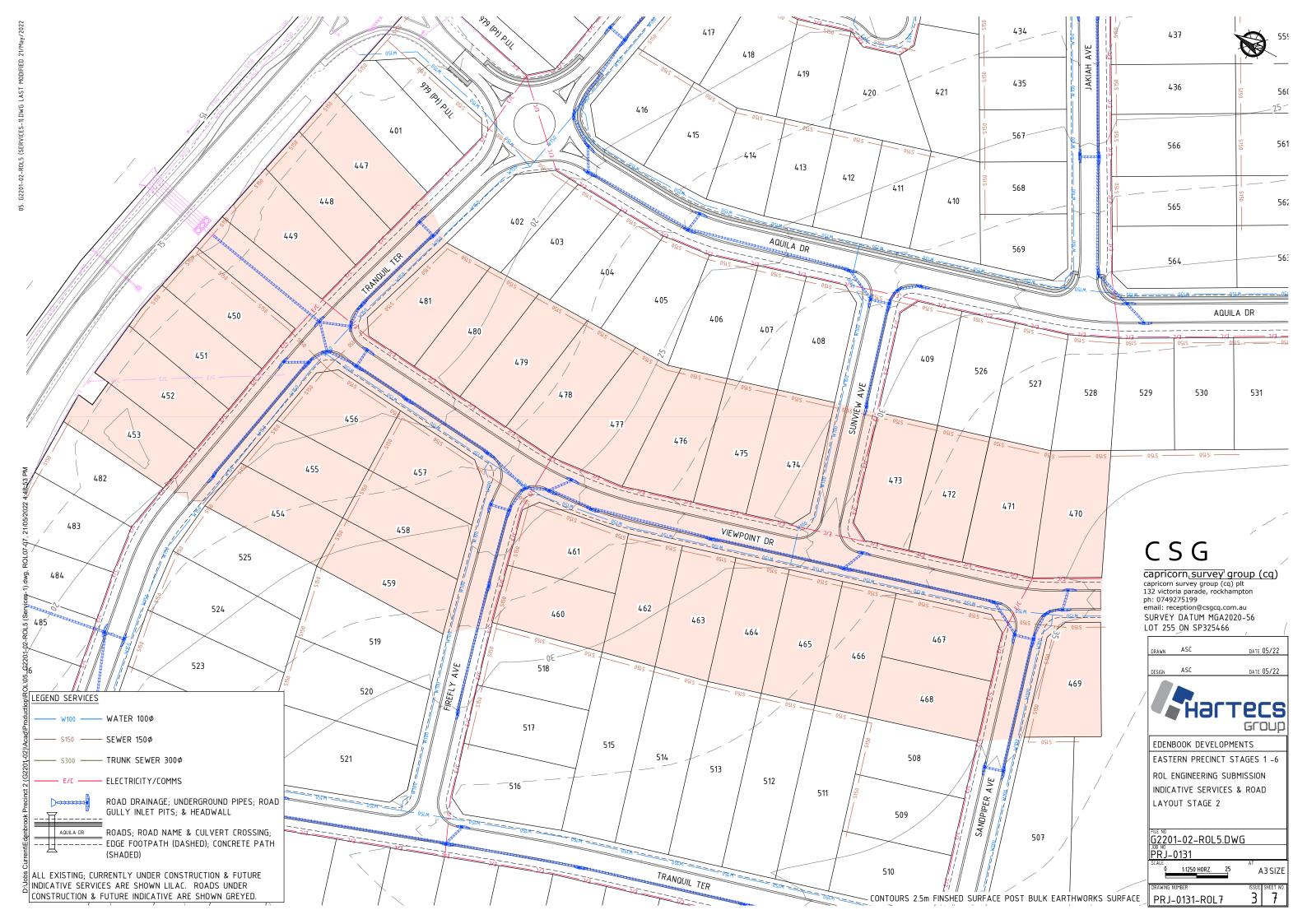


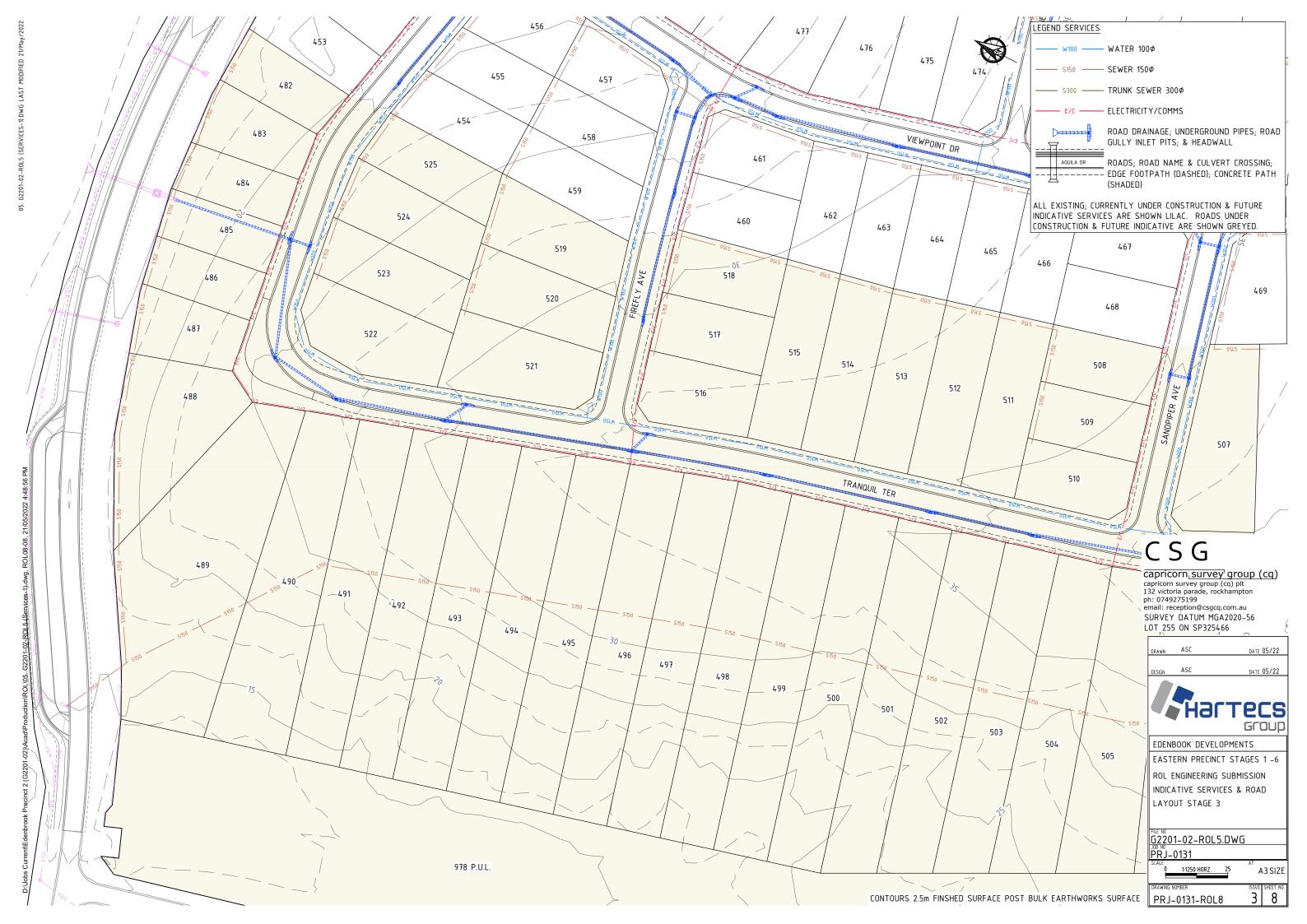
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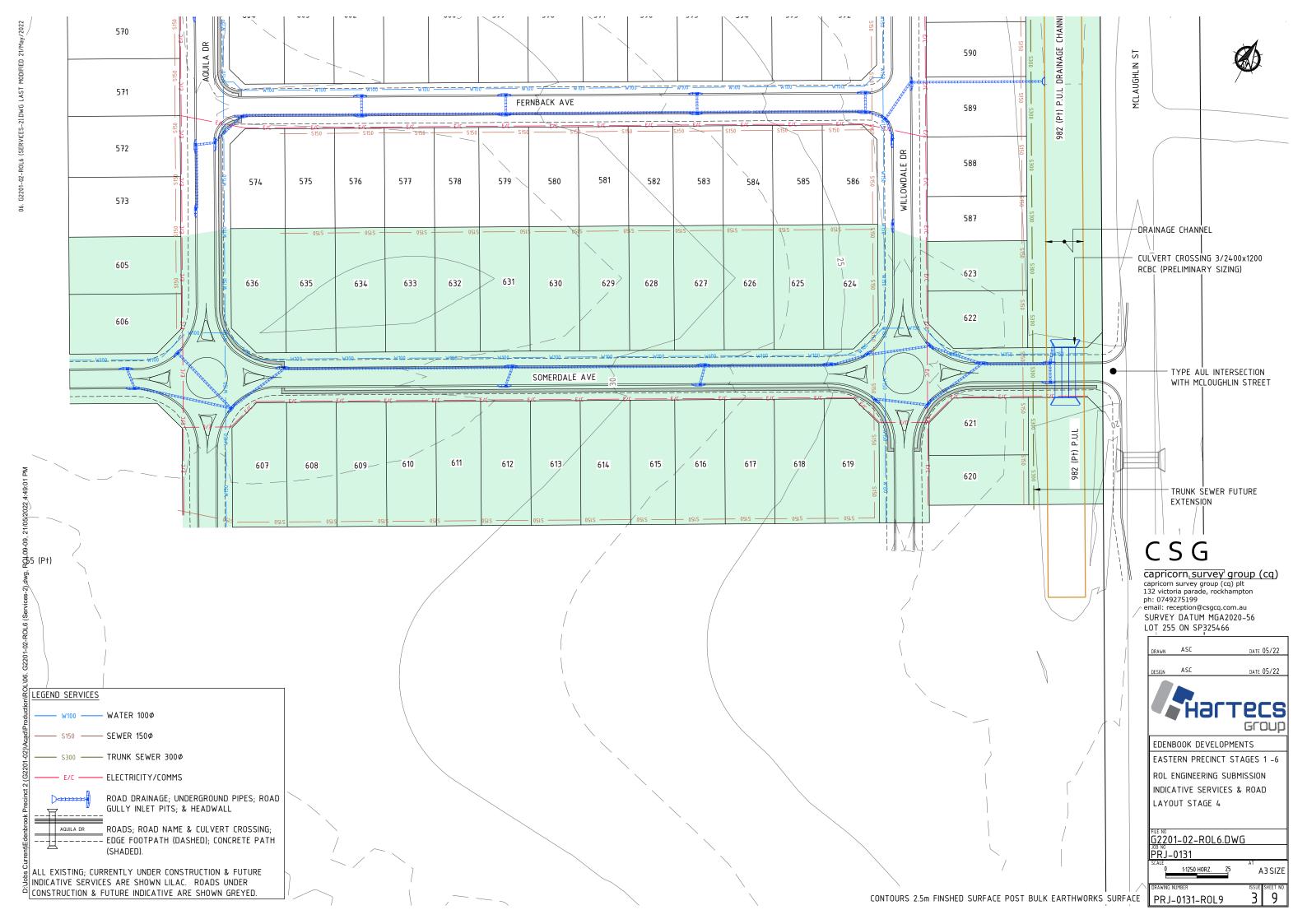
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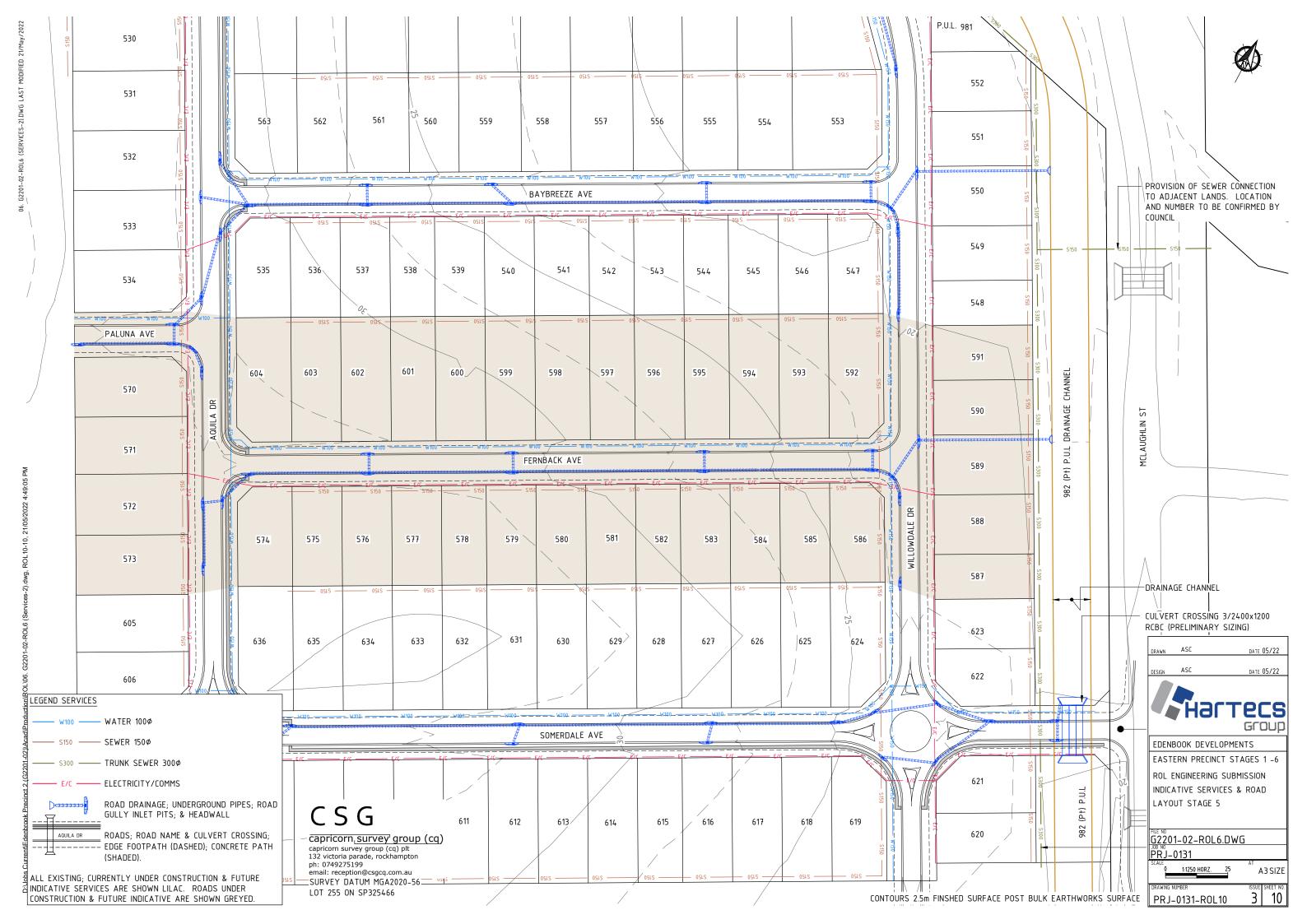
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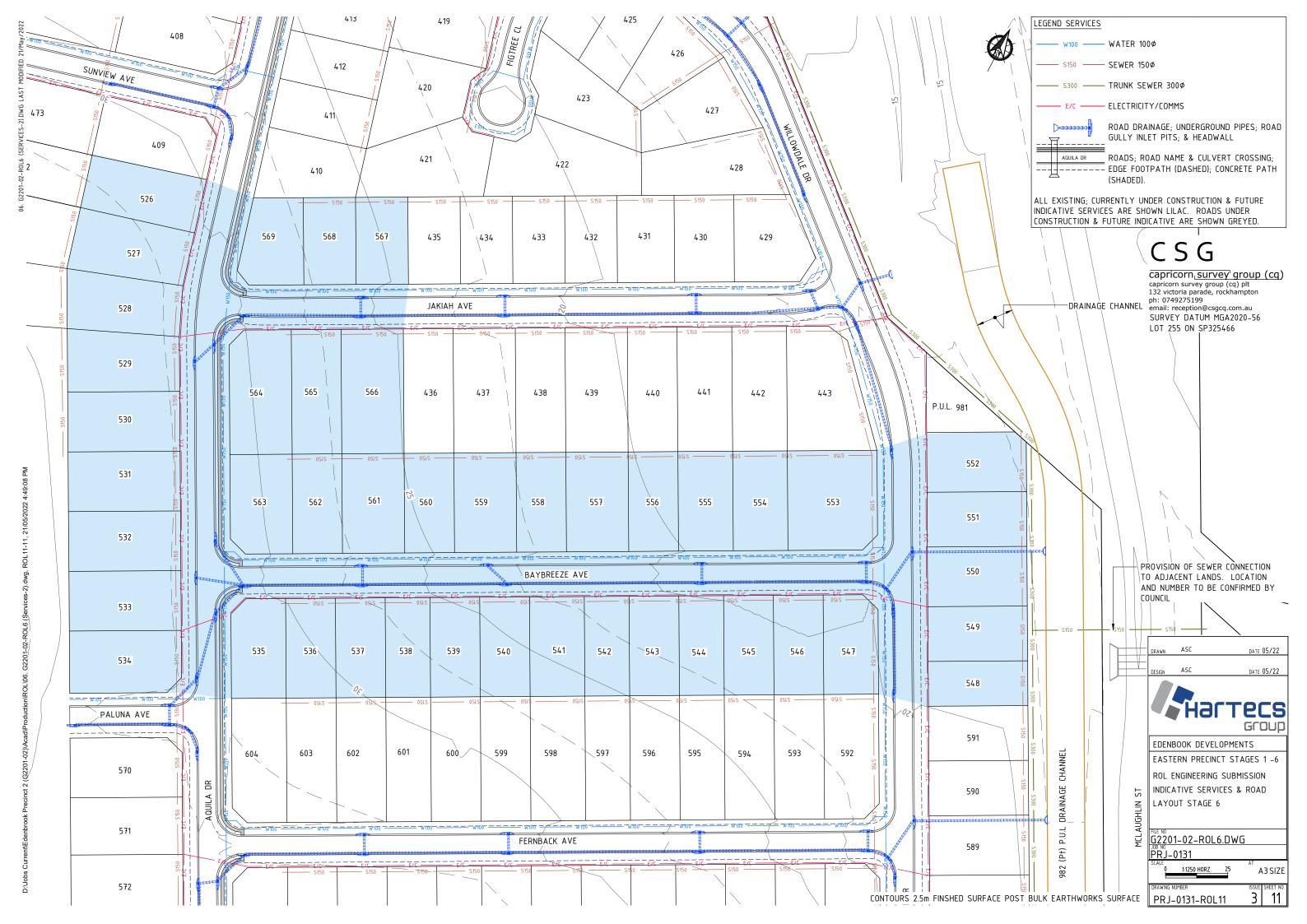


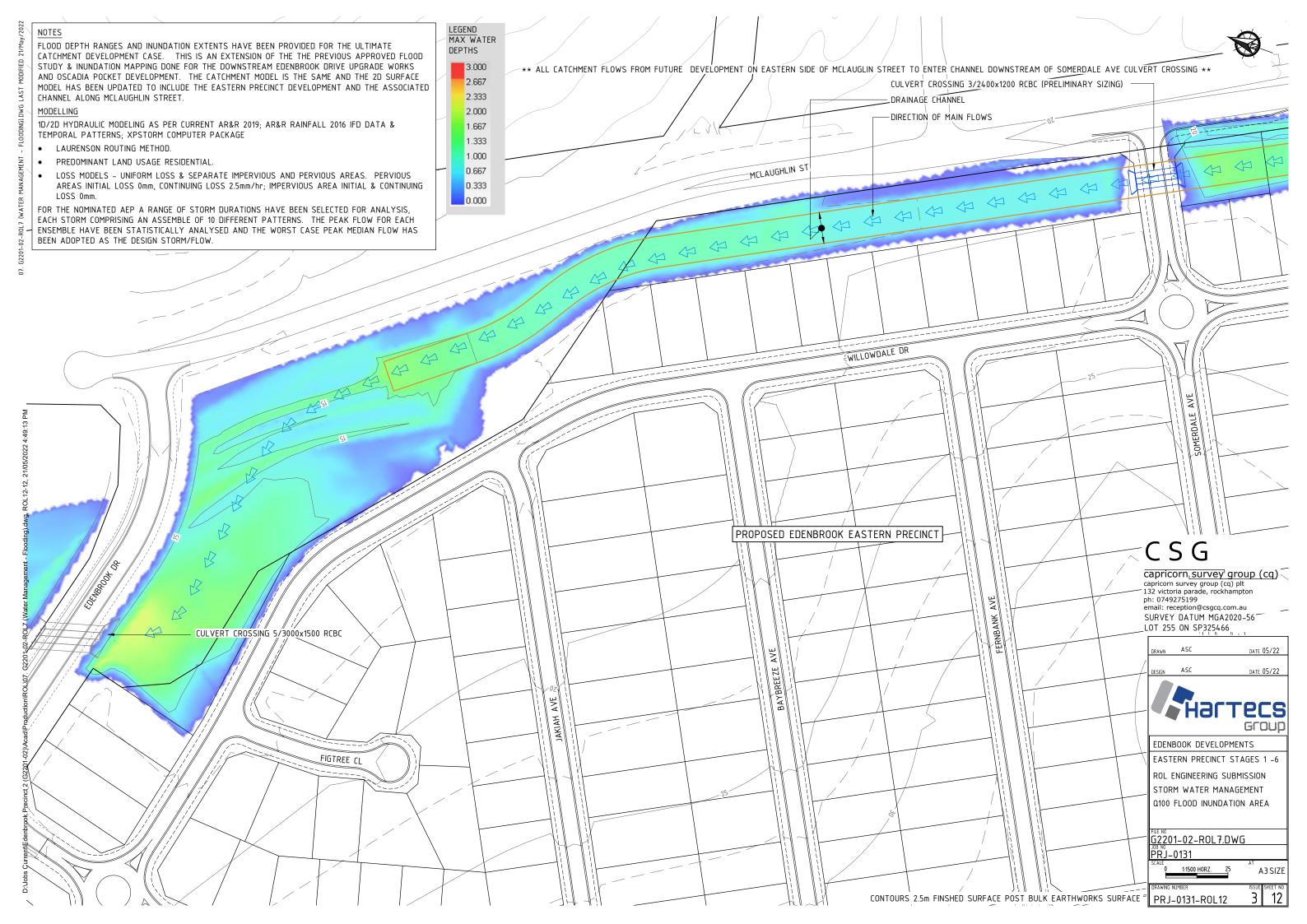














PROPOSED STORM WATER TREATMENT METHODOLOGY SAME AS ADOPTED FOR PREVIOUS EDENBROOK STAGES 8 & 10 - "STREET TREE" CONCEPT WITH CONCENTRATED END OF LINE TREATMENT AREA

- BATTERS GROUND COVER COMPRISING MIXTURE OF NATURAL GRASSES.
- TREATMENT DETENTION BAYS DENSE SHRUBS; HIGH UPTAKE TREES; LONG GRASSES; GROUND & CANOPY COVER "DENSE"; ROCK CENTRAL DRAINAGE STRIP WITH LONG GRASSES AND SELECTED SHRUBS. DEPTH 200mm-500m.
- BUNDS SELECTED HARDY LAWN TYPE GRASS; LOW LEVEL CREEPING SHRUBS; LONG GRASSES. HEIGHT 200mm-500mm.

FINISHED SURF. MCLAUGHLIN ST FILTER MEDIA - "CONDITIONED SOIL" ROCK LINING/FILTER DRAIN. BUND

CSG

capricorn<sub>L</sub>survey group (cq)

capricorn survey group (cq) plt 132 victoria parade, rockhampton ph: 0749275199 email: reception@csgcq.com.au SURVEY DATUM MGA2020-56 LOT 255 ON SP325466

DATE 05/22 ASC Hartecs Group EDENBOOK DEVELOPMENTS EASTERN PRECINCT STAGES 1 -6 ROL ENGINEERING SUBMISSION STORM WATER MANAGEMENT QUALITY (INDICATIVE) G2201-02-R0L8.DWG PR J-0131 A3 SIZE 3 | 13 | PRJ-0131-R0L13

CONTOURS 2.5m FINSHED SURFACE POST BULK EARTHWORKS SURFACE

# **Appendix C**Slope Stability Report



Report on Geotechnical Stability Assessment

Proposed Subdivision Edenbrook Estate (Precinct 2) Edenbrook Drive, Parkhurst

> Prepared for Hartecs Group Pty Ltd

> > Project 213255.00 May 2022





#### **Document History**

#### Document details

Project No.	213255.00	Document No.	R.001.RevA					
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	Proposed Subdivision							
Site address	Edenbrook Estate	(Precinct 2), Edenbroo	ok Drive, Parkhurst					
Report prepared for	Hartecs Group Pty	/ Ltd						
File name	213255.00.R.001.	RevA						

#### Document status and review

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Revision A	Michael-Davies-Hill	Brett Egen (RPEQ8597)	9 May 2022

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The undersigned, on behalf of Douglas Partners Pty Ltd, confirm that this document and all attached drawings, logs and test results have been checked and reviewed for errors, omissions and inaccuracies.

Signature	e	Date	
Author			
Reviewer	REDJUN.	9 May 2022	





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Appendix A: About This Report

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## Report on Geotechnical Stability Assessment Proposed Subdivision Edenbrook Estate (Precinct 2), Edenbrook Drive, Parkhurst

#### 1. Introduction

This report presents the results of a geotechnical stability assessment undertaken by Douglas Partners Pty Ltd (DP) for Precinct 2 as part of the Edenbrook Estate development on Edenbrook Drive, Parkhurst.

The geotechnical assessment was undertaken at the request of Hartecs Group Pty Ltd on behalf of Edenbrook Developments in accordance with DP's proposal 213255.00.P.001 dated 17 February 2022.

The aim of the assessment was to assess the stability of the proposed development in accordance with the requirements of the Rockhampton Regional Council's (RCC) steep land overlay code. The assessment comprised the review of regional geology, previous investigation results, historical aerial photographs, and available online mapping; followed by a site walk-over inspection by a senior geotechnical engineer, stability assessment and reporting.

This report must be read in conjunction with the notes entitled "About This Report" in Appendix A along with any other attached explanatory notes and should be kept in its entirety without separation of individual pages or sections.

#### 2. Site Description and Proposed Development

The development site is described as Lot 255 on SP325466, which encompasses both the northern and southern sides of Edenbrook Drive, Parkhurst (refer to Figure 1).

It is understood that the proposed residential development will comprise approximately 500 to 600 residential lots ranging in size. Supporting infrastructure will include subdivisional roads, water, sewerage and stormwater.

It is further understood that the proposed earthworks for a portion of the overall site will consist of bulk excavations up to approximately 7 m in height along the ridgeline and spurs, and filling up to approximately 9 m in the low lying re-entrants between the spurs (refer to Figure 2); generally creating relatively flat and level building platforms, some locally increasing up to approximately 15%. It is anticipated that similar earthworks will be required for the remainder of the site.





Figure 1: Site Location.

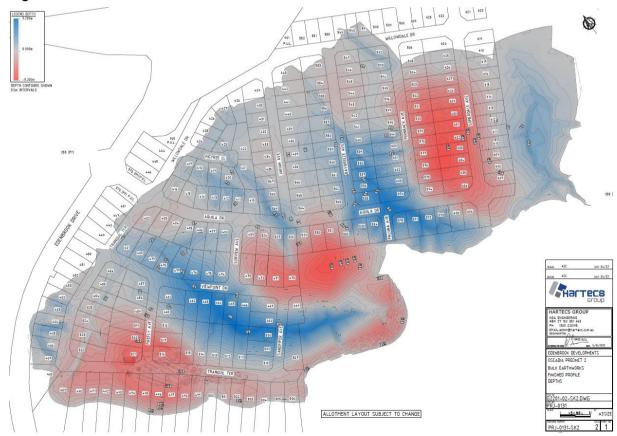


Figure 2: Proposed earthworks for a proportion of the overall site.



#### 3. Published Data

#### 3.1 Regional Geology

Reference to the Geological Survey of Queensland's 1:100,000 scale Rockhampton Region geological map indicates the site is located in an area underlain by the Early Carboniferous aged Rockhampton Group described as typically comprising "mudstone, siltstone, oolitic sandstone, and conglomerate, oolitic and crinoidal limestone" with local folds dipping moderately to steeply to the east.

#### 3.2 Topography

Reference to RCC's online contour mapping, the site is dominated by two prominent topographical features of high relief with a saddle connecting the two along the western part of the site. An elongated spur runs off to the north, with a number of smaller moderately sloping (between 10° and 15°) spurs running off to the north-east, to the east and to the south. A knoll is located atop of a spur towards the eastern part of the site. Steep (between 15° and 20°) re-entrants are located between the spurs. The site is also dominated by a second feature of high relief along the southern boundary of the site. As the site extends to the north-east, it generally flattens out.



Figure 3: RRC Contour Mapping.



#### 3.3 Steep Land

RCC's Steep Land Overlay identifies land with a slope of 15% or greater as being land potentially susceptible to landslide. Reference to the steep land overlay map (Figure 4), typically the moderately sloping side slopes of the spurs, and steeply sloping re-entrants are identified as steep land.

It should be noted that the steep land overlay map is a broad scale indication of the potential landslide susceptibility based on topography alone, and does not consider other factors such as regional geology or evidence of past instability.

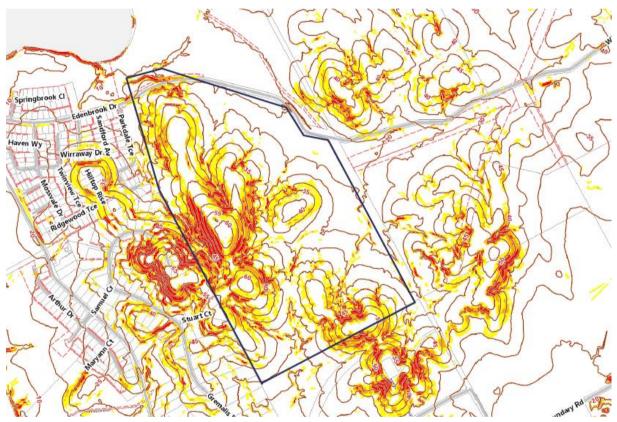


Figure 4: RRC Steep Land Overlay.

#### 3.4 Previous Investigations

The drill logs from previous drilling carried out by CQ Drilling and Blasting Pty Ltd were provided by the client. The previous bores were typically drilled across the western part of the site. The drilling conditions are generally described as being "soft" to between 0.5 m and 2.0 m depth. The "soft" conditions are inferred to be typical of residual soils overlying extremely weathered material, with conditions becoming harder with depth and penetration into less weathered and subsequently stronger rock.



#### 3.5 Aerial Photographs

Aerial photographs from 1956 to present were reviewed to assess for evidence of significant past instability.

The photos indicate no significant evidence of instability or changes in topography on the site.

#### 4. Field Work

The field work was carried out on 16 March 2022 and comprised a walk-over inspection by a senior geotechnical engineer from DP in order to make an appraisal of the general condition of the site in regard to topography, drainage, vegetation cover, geology, erosion and slope stability.

During the site walk-over, topographical features specific to the site were noted, and ground slopes were measured using a hand-held inclinometer.

The exposed conditions on site generally indicate shallow residual soils overlying weathered siltstone, which is consistent with the above described geology and previous borehole drilling by others.

No obvious or significant scarps, naturally hummocky or visibly disturbed ground surface, or tension cracks were observed; which would usually indicate the presence of local or global instability. Any large trees on the slopes were also generally straight.

No signs of groundwater seepage (ie. surface 'springs') were observed at the time of inspection. Surface water from the slopes appear to be naturally diverted towards the re-entrants and typically drain to the north-east or south-west. Localised scour and erosion was noted in a drainage gully located in the south-western corner of the site.

#### 5. Comments

#### 5.1 Slope Stability Risk Assessment

The terminology of the Australian Geomechanics Society (AGS) Practice Note Guidelines for Landslide Risk Management 2007 has been used in the descriptions of hazards and the qualitative assessment of likelihood, consequence and risk of slope instability. Terminology and risk matrix tables from the AGS Practice Note Guidelines are included in Appendix B.

A qualitative assessment of the likelihood, consequence and risk has been carried out for the site, based on the results of the site walk-over and experience in similar projects, provided that development of the site is carried out in accordance with good engineering practice for hillside developments and the recommendations within this report.



Table 1: Slope Instability Risk Assessment to Property

Hazard	Likelihood	Consequence to Property	Risk to Property	Comments
Shallow failure in proposed fill or unsupported cuts	"Unlikely"	"Minor to Medium"	"Low"	The proposed fill is retained by engineered designed retaining walls, with long batters no steeper than 2H:1V
Shallow rotational or translational slide in residual soils	"Unlikely"	"Minor to Medium"	"Low"	The likelihood of a shallow failure through the residual soils is considered unlikely due to the overall strength of these materials and no evidence of previous movement.
Deep rotational failure in residual soils or weathered bedrock	"Rare"	"Major"	"Low	The base geology is generally not adversely bedded or otherwise structured to be prone to deep instability.

Based on the results of the slope stability assessment, considering the geology of the site, relatively shallow depth to rock and the lack of evidence of any previous landslips, the risk to property and to properties adjacent to the site is considered to be "low". The AGS Guidelines suggest that a low level of risk is "usually acceptable" by regulators.

#### 5.2 Geotechnical Constraints

The potential impacts on slope stability for the proposed development have been assessed, and the measures recommended below in particular with reference to the AGS guidelines on hillside constructions have been designed to mitigate those impacts.

#### 5.2.1 Earthworks

Suitable unsurcharged temporary and permanent dry cut and fill batter slopes up to 3 m in height are presented in Table 2. Advice should be sought from DP for batter slopes greater than 3 m in height. Where groundwater seepage is encountered, batter slopes will need to be considerably flatter.



Table 2: Batter Slopes (unsurcharged, up to 3 m in height)

Material	Safe Batter Slope (H:V)	
	Short Term	Long Term
Controlled fill*, residual soils	1:1	2:1
Weathered rock	1:1	1.5:1

Notes: \* Depends on fill material type and level of compaction. Assumes clayey material compacted under 'Level 1' inspection and testing to minimum dry density ratio of 95% for Standard compaction.

Temporary excavations up to 1.5 m in depth may remain near vertical for short periods of time, provided that they remain dry at the time of construction and provided there are no loads, services, structures or traffic located within a distance from the crest equal to the batter height.

The above batter slopes are suggested with respect to slope stability only and do not allow for lateral stress relaxation which may result in movement of nearby in-ground services or shallow footings. If such services or footings are settlement sensitive, then the excavation may have to be positively supported.

Slopes may need to be flattened to 4H:1V or less, in order to allow vehicle access for maintenance of the slopes. It is recommended that all batters incorporate crest and toe drainage. The batters should also be covered with topsoil and vegetation (or similar) to provide long term erosion protection.

Long term cuts in very low strength (or stronger) rock is dependent upon the joint orientation within the rock mass. The above batter slopes are contingent upon geotechnical inspections during construction to verify that no adverse jointing and/or defects are present in the batter face. Steeper batters may be possible with the inclusion of passive nails/dowels, anchors and surface protection, but would be subject to detailed stability assessment.

It is recommended that where fill is to be placed over sloping ground, the slope should be benched to allow for the fill to be 'keyed' into the existing slope. These procedures will provide for greater stability of the fill and allow for adequate compaction to be achieved throughout the full depth of the fill. Filled batters should also be overfilled and then cut back to the required design batter angle in order to maximise compaction of the material in the batter faces.

Approved bulk fill should be placed in layers not exceeding 0.3 m 'loose' thickness, with each layer compacted to a minimum dry density ratio of 95% relative to Standard compaction. Where fill has a significant clay content, moisture content within the fill should be maintained within 2% of OMC during and after compaction. The upper 0.3 m of pavement subgrade and unbound pavement gravels should be compacted to a minimum dry density ratio of 100% relative to Standard compaction and to within the same moisture content range as given above.

Care should be taken not to use over-wet clayey soils as this can lead to problems associated with trafficability and workability. Clayey soils should also not be over-compacted (ie. not more than 102% Standard) or placed too dry of OMC, as this can lead to future swelling and softening with changes to moisture content or inundation from water.



Field density testing should be carried out to confirm the standard of compaction has been achieved and the placement moisture content. The frequency of testing should be carried out in accordance with AS 3798 (2007) and distributed reasonably evenly throughout the full depth and area of filling.

Level 1 inspection and testing of filling must be undertaken where the fill is to support buildings or pavements. It is also recommended that Level 1 inspection and testing be adopted for all trench backfill greater than 1.5 m deep in areas to support buildings or pavements as settlement of deep trench backfill can have significant impact on these works.

#### 5.2.2 Retaining Walls

The design of flexible and rigid retaining walls could be undertaken using a triangular pressure distribution and the earth pressure parameters given in Table 3. Flexible walls are those which are free to rotate or tilt (such as cantilevered walls) and should be designed using an active (Ka) earth pressure coefficient. Rigid walls are those which are restrained against rotation or tilt (ie. single anchored/propped walls) and should be designed using the at-rest earth pressure (Ko).

Passive resistance (Kp) at the toe of the wall should be ignored in the zone where future disturbance (eg. services trenches) could occur.

Table 3: Earth Pressure Coefficients (non-sloping crest backfill)

Material	Unit Weight (kN/m³)	Friction Angle (degrees)	Active Ka	At Rest Ko	Passive Kp
Controlled fill*, residual clay soils	19	26	0.40	0.55	2.5
Weathered rock	21	36	0.25	0.40	3.6

Notes: \* Depends on fill material type and level of compaction. Assumes clayey material compacted under 'Level 1' inspection and testing.

Allowance should be made for hydrostatic pressure build-up behind the retaining wall. It is recommended that all retaining walls be drained for full height in order to minimise hydrostatic pressure build-up behind the wall. Additional guidelines on wall drainage are provided in Appendix G of AS 4678 (2002).

Allowance for surcharge loads and sloping crest should also be made as appropriate. The effect of surcharge should be included by multiplying the vertical pressure developed by the surcharge by the appropriate lateral earth pressure coefficient as given in Table 3.

Preference should be given to adopting thin soil layers and using small hand-controlled compaction equipment during backfilling against retaining walls. This is in order to limit the stress applied to the walls during construction. Should heavy compaction be required, then wall stresses will be well in excess of Ko and temporary propping should be used.

Clayey backfill should not be placed too dry of optimum moisture content, as this can lead to increased future swelling with changes to moisture content or inundation from water creating additional load on the back of the wall.



It is recommended that factors of safety of 2 against overturning and sliding stability and 1.5 for global stability, be adopted in the design of all retaining walls.

For limit state design methods, the ultimate parameters provided above in Table 3 will need to be factored in accordance with AS 4678. Guidance on the selection of material strength partial factors is provided in Section 5.2 of AS 4678 and is dependent upon the nature and state of the insitu soils.

#### 5.2.3 Footing Design

Provided that earthworks is carried out in accordance with the recommendations in this report, it is considered that high level pad and/or strip footings founded in either controlled fill, competent residual soils or weathered rock may be adopted. Where the change in depth of fill is significant across a building platform (especially where there is cut to fill), the potential for differential movements should be noted, and if these are significant then piers through the fill and founding into natural should be adopted.

Slabs supported on high level footings should be stiffened to suit the expected ground surface movements due to potential soil reactivity. This should be confirmed following future site investigations on individual lots as required for building design.

'Pole' type houses are generally preferred on moderate to steeply sloping lots (if any), unless the buildings are benched into the hillslope.

Embedment required for retaining wall footings will be dependent on global stability checks as part of the retaining wall design.

All footing excavations should be inspected and tested by an experienced geotechnical to confirm bearing pressures prior to casting of concrete.

The above footing recommendations are considered to be the minimum requirements from a slope stability viewpoint and final footing design details will be dependent upon the extent of earthworks, proposed development loads and what is considered acceptable in terms of settlement and cost.

#### 5.2.4 Drainage

For subdivisional works, all stormwater collected on site should be prevented from discharging directly onto the slope or from ponding on the proposed building envelopes. All stormwater and surface water is to be directed via an approved stormwater containment system in a controlled manner to appropriate discharge points.



#### 6. References

AGS. (2007). *Practice Note Guidelines for Landslide Risk Management*. Australian Geomechnics, Volume 42, No 1: Australian Geomechanics Society, Landslide Taskforce, Landslide Practice Note Working Group.

AS 3798. (2007). Guidelines on Earthworks for Commercial and Residential Developments. Standards Australia.

AS 4678. (2002). Earth-retaining structures. Standards Australia.

#### 7. Limitations

Douglas Partners Pty Ltd (DP) has prepared this report for Precinct 2 as part of the Edenbrook Estate, Edenbrook Drive, Parkhurst in accordance with DP's proposal 213255.00.P.001 dated 17 February 2022. This report is provided for the exclusive use of Hartecs Group Pty Ltd and Edenbrook Developments for this project only and for the purposes as described in the report. It should not be used by or relied upon for other projects or purposes on the same or other site or by a third party. Any party so relying upon this report beyond its exclusive use and purpose as stated above, and without the express written consent of DP, does so entirely at its own risk and without recourse to DP for any loss or damage. In preparing this report DP has necessarily relied upon information provided by the client and/or their agents.

DP's advice is based upon the conditions encountered during previous investigations and observed during the site walk-over. The accuracy of the advice provided by DP in this report may be affected by undetected variations in ground conditions across the site between and beyond the sampling and/or testing locations. The advice may also be limited by budget constraints imposed by others or by site accessibility.

The assessment of atypical safety hazards arising from this advice is restricted to the geotechnical components set out in this report and based on known project conditions and stated design advice and assumptions. While some recommendations for safe controls may be provided, detailed 'safety in design' assessment is outside the current scope of this report and requires additional project data and assessment.

This report must be read in conjunction with all of the attached and should be kept in its entirety without separation of individual pages or sections. DP cannot be held responsible for interpretations or conclusions made by others unless they are supported by an expressed statement, interpretation, outcome or conclusion stated in this report.

This report, or sections from this report, should not be used as part of a specification for a project, without review and agreement by DP. This is because this report has been written as advice and opinion rather than instructions for construction.

#### **Douglas Partners Pty Ltd**

# Appendix A

About This Report

# About this Report Douglas Partners

#### Introduction

These notes have been provided to amplify DP's report in regard to classification methods, field procedures and the comments section. Not all are necessarily relevant to all reports.

DP's reports are based on information gained from limited subsurface excavations and sampling, supplemented by knowledge of local geology and experience. For this reason, they must be regarded as interpretive rather than factual documents, limited to some extent by the scope of information on which they rely.

#### Copyright

This report is the property of Douglas Partners Pty Ltd. The report may only be used for the purpose for which it was commissioned and in accordance with the Conditions of Engagement for the commission supplied at the time of proposal. Unauthorised use of this report in any form whatsoever is prohibited.

#### **Borehole and Test Pit Logs**

The borehole and test pit logs presented in this report are an engineering and/or geological interpretation of the subsurface conditions, and their reliability will depend to some extent on frequency of sampling and the method of drilling or excavation. Ideally, continuous undisturbed sampling or core drilling will provide the most reliable assessment, but this is not always practicable or possible to justify on economic grounds. In any case the boreholes and test pits represent only a very small sample of the total subsurface profile.

Interpretation of the information and its application to design and construction should therefore take into account the spacing of boreholes or pits, the frequency of sampling, and the possibility of other than 'straight line' variations between the test locations.

#### Groundwater

Where groundwater levels are measured in boreholes there are several potential problems, namely:

 In low permeability soils groundwater may enter the hole very slowly or perhaps not at all during the time the hole is left open;

- A localised, perched water table may lead to an erroneous indication of the true water table;
- Water table levels will vary from time to time with seasons or recent weather changes.
   They may not be the same at the time of construction as are indicated in the report;
- The use of water or mud as a drilling fluid will mask any groundwater inflow. Water has to be blown out of the hole and drilling mud must first be washed out of the hole if water measurements are to be made.

More reliable measurements can be made by installing standpipes which are read at intervals over several days, or perhaps weeks for low permeability soils. Piezometers, sealed in a particular stratum, may be advisable in low permeability soils or where there may be interference from a perched water table.

#### Reports

The report has been prepared by qualified personnel, is based on the information obtained from field and laboratory testing, and has been undertaken to current engineering standards of interpretation and analysis. Where the report has been prepared for a specific design proposal, the information and interpretation may not be relevant if the design proposal is changed. If this happens, DP will be pleased to review the report and the sufficiency of the investigation work.

Every care is taken with the report as it relates to interpretation of subsurface conditions, discussion of geotechnical and environmental aspects, and recommendations or suggestions for design and construction. However, DP cannot always anticipate or assume responsibility for:

- Unexpected variations in ground conditions.
   The potential for this will depend partly on borehole or pit spacing and sampling frequency:
- Changes in policy or interpretations of policy by statutory authorities; or
- The actions of contractors responding to commercial pressures.

If these occur, DP will be pleased to assist with investigations or advice to resolve the matter.

### About this Report

#### **Site Anomalies**

In the event that conditions encountered on site during construction appear to vary from those which were expected from the information contained in the report, DP requests that it be immediately notified. Most problems are much more readily resolved when conditions are exposed rather than at some later stage, well after the event.

#### **Information for Contractual Purposes**

Where information obtained from this report is provided for tendering purposes, it is recommended that all information, including the written report and discussion, be made available. In circumstances where the discussion or comments section is not relevant to the contractual situation, it may be appropriate to prepare a specially edited document. DP would be pleased to assist in this regard and/or to make additional report copies available for contract purposes at a nominal charge.

#### Site Inspection

The company will always be pleased to provide engineering inspection services for geotechnical and environmental aspects of work to which this report is related. This could range from a site visit to confirm that conditions exposed are as expected, to full time engineering presence on site.

# Appendix B

**AGS Guidelines** 

#### PRACTICE NOTE GUIDELINES FOR LANDSLIDE RISK MANAGEMENT 2007

#### APPENDIX C: - QUALITATIVE TERMINOLOGY FOR USE IN ASSESSING RISK TO PROPERTY (CONTINUED)

#### QUALITATIVE RISK ANALYSIS MATRIX – LEVEL OF RISK TO PROPERTY

LIKELIHO	CONSEQUENCES TO PROPERTY (With Indicative Approximate Cost of Damage)					
	Indicative Value of Approximate Annual Probability	1: CATASTROPHIC 200%	2: MAJOR 60%	3: MEDIUM 20%	4: MINOR 5%	5: INSIGNIFICANT 0.5%
A - ALMOST CERTAIN	10 <sup>-1</sup>	VH	VH	VH	Н	M or <b>L</b> (5)
B - LIKELY	10-2	VH	VH	Н	M	L
C - POSSIBLE	10 <sup>-3</sup>	VH	Н	М	M	VL
D - UNLIKELY	10 <sup>-4</sup>	Н	M	L	L	VL
E - RARE	10 <sup>-5</sup>	M	L	L	VL	VL
F - BARELY CREDIBLE	10 <sup>-6</sup>	L	VL	VL	VL	VL

Notes:

- For Cell A5, may be subdivided such that a consequence of less than 0.1% is Low Risk.
- When considering a risk assessment it must be clearly stated whether it is for existing conditions or with risk control measures which may not be implemented at the current (6) time.

#### RISK LEVEL IMPLICATIONS

	Risk Level	Example Implications (7)
VH	VERY HIGH RISK	Unacceptable without treatment. Extensive detailed investigation and research, planning and implementation of treatment options essential to reduce risk to Low; may be too expensive and not practical. Work likely to cost more than value of the property.
Н	HIGH RISK	Unacceptable without treatment. Detailed investigation, planning and implementation of treatment options required to reduce risk to Low. Work would cost a substantial sum in relation to the value of the property.
M	MODERATE RISK	May be tolerated in certain circumstances (subject to regulator's approval) but requires investigation, planning and implementation of treatment options to reduce the risk to Low. Treatment options to reduce to Low risk should be implemented as soon as practicable.
L	LOW RISK	Usually acceptable to regulators. Where treatment has been required to reduce the risk to this level, ongoing maintenance is required.
VL	VERY LOW RISK	Acceptable. Manage by normal slope maintenance procedures.

The implications for a particular situation are to be determined by all parties to the risk assessment and may depend on the nature of the property at risk; these are only **Note:** (7) given as a general guide.

#### PRACTICE NOTE GUIDELINES FOR LANDSLIDE RISK MANAGEMENT 2007

#### APPENDIX C: LANDSLIDE RISK ASSESSMENT

#### QUALITATIVE TERMINOLOGY FOR USE IN ASSESSING RISK TO PROPERTY

#### QUALITATIVE MEASURES OF LIKELIHOOD

Approximate A Indicative Value			Description	Descriptor	Level	
10-1	5x10 <sup>-2</sup>	10 years	20	The event is expected to occur over the design life.	ALMOST CERTAIN	A
10 <sup>-2</sup>	5x10 <sup>-3</sup>	100 years	20 years 200 years	The event will probably occur under adverse conditions over the design life.	LIKELY	В
10 <sup>-3</sup>		1000 years	200 years 2000 years	The event could occur under adverse conditions over the design life.	POSSIBLE	C
10 <sup>-4</sup>	5x10 <sup>-4</sup>	10,000 years	20,000 years	The event might occur under very adverse circumstances over the design life.	UNLIKELY	D
10 <sup>-5</sup>	$5x10^{-5}$ $5x10^{-6}$	100,000 years	, ,	The event is conceivable but only under exceptional circumstances over the design life.	RARE	Е
10 <sup>-6</sup>	3810	1,000,000 years	200,000 years	The event is inconceivable or fanciful over the design life.	BARELY CREDIBLE	F

Note: (1) The table should be used from left to right; use Approximate Annual Probability or Description to assign Descriptor, not vice versa.

#### QUALITATIVE MEASURES OF CONSEQUENCES TO PROPERTY

Approximate Cost of Damage		Description	Descriptor	Torrit
Indicative Value	Notional Boundary	Description	Descriptor	Level
200%	1000/	Structure(s) completely destroyed and/or large scale damage requiring major engineering works for stabilisation. Could cause at least one adjacent property major consequence damage.	CATASTROPHIC	1
60%	100%	Extensive damage to most of structure, and/or extending beyond site boundaries requiring significant stabilisation works. Could cause at least one adjacent property medium consequence damage.	MAJOR	2
20%	40% 10%	Moderate damage to some of structure, and/or significant part of site requiring large stabilisation works.  Could cause at least one adjacent property minor consequence damage.	MEDIUM	3
5%	1%	Limited damage to part of structure, and/or part of site requiring some reinstatement stabilisation works.	MINOR	4
0.5%	170	Little damage. (Note for high probability event (Almost Certain), this category may be subdivided at a notional boundary of 0.1%. See Risk Matrix.)	INSIGNIFICANT	5

**Notes:** 

- (2) The Approximate Cost of Damage is expressed as a percentage of market value, being the cost of the improved value of the unaffected property which includes the land plus the unaffected structures.
- (3) The Approximate Cost is to be an estimate of the direct cost of the damage, such as the cost of reinstatement of the damaged portion of the property (land plus structures), stabilisation works required to render the site to tolerable risk level for the landslide which has occurred and professional design fees, and consequential costs such as legal fees, temporary accommodation. It does not include additional stabilisation works to address other landslides which may affect the property.
- (4) The table should be used from left to right; use Approximate Cost of Damage or Description to assign Descriptor, not vice versa

#### PRACTICE NOTE GUIDELINES FOR LANDSLIDE RISK MANAGEMENT 2007

#### APPENDIX G - SOME GUIDELINES FOR HILLSIDE CONSTRUCTION

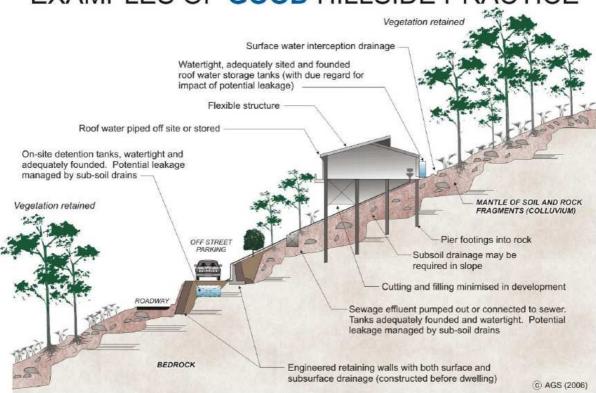
#### GOOD ENGINEERING PRACTICE

ADVICE

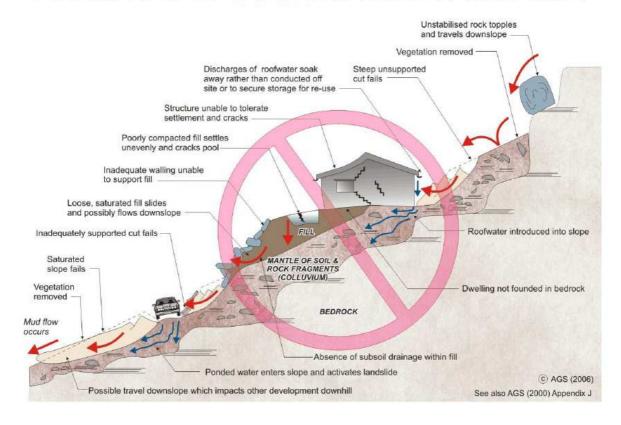
#### POOR ENGINEERING PRACTICE

GEOTECHNICAL	Obtain advice from a qualified, experienced geotechnical practitioner at early	Prepare detailed plan and start site works before
ASSESSMENT	stage of planning and before site works.	geotechnical advice.
PLANNING		
SITE PLANNING	Having obtained geotechnical advice, plan the development with the risk arising from the identified hazards and consequences in mind.	Plan development without regard for the Risk.
DESIGN AND CON		
	Use flexible structures which incorporate properly designed brickwork, timber	Floor plans which require extensive cutting and
HOUSE DESIGN	or steel frames, timber or panel cladding.	filling.
HOUSE DESIGN	Consider use of split levels.	Movement intolerant structures.
	Use decks for recreational areas where appropriate.	
SITE CLEARING	Retain natural vegetation wherever practicable.	Indiscriminately clear the site.
ACCESS & DRIVEWAYS	Satisfy requirements below for cuts, fills, retaining walls and drainage.  Council specifications for grades may need to be modified.	Excavate and fill for site access before geotechnical advice.
DRIVEWAIS	Driveways and parking areas may need to be fully supported on piers.	geotechnical advice.
EARTHWORKS	Retain natural contours wherever possible.	Indiscriminatory bulk earthworks.
	Minimise depth.	Large scale cuts and benching.
CUTS	Support with engineered retaining walls or batter to appropriate slope.	Unsupported cuts.
	Provide drainage measures and erosion control.	Ignore drainage requirements
	Minimise height.	Loose or poorly compacted fill, which if it fails,
	Strip vegetation and topsoil and key into natural slopes prior to filling.	may flow a considerable distance including
Enro	Use clean fill materials and compact to engineering standards.	onto property below.
FILLS	Batter to appropriate slope or support with engineered retaining wall.  Provide surface drainage and appropriate subsurface drainage.	Block natural drainage lines. Fill over existing vegetation and topsoil.
	Trovide surface dramage and appropriate subsurface dramage.	Include stumps, trees, vegetation, topsoil,
		boulders, building rubble etc in fill.
ROCK OUTCROPS	Remove or stabilise boulders which may have unacceptable risk.	Disturb or undercut detached blocks or
& BOULDERS	Support rock faces where necessary.	boulders.
	Engineer design to resist applied soil and water forces.	Construct a structurally inadequate wall such as
RETAINING	Found on rock where practicable.	sandstone flagging, brick or unreinforced
WALLS	Provide subsurface drainage within wall backfill and surface drainage on slope	blockwork.
	above. Construct wall as soon as possible after cut/fill operation.	Lack of subsurface drains and weepholes.
	Found within rock where practicable.	Found on topsoil, loose fill, detached boulders
	Use rows of piers or strip footings oriented up and down slope.	or undercut cliffs.
FOOTINGS	Design for lateral creep pressures if necessary.	
	Backfill footing excavations to exclude ingress of surface water.	
	Engineer designed.	
	Support on piers to rock where practicable.	
SWIMMING POOLS	Provide with under-drainage and gravity drain outlet where practicable.	
	Design for high soil pressures which may develop on uphill side whilst there may be little or no lateral support on downhill side.	
DRAINAGE	may be fittle of no fateral support on downline side.	
2111111102	Provide at tops of cut and fill slopes.	Discharge at top of fills and cuts.
	Discharge to street drainage or natural water courses.	Allow water to pond on bench areas.
SURFACE	Provide general falls to prevent blockage by siltation and incorporate silt traps.	
	Line to minimise infiltration and make flexible where possible.	
-	Special structures to dissipate energy at changes of slope and/or direction.	Di i con con i con
	Provide filter around subsurface drain.	Discharge roof runoff into absorption trenches.
Subsurface	Provide drain behind retaining walls. Use flexible pipelines with access for maintenance.	
	Prevent inflow of surface water.	
	Usually requires pump-out or mains sewer systems; absorption trenches may	Discharge sullage directly onto and into slopes.
SEPTIC &	be possible in some areas if risk is acceptable.	Use absorption trenches without consideration
SULLAGE	Storage tanks should be water-tight and adequately founded.	of landslide risk.
EROSION	Control erosion as this may lead to instability.	Failure to observe earthworks and drainage
CONTROL &	Revegetate cleared area.	recommendations when landscaping.
LANDSCAPING		
	ITE VISITS DURING CONSTRUCTION	
DRAWINGS	Building Application drawings should be viewed by geotechnical consultant	
SITE VISITS	Site Visits by consultant may be appropriate during construction/	
	MAINTENANCE BY OWNER	
OWNER'S	Clean drainage systems; repair broken joints in drains and leaks in supply	
RESPONSIBILITY	pipes.	
	Where structural distress is evident see advice.	
	If seepage observed, determine causes or seek advice on consequences.	<u> </u>

## **EXAMPLES OF GOOD HILLSIDE PRACTICE**



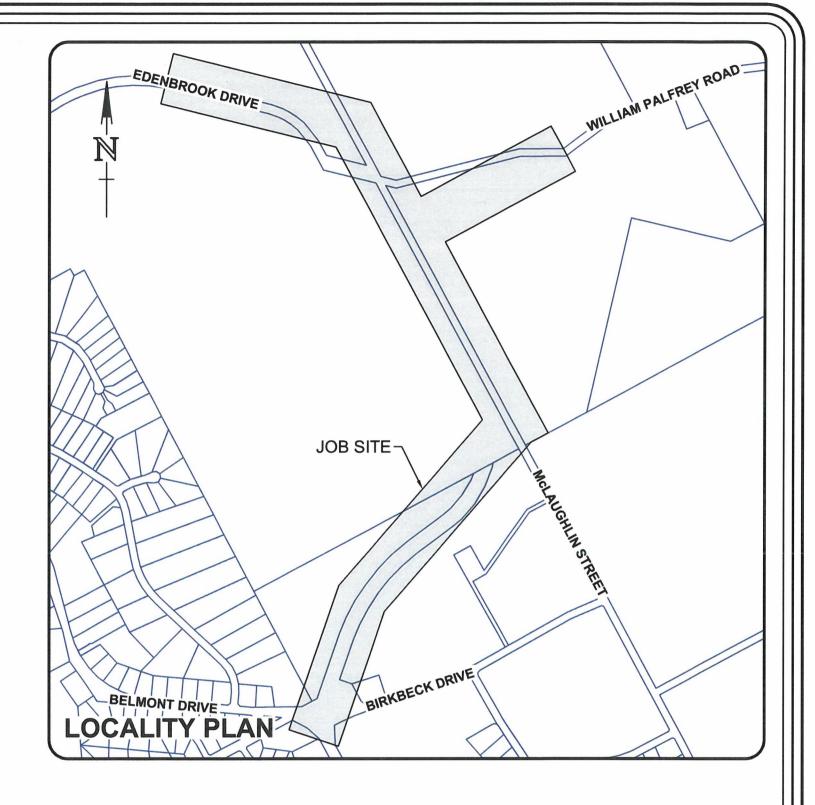
# **EXAMPLES OF POOR HILLSIDE PRACTICE**



# Appendix D RRC PRELIMINARY DESIGN FOR MCLAUGHLIN STREET (first 10 drawings of RRC set only)



DWG	DRAWING INDEX
No.	DIVAVVIIVO INDEX
	ROADWORKS CONSTRUCTION
2020-229-01	OVERALL LAYOUT PLAN
2020-229-02	TYPICAL SECTIONS & DETAILS
2020-229-03	WORKING PLAN - CONTROL LINE 1 - SHEET 1 OF 4
2020-229-04	WORKING PLAN - CONTROL LINE 1 - SHEET 2 OF 4
2020-229-05	WORKING PLAN - CONTROL LINE 1 - SHEET 3 OF 4
2020-229-06	WORKING PLAN - CONTROL LINE 1 - SHEET 4 OF 4
2020-229-07	WORKING PLAN - CONTROL LINE 2
2020-229-08	WORKING PLAN - CONTROL LINE 3
2020-229-09	DRAINAGE CATCHMENT PLAN
2020-229-10	DRAINAGE DETAILS - DRAIN LINE 1
2020-229-11	DRAINAGE DETAILS - DRAIN LINE 2
2020-229-12	DRAINAGE DETAILS - DRAIN LINE 3
2020-229-13	DRAINAGE DETAILS - DRAIN LINE 4
2020-229-14	CROSS SECTIONS - CONTROL LINE 1 - SH 1 OF 21
2020-229-15	CROSS SECTIONS - CONTROL LINE 1 - SH 2 OF 21
2020-229-16	CROSS SECTIONS - CONTROL LINE 1 - SH 3 OF 21
2020-229-17	CROSS SECTIONS - CONTROL LINE 1 - SH 4 OF 21
2020-229-18	CROSS SECTIONS - CONTROL LINE 1 - SH 5 OF 21
2020-229-19	CROSS SECTIONS - CONTROL LINE 1 - SH 6 OF 21
2020-229-20	CROSS SECTIONS - CONTROL LINE 1 - SH 7 OF 21
2020-229-21	CROSS SECTIONS - CONTROL LINE 1 - SH 8 OF 21
2020-229-22	CROSS SECTIONS - CONTROL LINE 1 - SH 9 OF 21
2020-229-23	CROSS SECTIONS - CONTROL LINE 1 - SH 10 OF 21
2020-229-24	CROSS SECTIONS - CONTROL LINE 1 - SH 11 OF 21
2020-229-25	CROSS SECTIONS - CONTROL LINE 1 - SH 12 OF 21
2020-229-26	CROSS SECTIONS - CONTROL LINE 1 - SH 13 OF 21
2020-229-27	CROSS SECTIONS - CONTROL LINE 1 - SH 14 OF 21
2020-229-28	CROSS SECTIONS - CONTROL LINE 1 - SH 15 OF 21
2020-229-29	CROSS SECTIONS - CONTROL LINE 1 - SH 16 OF 21
2020-229-30	CROSS SECTIONS - CONTROL LINE 1 - SH 17 OF 21
2020-229-31	CROSS SECTIONS - CONTROL LINE 1 - SH 18 OF 21
2020-229-32	CROSS SECTIONS - CONTROL LINE 1 - SH 19 OF 21
2020-229-33	CROSS SECTIONS - CONTROL LINE 1 - SH 20 OF 21
2020-229-34	CROSS SECTIONS - CONTROL LINE 1 - SH 21 OF 21
2020-229-35	CROSS SECTIONS - CONTROL LINE 2 - SH 1 OF 6 CROSS SECTIONS - CONTROL LINE 2 - SH 2 OF 6
2020-229-36 2020-229-37	CROSS SECTIONS - CONTROL LINE 2 - SH 2 OF 6  CROSS SECTIONS - CONTROL LINE 2 - SH 3 OF 6
2020-229-37	CROSS SECTIONS - CONTROL LINE 2 - SH 3 OF 6  CROSS SECTIONS - CONTROL LINE 2 - SH 4 OF 6
2020-229-38	CROSS SECTIONS - CONTROL LINE 2 - SH 4 OF 6  CROSS SECTIONS - CONTROL LINE 2 - SH 5 OF 6
2020-229-39	CROSS SECTIONS - CONTROL LINE 2 - SH 5 OF 6  CROSS SECTIONS - CONTROL LINE 2 - SH 6 OF 6
	CROSS SECTIONS - CONTROL LINE 2 - SH 6 OF 6  CROSS SECTIONS - CONTROL LINE 3 - SH 1 OF 2
2020-229-41 2020-229-42	CROSS SECTIONS - CONTROL LINE 3 - SH 1 OF 2  CROSS SECTIONS - CONTROL LINE 3 - SH 2 OF 2
2020-229-42	CROSS SECTIONS - CONTROL LINE 3 - 3H 2 OF 2

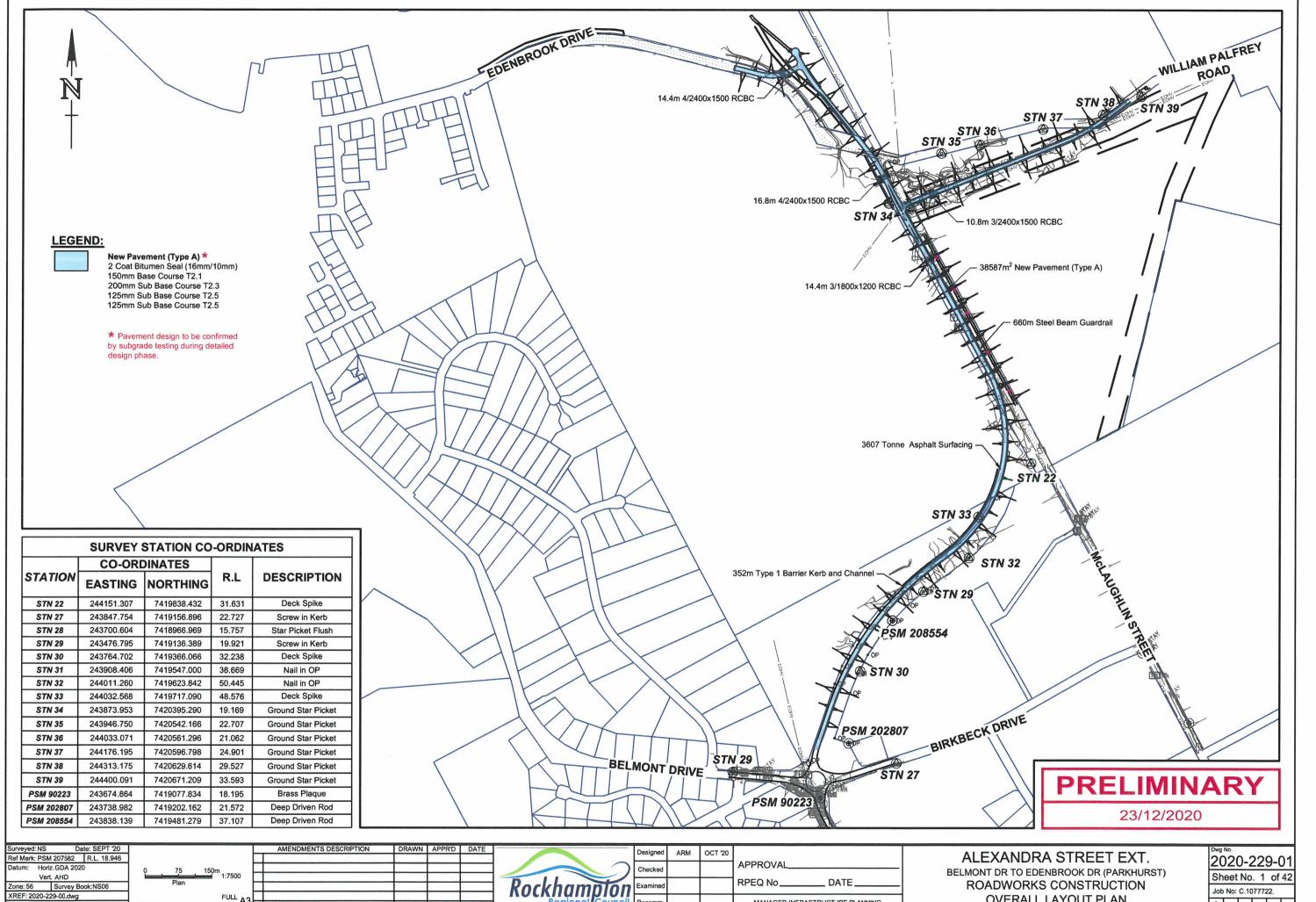


ALEXANDRA STREET EXT.

BELMONT DR TO EDENBROOK DR (PARKHURST)

ROADWORKS CONSTRUCTION

PROJECT No. 2020-229

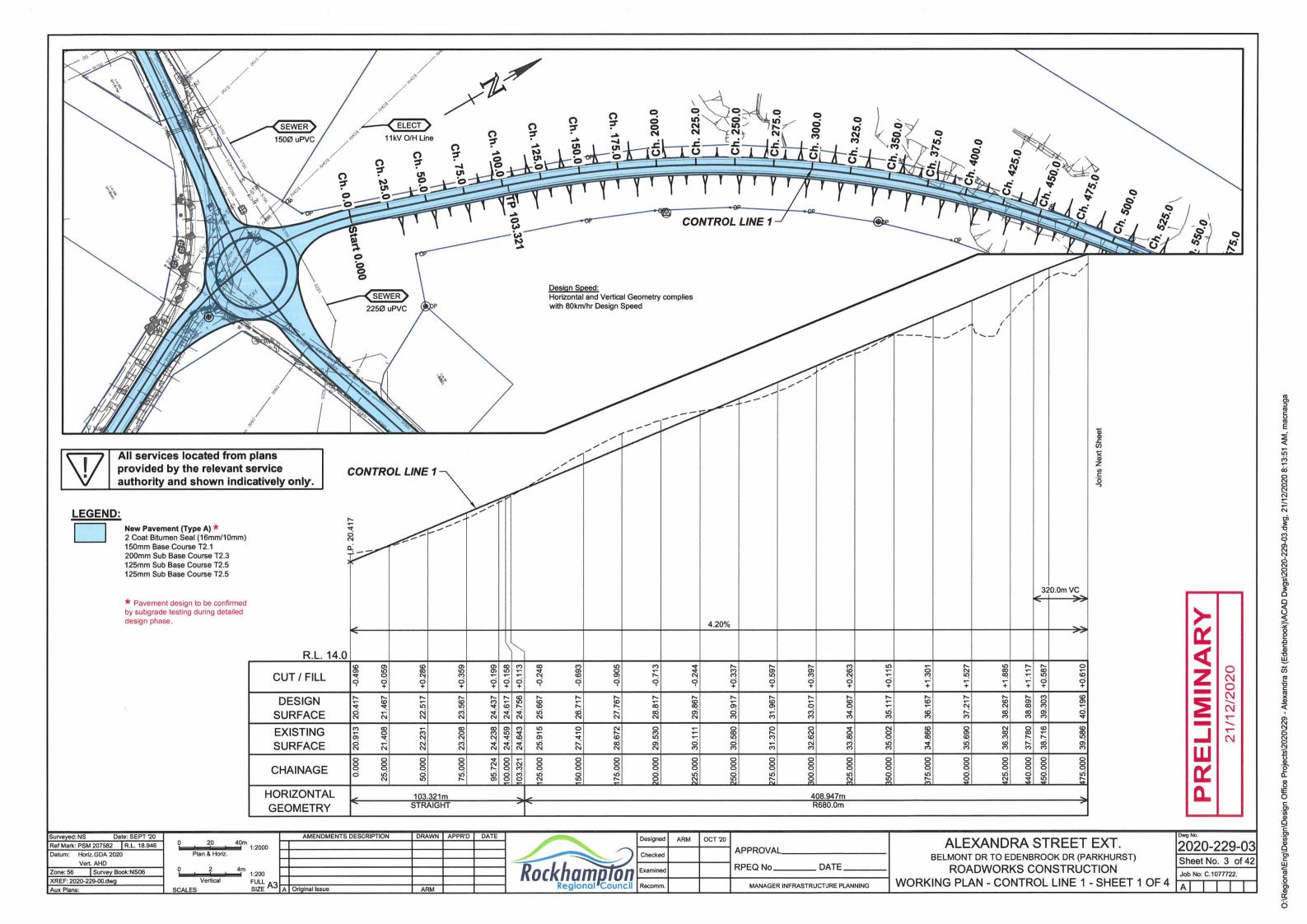


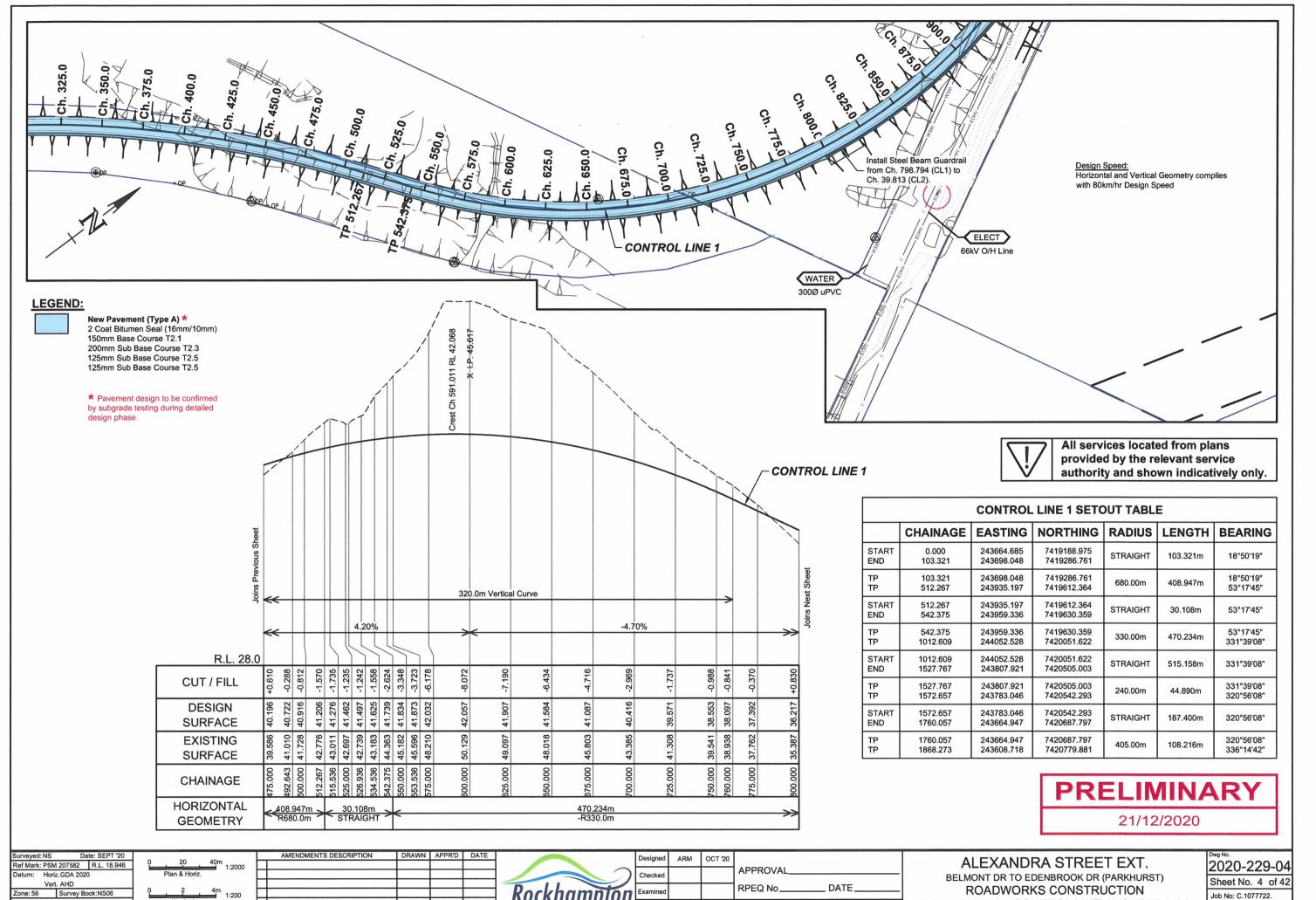
XREF: 2020-229-00.dwg

Job No: C.1077722.

**OVERALL LAYOUT PLAN** 

MANAGER INFRASTRUCTURE PLANNING





FULL

WORKING PLAN - CONTROL LINE 1 - SHEET 2 OF 4

MANAGER INFRASTRUCTURE PLANNING

Vertical

XREF: 2020-229-00.dwg

FULL A3 A Original Iss

WORKING PLAN - CONTROL LINE 1 - SHEET 3 OF 4

MANAGER INFRASTRUCTURE PLANNING

