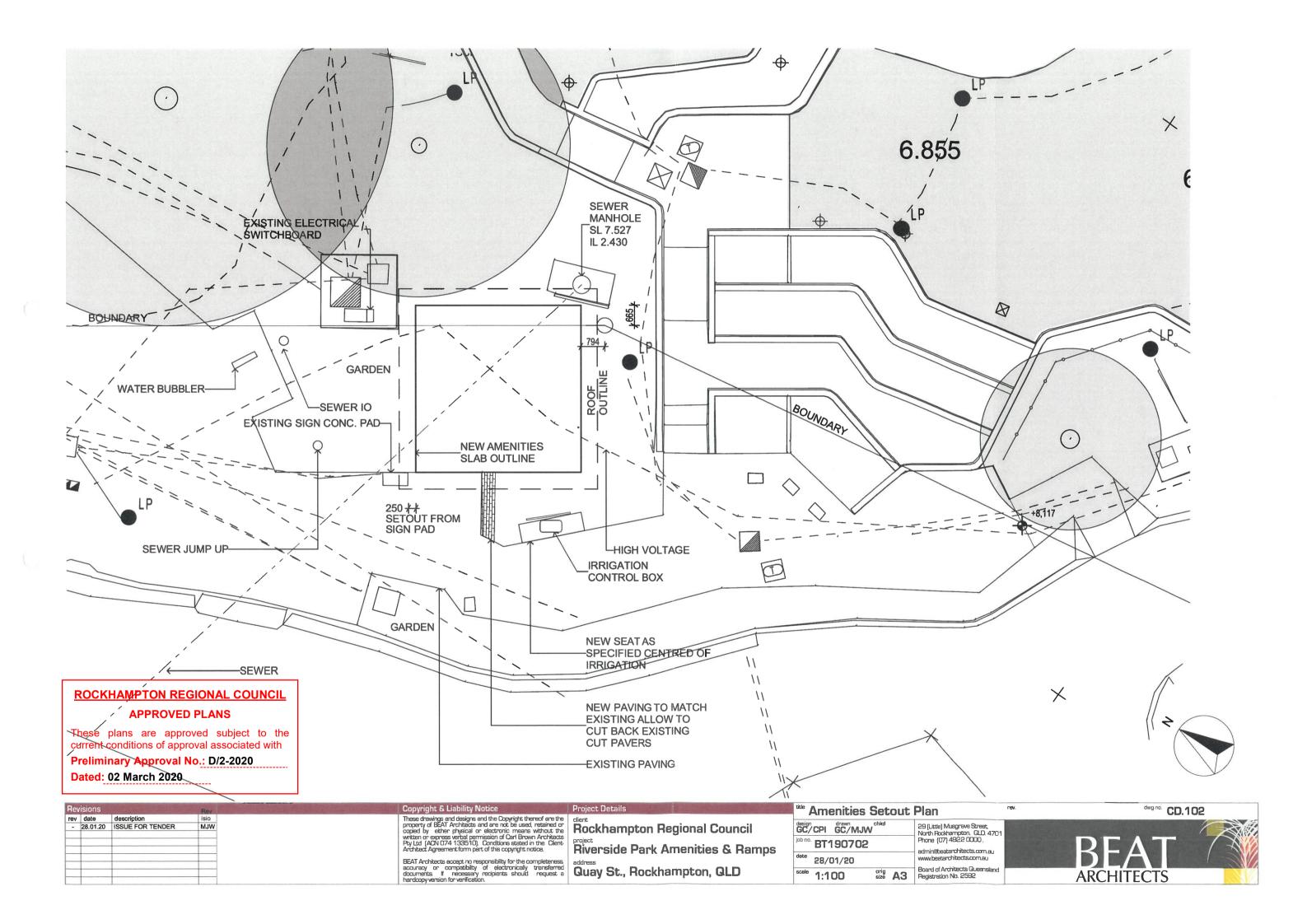
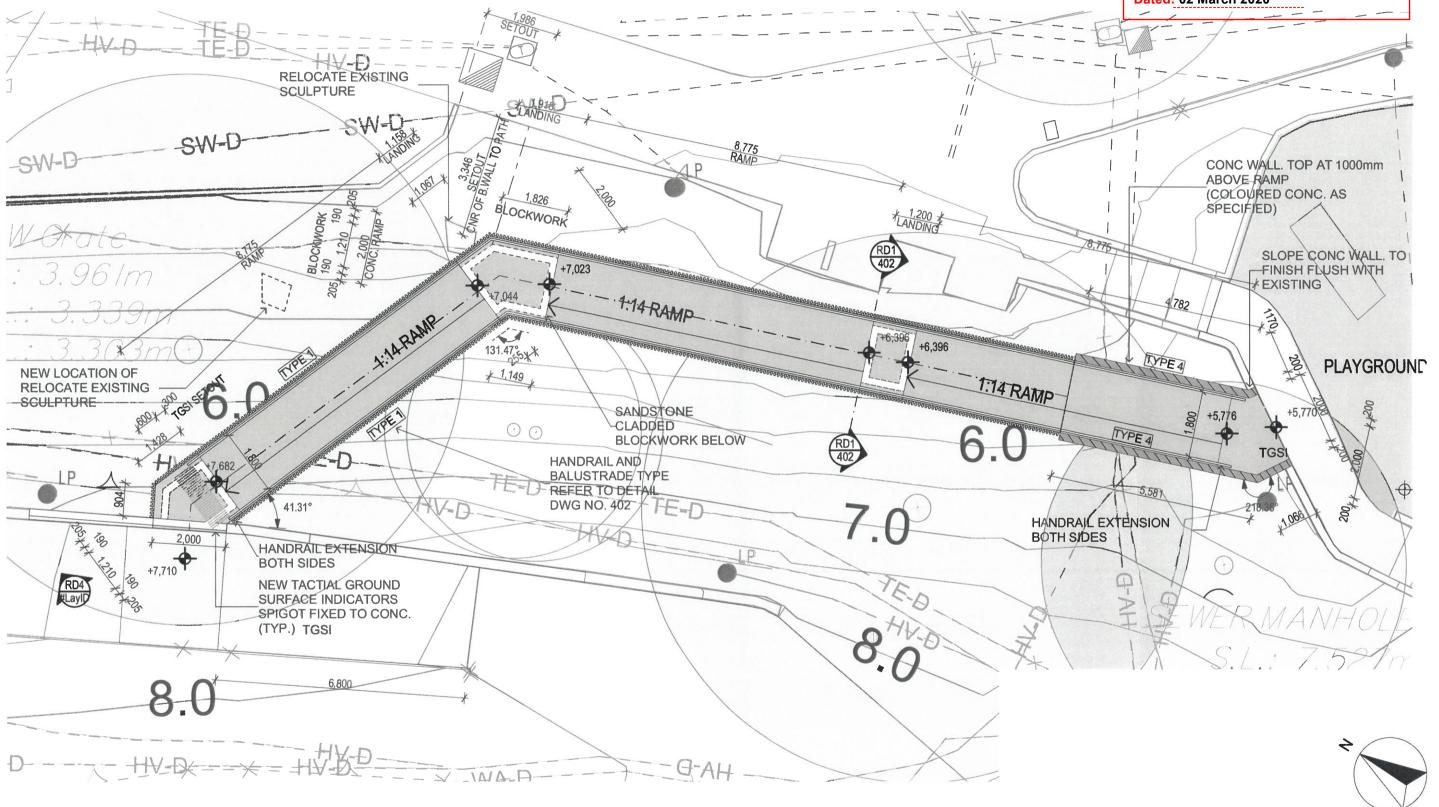
These plans are approved subject to the current conditions of approval associated with **Preliminary Approval No.: D/2-2020** Dated: 02 March 2020 ROY RIVER FITZROY RIVER 4.0 === PROPOSED NEW **NORTH RAMP CARPARK** 8.0 ----PROPOSED NEW XX RAMPING ROAD FROM CARPARK 7 SOUTH RAMP 8.0 **PROPOSED QUAY STREET NEW AMENITIES** SLAB EDGE (ROOF OUTLINE SHOWN DASHED) SEWER MANHOLE S.L: 8.633m LEGEND **QUAY STREET** CONTOUR LINE WITH ELEVATION RETAINING WALL FENCE BOTTOM OF BANK LIGHT POLE TOP OF BANK POWER POLE VALVE CHANGE OF GRADE STORMWATER LINE WATER METER SEWER LINE UNDERGROUND ELECTRICAL SEWER MANHOLE ELECTRICAL PIT SERVICE VALVE WATER METER WATER MAIN (GRADE D) TELSTRA PIT TELSTRA LINE (GRADE D) EDGE OF VEGETATION SITE PHOTO IRRIGATION CONTROL BOX STORMWATER MANHOLE SIGN EDGE OF BITUMEN BOLLARD SAIL SHADE POLE TREE ROOFWATER DISCHARGE EDGE OF CONCRETE CENTRELINE OF ROAD INSPECTION OUTLET SEWER JUMP UP Copyright & Liability Notice dwg no. CD.101 * Site Plan These drawings and designs and the Copyright thereof are the property of BEAT Architects and are not be used, retained or opped by either physical or electronic means without the written or express verbel permission of Carl Brown Architects Pty Ltd [ACN 074 133510]. Canditions stated in the Client-Architect Agreement form part of this copyright notice. date description 28.01.20 ISSUE FOR TENDER 29 (Little) Musgrave Street, North Rockhampton, GLD, 4701 Phone (07) 4922 0000, Rockhampton Regional Council GC/CPI GC/MJW chke BT190702 Riverside Park Amenities & Ramps admin@beatarchitects.com.au BEAT Architects accept no responsibility for the completeness accuracy or competibility of electronically transferred documents. If necessary recipients should request a hardcopy version for verification. 28/01/20 Quay St., Rockhampton, QLD orig size A3 Board of Architects Queensland Registration No. 2592 1:350

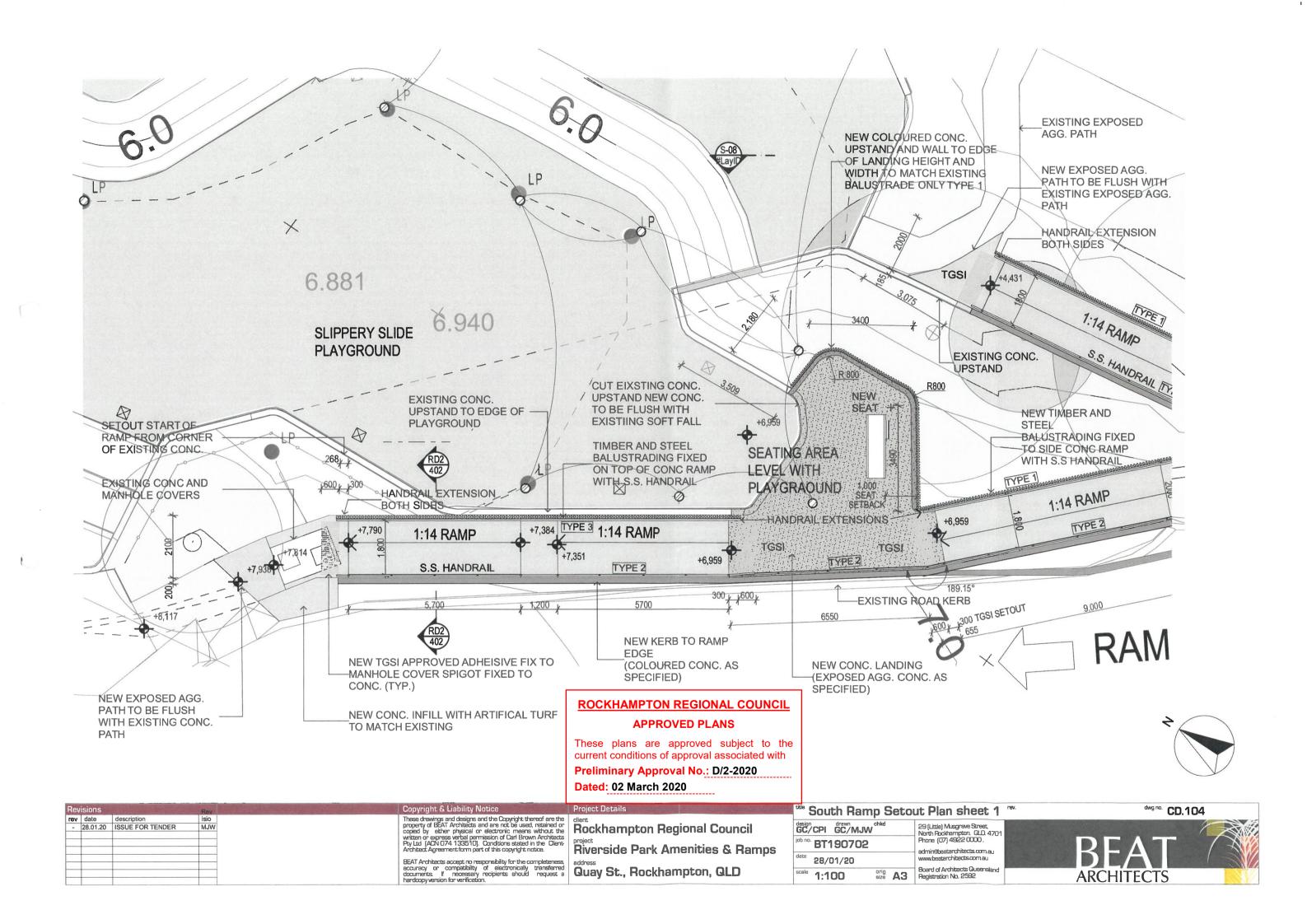
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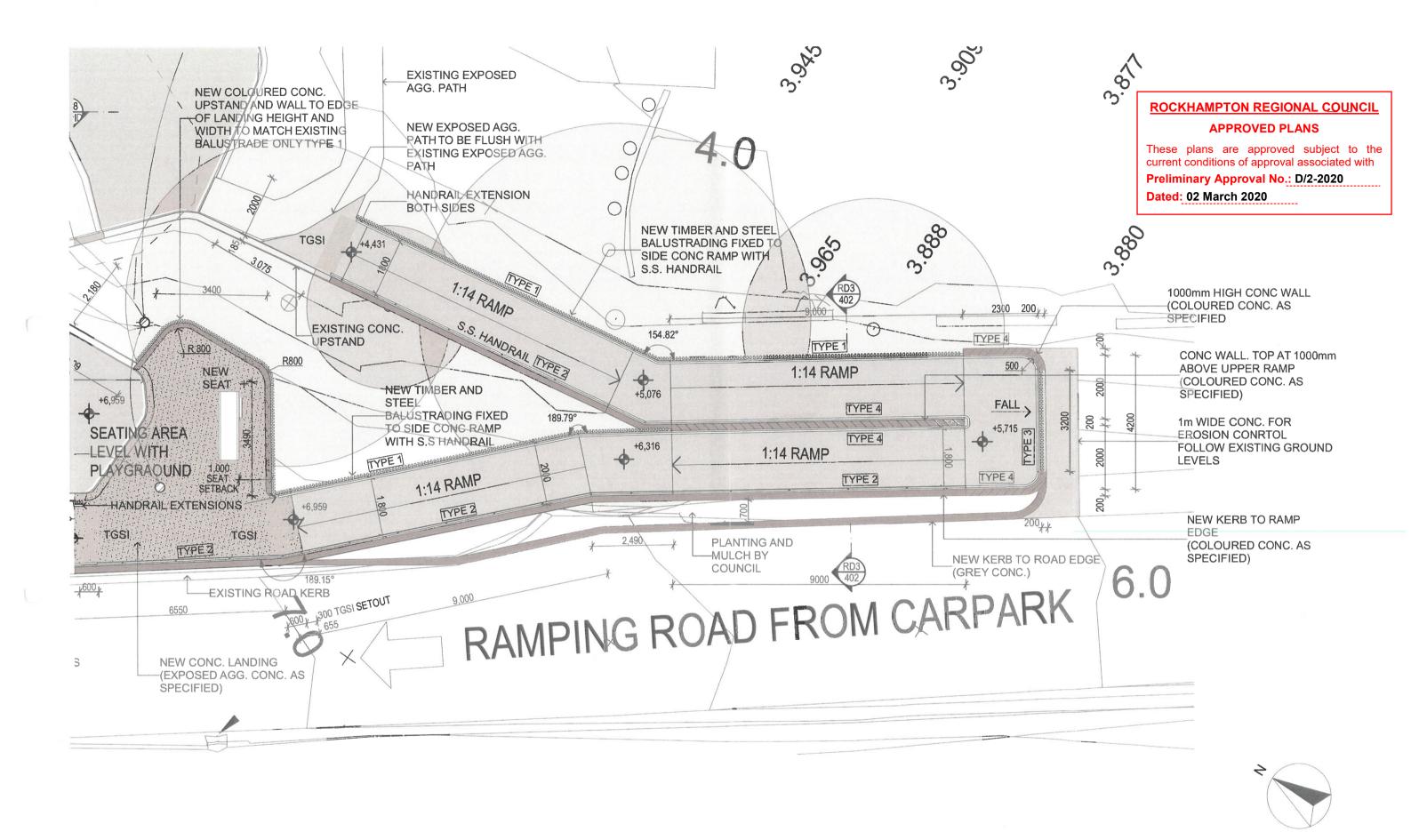




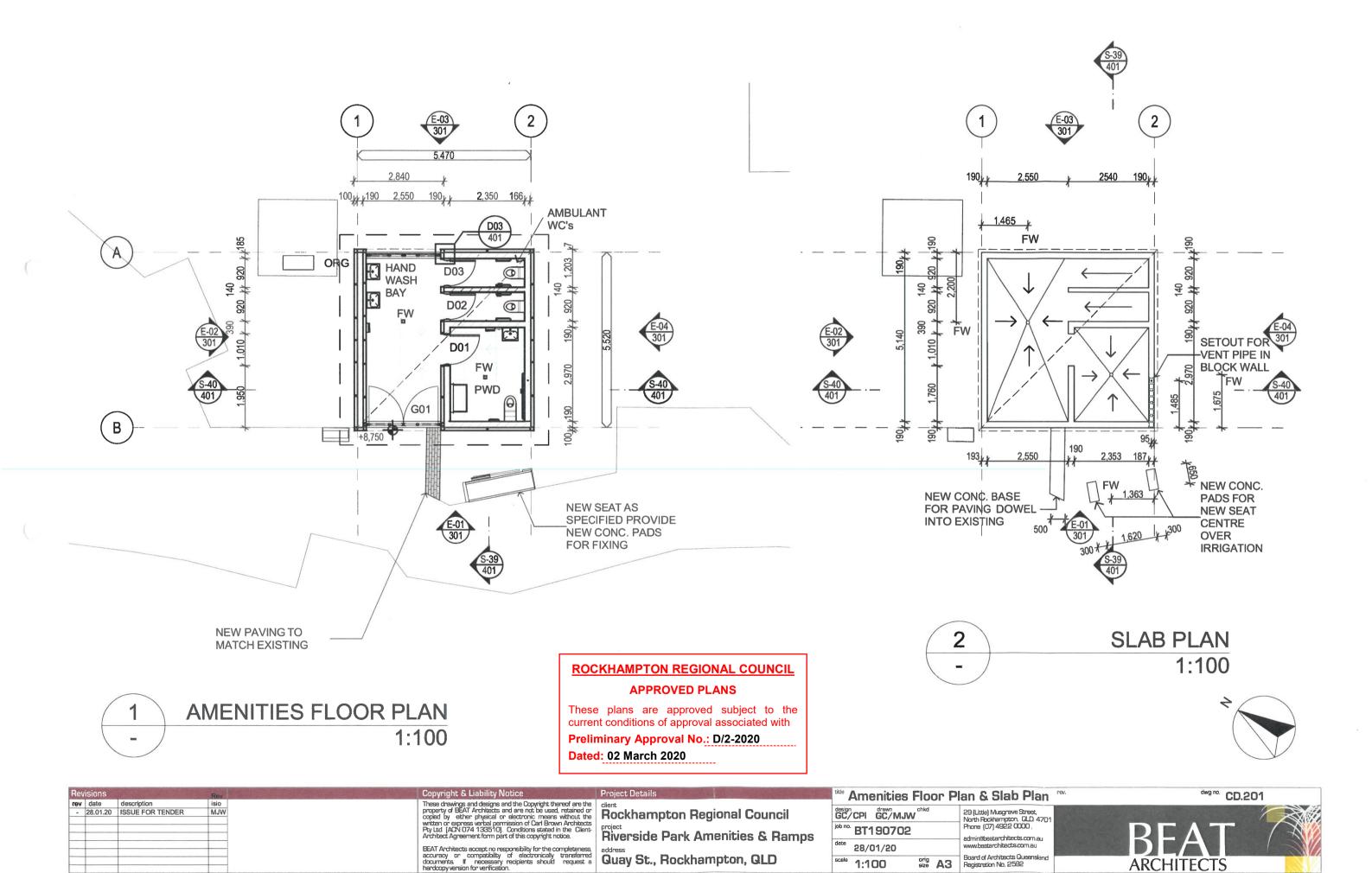


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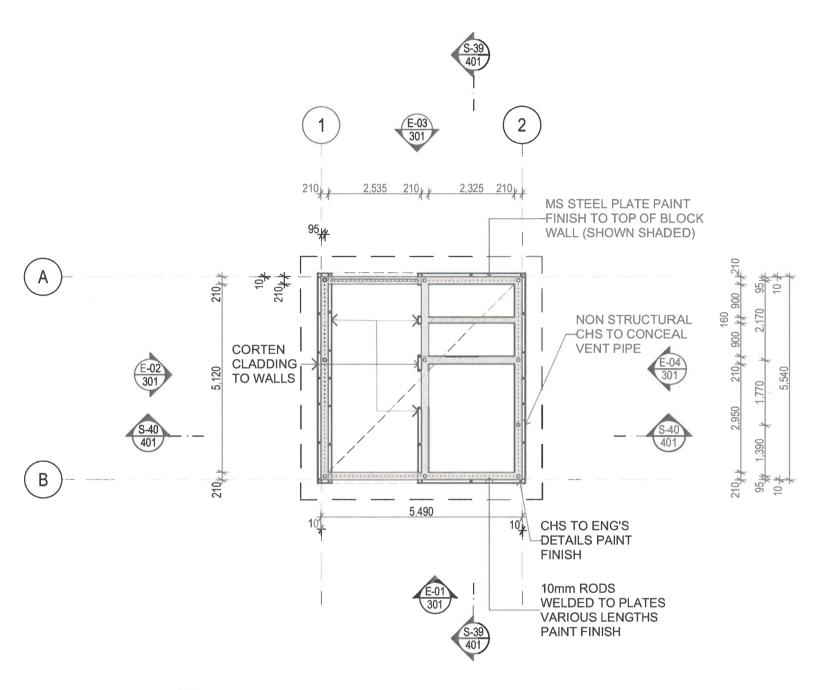


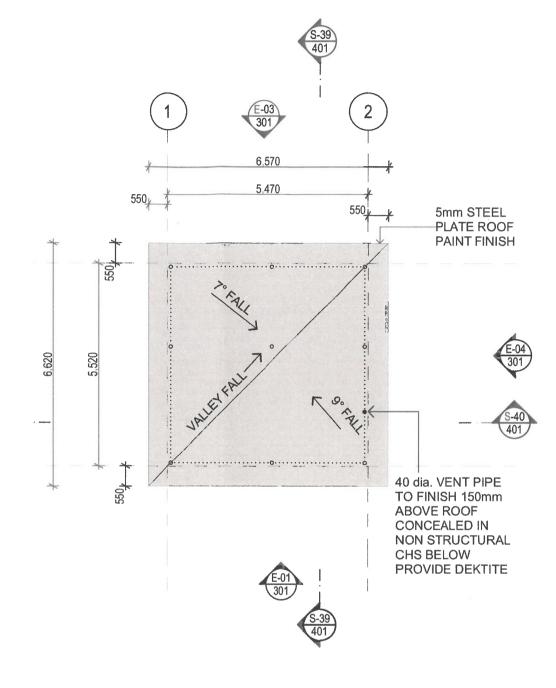
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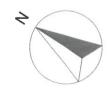
5. TOP OF BLOCK WALL PLAN
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6. ROOF PLAN 1:100

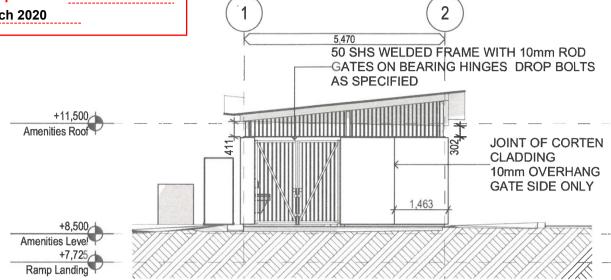


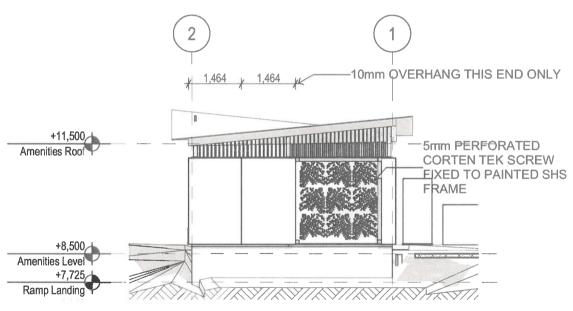
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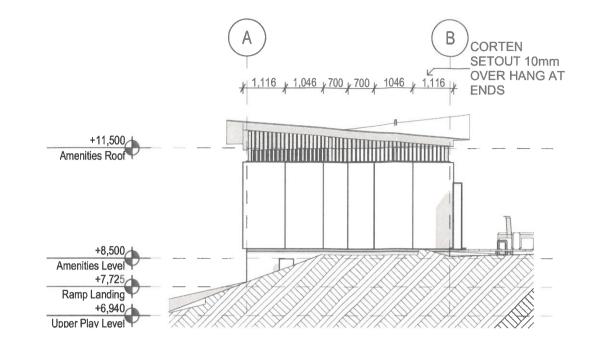




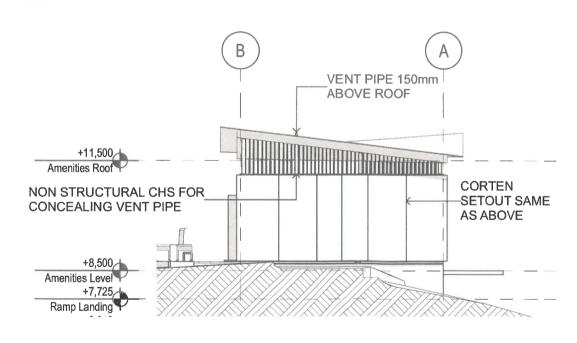
NORTH ELEVATION 1:100

SOUTH ELEVATION

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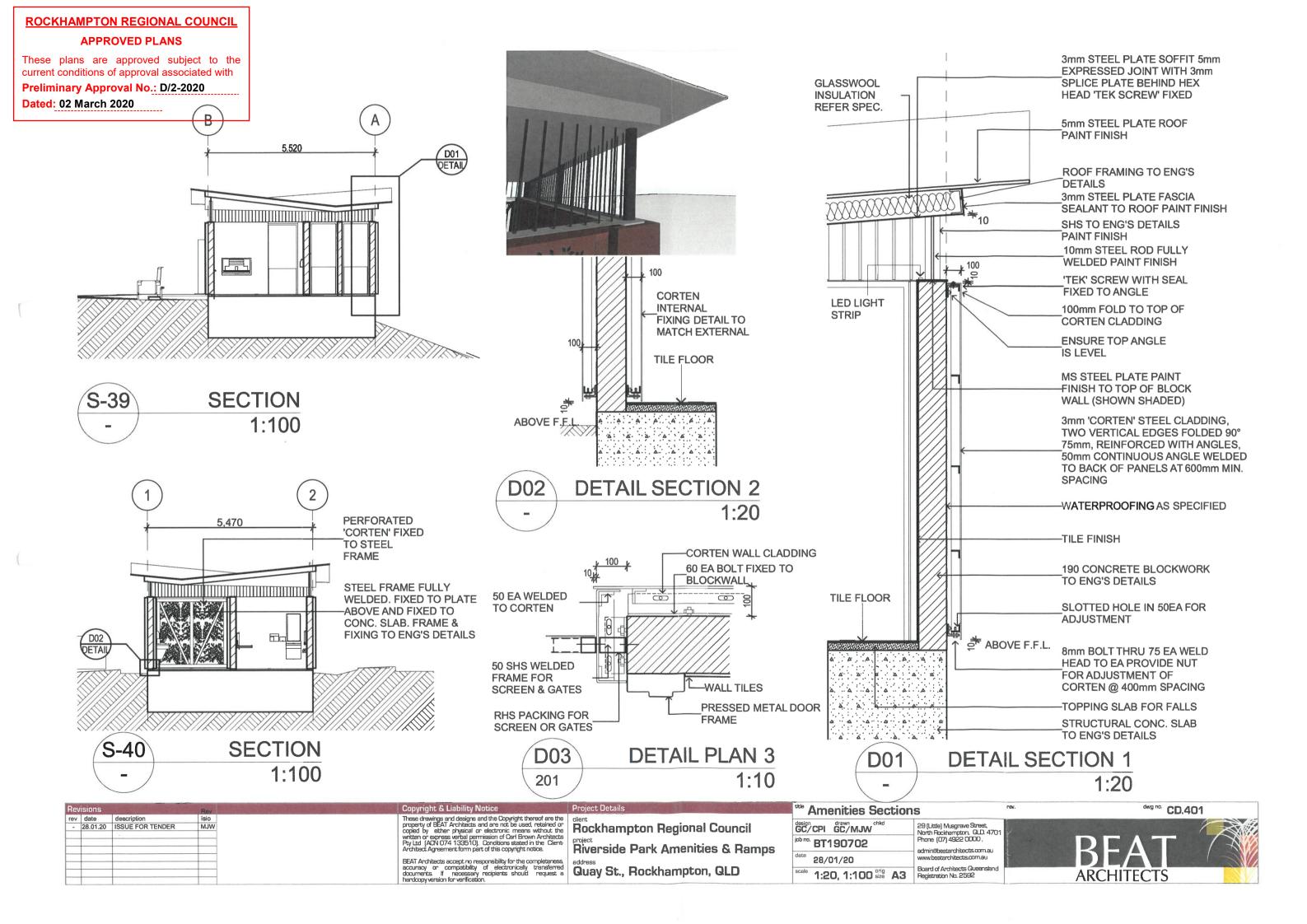


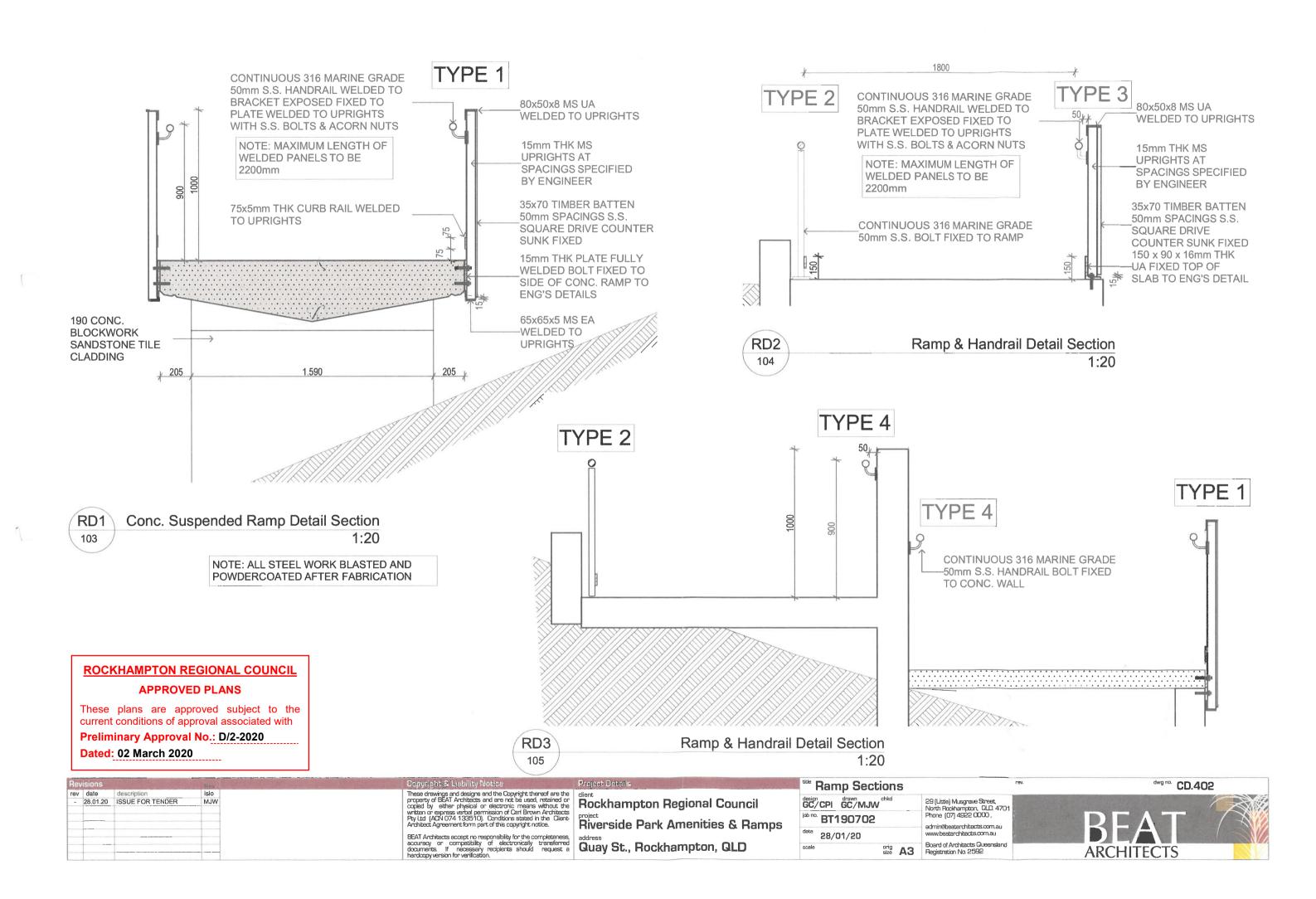


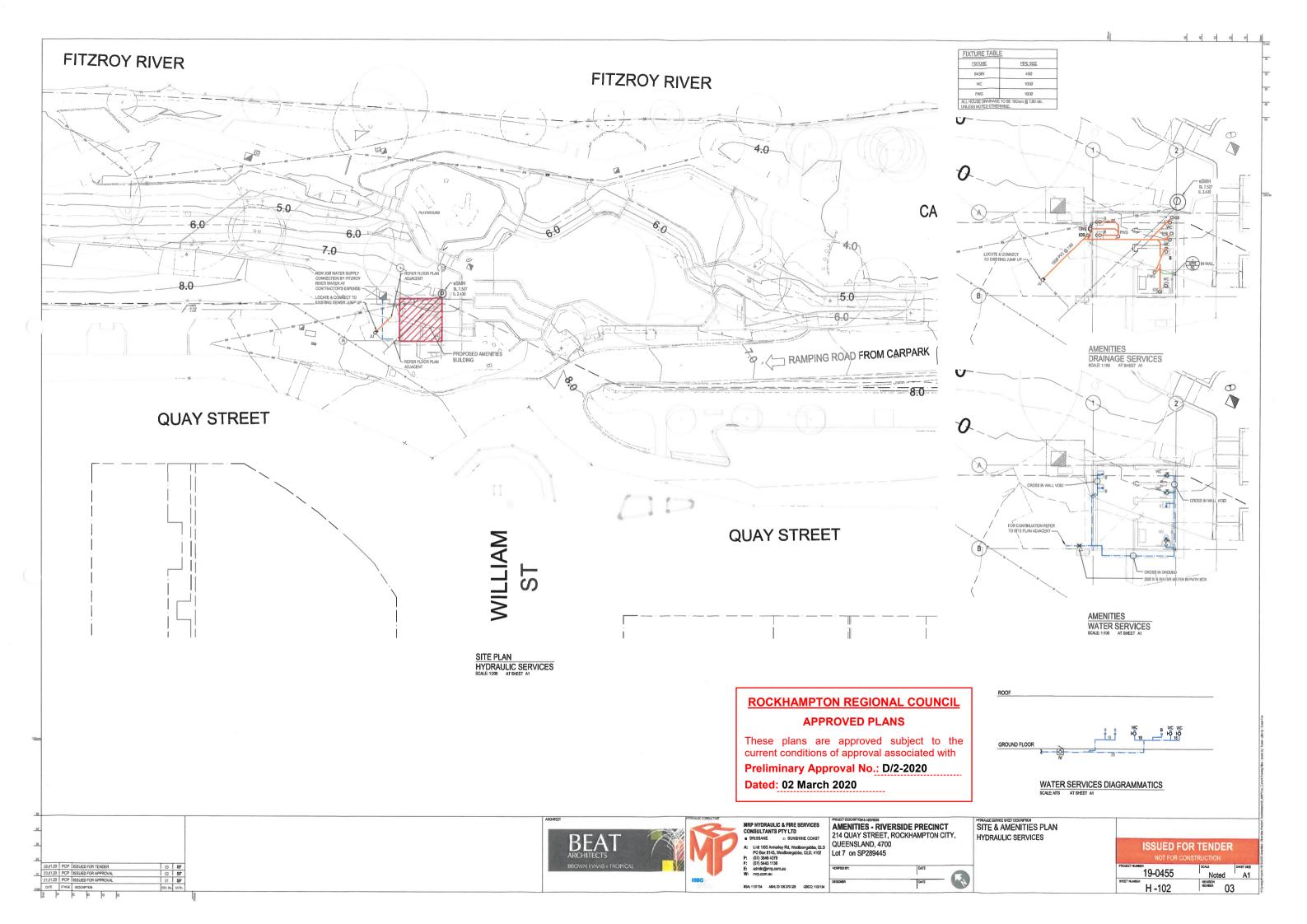


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ROCKHAMPTON REGIONAL COUNCIL

APPROVED PLANS

These plans are approved subject to the

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Preliminary Approval No.: D/2-2020

Dated: 02 March 2020

3 March 2016

Rockhampton Regional Council PO Box 1860 Rockhampton QLD 4700

Attention: Andrew Collins

Dear Andrew

Quay Street Riverbank Development - High Level Scour Assessment

The Quay Street Riverbank Development will consist of recreational, amenity and commercial uses including promenades, piers, gardens and building structures. As the proposed development borders the Fitzroy River, there is potential for flood and scour damage of the development during flood events in which the banks of the Fitzroy River are overtopped.

With reference to Table 1 and Chart 1 below, bank overtopping within the subject site may occur for flood levels greater than approximately 4.8 mAHD (6.25 mRGD, meters Rockhampton Gauge Datum = mAHD + 1.45m).

Following completion of the high level flood impact assessment for the development, the findings of which were delivered to Rockhampton Regional Council (RRC) via email on 25 January 2016, AECOM Australia Pty Ltd (AECOM) have been engaged to undertaken a high level scour assessment of the project.

1.0 Objective

The objective of this stage of the project is to undertake a high level, qualitative scour assessment to identify areas within the proposed development that could be at potential risk of scour during an out of bank flood event in the Fitzroy River. The scour assessment is limited to the overbank area only and does not include assessment of flood risk to buildings.

The investigation is to utilise RRCs existing TUFLOW model of the Fitzroy River which has been previously calibrated and deemed suitable for this high level investigation.

2.0 Data

Information collected and reviewed to inform this high level assessment includes the following:

- Development layout plans (Urbis December 2015, Woods Bagot January 2016).
- Maximum depth, water level and velocity results file from a TUFLOW hydraulic model of the Fitzroy River.

As noted above a dynamically linked one dimensional (1D) / two dimensional (2D) TUFLOW hydraulic model has previously been prepared for the Fitzroy River for the purposes of assessing flood risk. This model covers a large reach of the Fitzroy River and has a 25m grid resolution of the greater Rockhampton area (See Figure 1). The results therefore present a coarse representation of flood water velocity at the proposed development. This flood risk model has been calibrated, verified and undergone external peer review.

The model outputs have been analysed to identify indicative flow velocities in the flood water to enable a qualitative, high level assessment of the risk of potential scour of the proposed development during an overbank flooding event.

3.0 Model Results

The 1D/2D TUFLOW model has been simulated for a range of events, including the 39%, 18%, 10%, 5%, 2% and 1% Annual Exceedance Probability (AEP) design storm events for the pre-development scenario. The model has also been simulated for the 1% AEP design storm event with a broad scale representation of the proposed Quay Street Riverbank Development within the model. A presentation of the post-development peak flood velocity and peak flood elevation for the 1% AEP design event is presented in Figure 2 and Figure 3 respectively. These figures also present the general layout of the development.

The model outputs of velocity, depth and elevation are provided in Table 1, at a location within the development area that is 100m upstream of the proposed building on Denham Street. This location has been selected as the results are representative though the whole development area.



Table 1 Model Results at one Representative Location

Model Scenario	Peak Velocity * (m/s)	Peak Depth (m)	Peak Water Level (mAHD)	Equivalent Gauge Level (mRGD) **
Pre-development 39% AEP	0.00	0.00	3.06	4.48
Pre-development 18% AEP	0.56	2.58	6.07	7.42
Pre- development 10% AEP	0.87	3.47	6.96	8.27
Pre- development 5% AEP	1.01	4.09	7.58	8.92
Pre- development 2% AEP	1.05	4.40	7.89	9.25
Pre- development 1% AEP	1.09	4.68	8.17	9.56
Post- development 1% AEP	1.01	4.69	8.18	9.56

^{*} Peak velocities shown are depth averaged velocities extracted from the 2D model and may not represent the actual peak velocity within the water column.

The results in Table 1 suggest that there is negligible change in the flood characteristics of the 1% AEP event due to the development. It also indicates that although there is a difference in flood water depth / level for the design events from 5% AEP through to 1% AEP, there is only minor difference in the maximum flood velocities.

Frequency of Inundation

The proposed development has an elevation of between 4.8 mAHD and 8.0 mAHD (6.25 mRGD to 9.45 mRGD). The peak flood elevations for the events have been plotted in Chart 1. This indicates that parts of the development have less than a 25% AEP flood immunity.

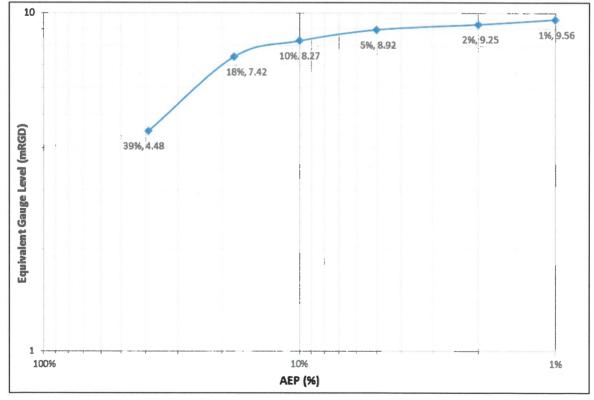


Chart 1 Peak Flood Elevation - Rockhampton Flood Gauge

^{**} mRGD = meters Rockhampton Gauge Datum (mAHD + 1.45m), represents the equivalent peak Rockhampton flood gauge level for the AEP event. The Rockhampton flood gauge is located at the eastern end of Derby Street, approximately 300m south of the subject site.



4.0 **High Level Scour Assessment**

The model grid resolution is 25m and the development site is approximately 30m wide. There is not sufficient resolution in the model grid to determine the flow paths through the site. Due to this, the velocities modelled through the site may be significantly over or underestimated as local changes in topography across the site and obstructions to flow have not been represented in detail. To determine detailed velocity calculations throughout the site, would require a finer (1m or less) grid resolution model representing the proposed development topography.

In the absence of detailed velocity data an assessment of potential locations of scour risk at the site have been identified in Table 2. The potential locations that may be subjected to scour have been mapped and presented in Figure 4.

Table 2 Potential Areas subject to Scour

Development Feature	Potential Scour Mechanisms	Comment on Quay Street Riverbank Development Scour Potential			
Pier Structures	A scour hole can occur immediately upstream and / or downstream of pier type structures due to accelerated flows, with the material being deposited immediately downstream of the pier.	All piers proposed for the project will utilise existing pier locations. It is noted that these existing piers have experienced multiple flood events with no documented scour issues. It is considered that the scour risk is therefore low.			
Wide Obstructions (walls/buildings)	Flow will be directed around wide obstructions. This may increase localised changes in velocity and cause eddies downstream, increasing the scour potential.	There are wide obstructions proposed within the Riverbank Development which may result in localised increases in velocity and downstream eddies. The risk of scour is however considered low as observed during previous flood events. The existing areas of wide obstructions did not result in increased scour in the vicinity or downstream of the obstruction.			
Interface between structures / pavement and non- paved	The higher strength paved areas and structures can focus energy to the adjacent non-paved area and potentially cause undermining of the pavement.	The existing ground conditions have a number of transitions between concrete and grassed areas, which have not previously been observed to experience scour during flood events. The risk is therefore considered low under the proposed development.			
Steep change in topography	Large changes in elevation such as at walls, or steps can cause a sudden change in the flow pattern and velocity. This can cause eddies and increased scour potential.	The existing steep changes in grade do not show evidence of increased scour potential during previous flood events. Again the risk of scour is considered low under the proposed development.			
Grassed areas	Grassed areas can form a protective barrier for the underlying soils. However, damage to the grass can expose the underlying soil and potentially lead to scour.	Due to the relatively low peak velocities predicted in the development area, the risk of damage to established grass areas is considered low. This is evidenced by previous overbank flooding of the area which did not result in damage to established grass areas.			
Mulched garden bed	The mulch within garden beds is at risk of floatation and removal at low velocities.	Observations following previous overbank flooding have shown that garden bed areas are at a high risk of removal due to floatation of mulch and other light materials.			

Final recommendations on treatments have not provided at this stage of the project, due to the three dimensional (3D) design of the proposed works not being available. As noted above, the current model resolution also limits a detailed assessment of scour potential.



5.0 Conclusion and Recommendations

The high level scour assessment has identified a number of areas within the Quay Street Riverbank Development which have the potential for increased scour risk. The summary provided in Table 2 and graphically on Figure 4 identifies these areas and the reason for the potential scour risk.

As noted above at the time of completion of this high level scour assessment, the 3D design was not complete and detailed ground surface levels of the proposed development were not available. It is therefore recommended that this assessment be reviewed once the 3D design is complete.

It is further recommended that the designers take this high level assessment into account and, if deemed necessary, consider undertaking a more detailed scour assessment using a finer model resolution.

Other General Comments

During our review of the proposed development design plans, we note the following general comments related to our extensive experience with Fitzroy River flooding within the study area:

- New infrastructure should be designed for easy clean down, as this area is susceptible to deposits of silt and debris once flood waters recede.
- All new structures will need to be designed for hydrodynamic loading as per the relevant standard, taking into particular account loads imposed by uplift and debris loading.
- Any below ground structures (e.g. pump stations, lifts etc) should be assessed and designed for buoyancy forces that may be imposed during Fitzroy River flood events, where the overbank area is submerged.

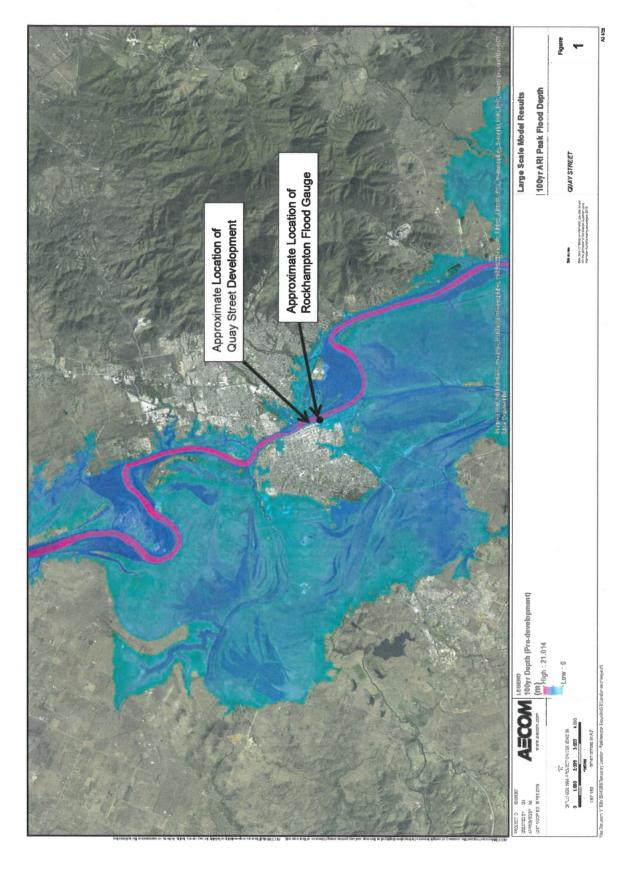
Yours faithfully for AECOM Australia Pty Ltd

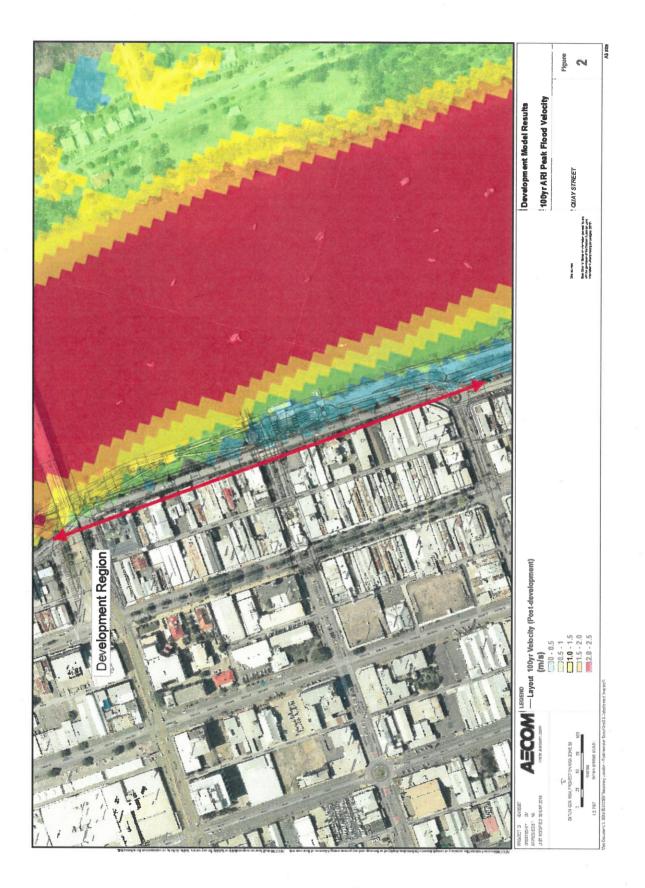
Ben McMaster

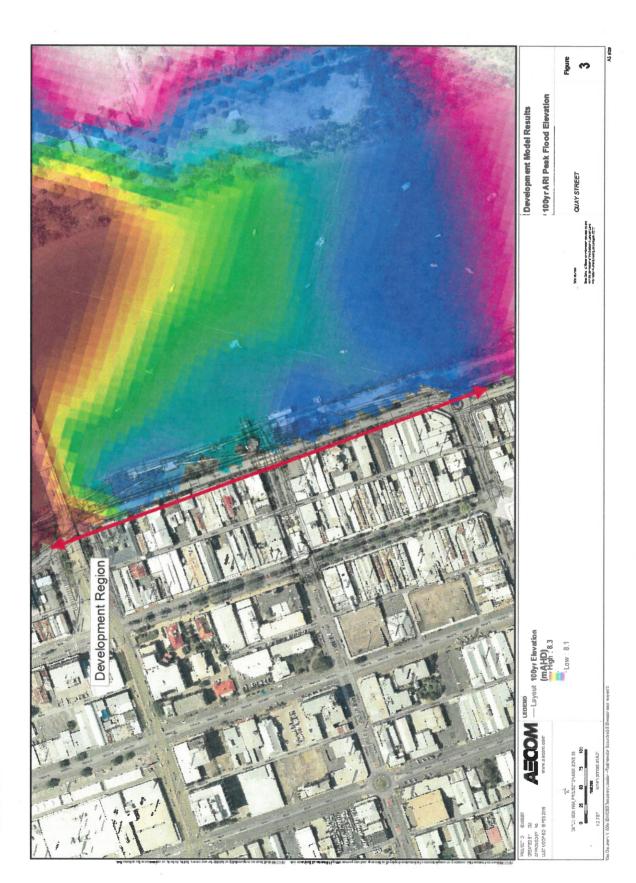
Rockhampton Office Manager ben.mcmaster@aecom.com

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From:

Corbett, Richard < Richard.Corbett@aecom.com>

Sent:

Monday, 25 January 2016 6:48 PM

To:

Andrew Collins

Cc:

Robert Holmes; Maree Anderson; Angus Russell; McMaster, Ben

Subject:

Quay Street Riverbank Development - Results of High Level Flood Impact

Assessment

Attachments:

image002.emz; image015.emz; RL5-16.pdf

Andrew,

Hi, how are you? Hope you had a pleasant weekend.

The TUFLOW modelling for **Stage 1 – Project Setup and Initial High Level Flood Impact Assessment** is now complete.

The recently updated Yeppen South As-Constructed TUFLOW model was used as the Basecase for this assessment. The following changes were implemented to create the Developed Case:

☐. 2 x 25m grid cells raised to 99m (glass wall), over the Saigon Saigon structure.

□. 1 x 25m grid cell raised by 1m over the wet play area (as per design plans provided).

☐. Centreline along Quay Street updated using design levels provided.

Note that the stairs to the north-west of Saigon Saigon were not altered, due to their sub-grid scale size.

The results show minimal difference in Peak Water Surface Elevations (PWSE) for the 1% AEP event (refer image below).

There is a slight increase upstream of Saigon Saigon, of ~0.01m, accompanied by a maximum ~0.03m decrease downstream.

The green area depicts a grid cell that 'was wet and is now dry'.

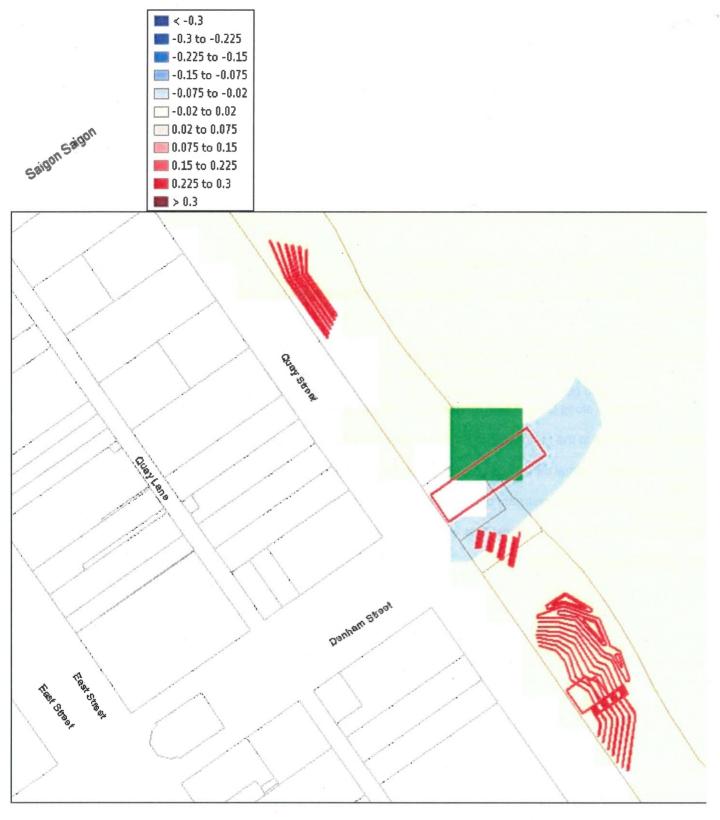
1% AEP Difference in PWSE

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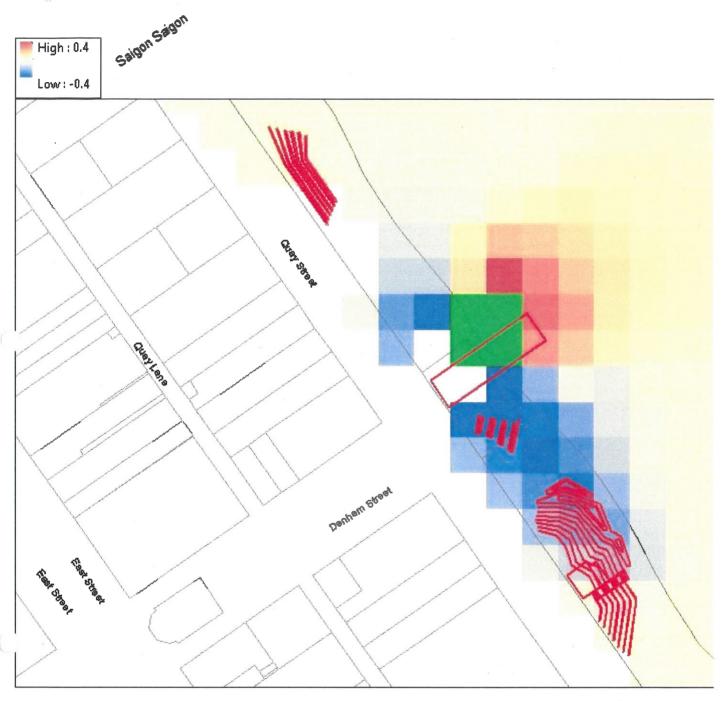
Dated: 02 March 2020



The maximum increase in velocity is \sim 0.4m/s adjacent to the Saigon Saigon structure, which raises the depth averaged peak velocity to \sim 1.65m/s.

The difference in Peak Velocity is shown in the image below.

1% AEP Difference in Peak Velocity



As the Stage 1 assessment has predicted minimal impact, AECOM recommends that there is no need to undertake **Stage 2a – Detailed Flood Impact Assessment**.

Note that our final QA is in progress and this recommendation will be confirmed on Wednesday.

We will also be in contact later in the week to discuss the requirements for Stage 2b – Scour Assessment and Advice.

Let me know if you require any further information regarding the Stage 1 assessment.

Regards

Richard Corbett

Senior Civil Engineer
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Richard.Corbett@aecom.com

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