

#### **ROCKHAMPTON REGIONAL COUNCIL**

#### **APPROVED PLANS**

These plans are approved subject to the current conditions of approval associated with

Development Permit No.: D/182-2023

Dated: 19 April 2024

# Technical Memorandum

То:	From
Sophie Muggeridge Planning Officer Rockhampton Regional Council general.enquiries@rrc.qld.gov.au	Chris Hewitt Associate Director/Principal Traffic Engineer RPEQ 05141 McMurtrie Consulting Engineers chris@mcmengineers.com

### 1 RRC Request for Information Response

The following responses are provided to the nominated items of the Request for Information.

#### Item 2.1

**Request**: The traffic generation rates for the proposed use appears to be under-estimated given the observations made for similar uses within Rockhampton. It is acknowledged that there is little information on the traffic generation for a drive-through coffee shop within Australian-based resource materials however it would be prudent to carry out surveys on existing similar uses to provide some certainty to the rates provided.

Given the traffic impacts other drive-through coffee shops in Rockhampton have had, please provide further justification as to how the traffic generation rates provided are appropriate for the use. This may require peak hour surveys of existing similar uses for comparison and revision of the SIDRA analysis as necessary.

**Response:** Reference is made to Bitzios *Trip Generation Drive Through Coffee Outlets Data and Analysis Report with Appendices*, which provides recommended traffic generation rates for drive through coffee shops based on surveys conducted at a number of sites across NSW. In accordance with the recommended range of 70-130 trips in the AM peak hour, and with consideration that the proposed use is in a regional area, a revised traffic generation rate in the AM peak hour of 70 trips/hr has been adopted. Based on the surveyed PM peak hour generation rate being on average ~25% of the AM peak hour generation rate, a conservative 35 trips/hr in the PM peak has been adopted, which represents 50% of the AM peak rate.

PROJECT: Zarraffa's Gracemere

DATE: 15/02/24 OUR REF: R002-23-24/009

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#### Item 2.2

**Request:** The 2018 traffic survey figures used to inform the Traffic Impact Assessment do not appear to have considered the recently constructed Child Care Centre opposite the subject site, or the recently approved take away restaurant adjacent to the site. As such, Council has concerns that the background traffic volumes have been underestimated for the purposes of the analysis.

Please confirm whether the traffic generation associated with these sites have been considered within the SIDRA analysis and amend the Traffic Impact Assessment where necessary.

**Response:** The traffic generated by the proposed Hungry Jacks facility, in accordance with the approved GFA and traffic generation rate (Approval Reference D48-2022) has been applied to the revised Traffic Impact Assessment – refer to the Revision B Traffic Impact Assessment. It is noted that the Child Care Centre adjacent the site has been operational since at least 7 April 2017 (refer to Figure 1), and the intersection counts were carried out on 22 March 2018. Therefore, it is seen that the traffic generated by the Child Care Centre has already been included in the intersection counts used for the assessment.



Figure 1 – 7 April 2017 Aerial Imagery (Source: QLD Globe)

#### Item 2.3

**Request**: It is noted that the average delay for the 2024 PM post development scenario for the John Street leg is slightly less than that of the pre-development scenario, for the same cycle time.

Please advise how this been achieved?

**Response:** The change noted is due to the redistribution of traffic on the intersection as a result of the drop in trip assumptions and does not represent a tangible change to the performance of the intersection.

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### 2 TMR Request for Information Response

The following responses are provided to the nominated items of the Request for Information.

#### Item 1

**Request**: The following issues were identified with the Traffic Impact Assessment (TIA) prepared by McMurtrie Consulting Engineers, dated 15 December 2023, reference R002-23-24/012:

- (a) SARA considers the figure of 45 trips per hour to below the traffic generation rates for similar drive thru facilities across the Rockhampton region. In lieu of this, Rockhampton and surrounding townships are currently experiencing a number of traffic concerns from similar drive thru facilities. In particular, the constant queue spill-over out of premises from drive thru facilities that compromise the safety and operational efficiency of the surrounding road network.
- (b) The TIA has not considered the cumulative traffic impacts resulting from the approved Hungry Jack's (located on the balance of the subject site) and the Child Care Centre across the road, and how this may impact the safety and efficiency of the Lawrie Street / John Street intersection.

Please provide an amended TIA which addresses the following matters:

- a) undertake a traffic survey on a similar drive thru facility (for example, the existing Zarraffa's drive thru Coffee Shop located on Musgrave Street, Berserker and/or the Gus's drive thru Coffee Shop on Homemaker Drive, Yeppoon) and provide updated traffic generation rates reflecting the results of this traffic survey.
- b) provide an assessment of the cumulative traffic impacts from the proposed development which considers traffic generated from the approved Hungry Jack's facility and the Child Care Centre located across the road and how this impacts the safety and operational efficiency of the Lawrie Street / John Street intersection.

#### Response:

- (a) Both the existing Zarraffa's on Musgrave Street and the Gus's Coffee on Homemaker Drive are sites with known issues stemming from a lack of queue length (~21m and ~13m respectively, measured from the order point to the nearest conflict point). The proposed development will provide approximately 43m of queue length, which is a significant improvement on both sites recommended to complete a survey upon. It is seen that surveying a site with known issues would provide a skewed traffic generation rate. In lieu of this, reference is made to Bitzios *Trip Generation Drive Through Coffee Outlets Data and Analysis Report with Appendices*, which provides recommended traffic generation rates for drive through coffee shops based on surveys conducted at a number of sites across NSW. In accordance with the recommended range of 70-130 trips in the AM peak hour, and with consideration that the proposed use is in a regional area, a revised traffic generation rate in the AM peak hour of 70 trips/hr has been adopted. Based on the surveyed PM peak hour generation rate being on average ~25% of the AM peak hour generation rate, a conservative 35 trips/hr in the PM peak has been adopted, which represents 50% of the AM peak rate.
- (b) The traffic generated by the proposed Hungry Jacks facility, in accordance with the approved GFA and traffic generation rate (Approval Reference D48-2022) has been applied to the revised Traffic Impact Assessment refer to the updated Revision B Traffic Impact Assessment. It is noted that the Child Care Centre adjacent the site has been operational since at least 7 April 2017 (refer to Figure 1), and the intersection counts were carried out on 22 March 2018. Therefore, it is seen that the traffic generated by the Child Care Centre has already been included in the intersection counts used for the assessment.





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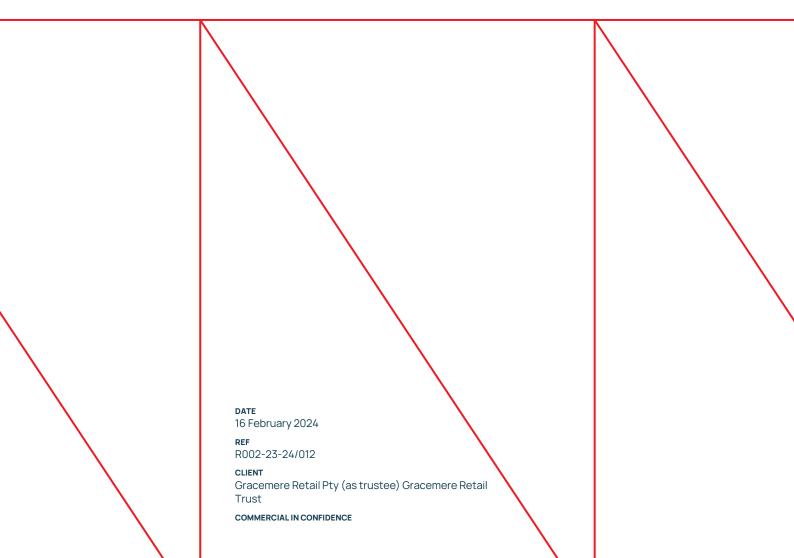
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# Zarraffas Drive Through at 6 Lawrie St, Gracemere 4702 (Lot 604 on R2642)

Traffic Impact Assessment



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Document Information				
Prepared for Gracemere Retail Pty (as trustee) Gracemere Retail Trust				
Document Name	Traffic Impact Assessment			
Job Reference	R002-23-24/012			
Revision	В			

Document History							
Revision	Date	Description of Revision	Prepared		Approved by		
			by	Name	Signature	RPEQ No	
А	15/12/2023	Original Issue	R. Crouch	L. McMurtrie	LWHA.	15243	
В	16/02/2024	RFI Response	R. Crouch	C. Hewitt	aff:#	05141	

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## **Appendices**

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Appendix B: Turning Movement Forecasts

Appendix C: Intersection Analysis
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### 1 Introduction

### 1.1 Project Background

Gracemere Retail Pty (as trustee) Gracemere Retail Trust are proposing to establish a Zarraffas Coffee Drive Through at 6 Lawrie St, Gracemere 4702, on land described as Lot 604 on R2642. The drive through is expected to cater for south-east bound passing traffic on the adjacent section of Lawrie St, with site access being located on John St and providing parking facilities for light vehicles.

The site is subject to a previous approval (D/48-2022), which allowed for various Food and Drink outlets on the site, namely a Hungry Jacks drive through.

#### 1.2 Scope and Study Area

McMurtrie Consulting Engineers (MCE) have been commissioned by Gracemere Retail Pty (as trustee) for Gracemere Retail Trust to undertake a Traffic Impact Assessment (TIA) for the proposed Coffee Drive Through.

This Traffic Impact Assessment (TIA) was carried out to determine the level of potential impacts of the project on the operation of the surrounding road network. The outcomes of the TIA will be used in support of the Development Application which will be assessed by Department of Transport and Main Roads (TMR) and Rockhampton Regional Council (RRC)

The assessment methodology adopted for this TIA is summarised in the key tasks listed below.

- Broadly identify the existing transport infrastructure which is of relevance to the project.
- Estimate traffic generation associated with the project and the distribution of this development traffic on the identified road network.
- Assess the potential impact of the project on the surrounding transport infrastructure.
- Identify potential mitigation and management strategies to be implemented to offset the impact of the proposed project (if required).

The process allows for the assessment of the traffic impacts of the project in terms of road safety, access requirements, road link capacity and other transport infrastructure. Following this, if required, potential mitigation and/or management measures would be formulated to address the potential traffic impacts caused by the proposed Project.

#### 1.2.1 Study Area

As previously identified, the proposed Zarraffas Coffee Drive Through is proposed to be located at 6 Lawrie St, Gracemere 4702, on land described as Lot 604 on R2642. The site is located along John St near the intersection with Lawrie St

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DATE: 16/02/24 OUR REF: R002-23-24/012

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### 2 Existing Conditions

### 2.1 Surrounding Road Network Links

#### **Lawrie Street**

Lawrie Street links the intersection of Mclaughlin St and Old Capricorn Highway with Gavial Gracemere Road in Gracemere, Queensland. Lawrie Street intersects with John Street at a four-way intersection, with Russell Street comprising the opposing approach. This intersection was previously a roundabout but has been updated to a signalised intersection by the Department of Transport and Main Roads in approximately 2023.

#### John Street

John St is typically a two-way, one lane road with an (unposted) speed limit of 50km/h, generally with direct access to properties fronting the route. The northbound and southbound lanes along John St were unseparated, allowing vehicles to pass and turn into the opposite lane.

Adjacent the proposed development site, the speed limit is 50km/hr, and the road is currently classified as a Major Urban Collector.

Access to John Street for the proposed development will be from the northbound direction as indicated in Figure 1 below and will be left & right in/out only given the undivided nature of John St. Refer to Appendix A for the development layout plan.



Figure 1 - Study area - 6 Lawrie St, Gracemere QLD

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#### 2.2 Traffic Volumes

#### 2.2.1 Road Link Volumes

The traffic volumes for the relevant section of road network were established from turning movement surveys, referenced from the existing approval (D/48-2022), for Lawrie/John/Russell St intersection from 6:00am to 6:00pm on Thursday, 22 March 2018. Relevant data for the peak periods of the assessed intersection are shown below in Table 1. Which the calculated volumes representative of all the vehicular movements throughout the intersection during the peak hour periods.

Table 1: Intersection Attributes

Attribute	Morning Peak (Weekday)	Evening Peak (Weekday)	
Peak Hour	8:00am - 9:00am	3:00pm - 4:00pm	
Volume (VPH)	1610	1710	
% HV	2.20%	4.20%	
Peak Flow Factor	100%	100%	

#### 2.3 Intersection Operations

#### 2.3.1 Intersection Parameters

Due to the development's proximity to the Lawrie/John/Russell Street signalised intersection a series of SIDRA analyses were conducted to quantify the current traffic conditions. The analysis was based on the traffic count data, as obtained from the existing approval (D/48-2022), with the attributes determined in Table 1 and appropriate as-constructed signal phasing/cycle times.

The results are displayed as Degree of Saturation (DOS), 95<sup>th</sup> percentile vehicle queues and the Critical Movement at the designed intersection. DOS for movement is specified as the ratio of traffic demand to the capacity of movement. Also, Critical Movement correlates to the approach or movement with the greatest Degree of Saturation. The Operational Rating and Level of Service (LOS) for all intersection types can be seen in Table 2 below.

Table 2: SIDRA Intersection Ratings

Level of Service (LOS)	Signalised	Roundabout	Priority
LOS A	x ≤ 60%	x ≤ 60%	x ≤ 60%
LOS B	60% < x ≤ 70%	60% < x ≤ 70%	60% < x ≤ 70%
LOS C	70% < x ≤ 90%	70% < x ≤ 85%	70% < x ≤ 80%
LOS D	90% < x ≤ 95%	85% < x ≤ 95%	80% < x ≤ 90%
LOS E	95% < x ≤ 100%	95% < x ≤ 100%	90% < x ≤ 100%
LOS F	100% < x	100% < x	100% < x

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#### 2.3.2 SIDRA Layout and Results

The adopted signalised intersection SIDRA layout for the Lawrie/John/Russell St intersection is shown in Figure 2

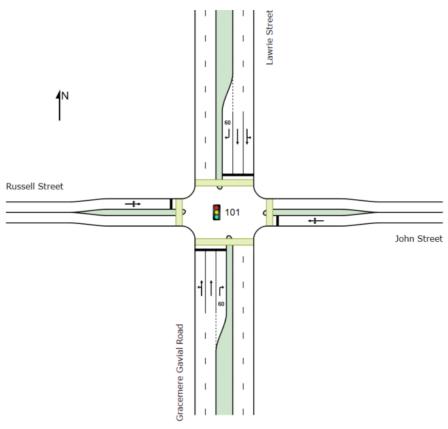


Figure 2: Lawrie/John/Russell Street Intersection

The results from SIDRA for the Lawrie/John/Russell St intersection analysis are summarised in Table 3 and Appendix C. From the acquired results the intersection displays a LOS C operations with the current weekday morning/evening peak hour specifications.

Table 3: Lawrie/John/Russell Street Intersection Operations

Peak Hour	Cycle Time	DOS	Critical Movement Delay	95% Queue	Critical Approach
Weekday AM	100s	66%	29.6s	18.3 Veh	Gracemere Gavial Rd
Weekday PM	100s	62%	16.7s	12.5 Veh	Lawrie St

### 2.4 Road Safety Issues

#### 2.4.1 Existing Site Conditions

A desktop review of the existing traffic conditions on the relevant road network was undertaken by Lachlan McMurtrie (RPEQ/Road Safety Auditor) on Wednesday 22 November 2023. No obvious safety issues were identified.

#### 2.4.2 Road Crash History Review

A review of the road crash history at the Lawrie/John/Russell Street intersection was undertaken using the road crash data available from Queensland Globe Database, with the assessment completed from data from the past nine years (January 2015 – November 2023).

The results of this assessment identified two crashes within the proximity of the intersection, within the selected timeframe. However, it is noted that this data is historic in nature as it relates to the previous roundabout configuration and not the upgraded signalised layout. This change in layout limits the value of the crash history data in terms of future evaluation.

Table 4: Summary of Road Crash History (2015-2023)

Crash Ref. No.	Crash Year	Crash Severity	Crash Type	DCA Code	Crash Description			
Lawrie/John/Rus	Lawrie/John/Russell Street Intersection							
256611	2017	Hospitalisation	Multi-Vehicle	303	Veh'S Same Direction: Right Rear			
256626	2018	Minor Injury	Multi-Vehicle	301	Veh'S Same Direction: Right Rear			

The results above indicate that the increased traffic generated by the proposed development, can't be considered a specific safety risk. With only two crashes recorded in the vicinity of the proposed site over the last nine years (2015-2023) and the site configuration being updated from a roundabout to a signalised intersection. It is noted that both of these incidents were prior to the signalisation of the intersection.

#### 2.5 Site Access

There is currently no site access to the lot. Historically the lot maintained unhindered access to John Street for the majority of the frontage.

#### 2.6 Active and Public Transport

#### 2.6.1 Pedestrian & Cyclists

Regarding the proposed development site, pedestrian footpaths are provided on both sides of Lawrie Street. Along with a footpath present on John Street extending to the northern boundary of 4 John Street (Lot 505 R2642). The Lawrie/John/Russell Street signalised intersection has pedestrian crossings present for all approaches.

Additionally, there is currently on-road cyclist lanes on Lawrie Street and John Street and present on all approaches for the Lawrie/John/Russell St signalised intersection.

#### 2.6.2 Public Transport

Public transport routes are present along both sides of Lawrie Street, with public bus stops located within 200m of the proposed development lot. These bus stops are serviced by Young's Bus Service and comprise bus route 21 & 22, running between Gracemere, Rockhampton, Bouldercombe and Mt Morgan. With approximately one bus serviced in each direction per hour during operational hours along the routes on weekdays and weekends.

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### 3 Proposed Development Details

### 3.1 Operational Details

The proposed development is a Coffee Drive Through, which will occupy the northern half of Lot 604 on R2642 shown in the site plan included as Appendix A. The proposed development represents the final form of the site, and no further development is expected.

The development will provide a drive through service with outdoor seating along with six (6) spaces for onsite parking. Vehicular access is proposed via a left and right in/out access intersection with John St, while the largest design vehicle anticipated to require access to the site is a Medium Rigid Vehicle for delivery and waste collection. It is expected that the hours of collection for waste will be outside the peak period of operation.

The proposed Drive Through building has an area of 64m<sup>2</sup> GFA (with approximately 42m<sup>2</sup> of seating area), with parking spaces provided for cars parking near the building. The traffic elements of the proposed development are discussed further in the following sections.

#### 3.2 Proposed Access and Parking

#### 3.2.1 Site Access

As previously identified, vehicular access to the Drive Through development is proposed to be provided via a left and right in/out access intersection with John St catering for vehicles in the northbound and southbound lanes. A second left and right out only access is proposed to service the drive-through facility, which is required by the confined nature of the lot.

It is acknowledged that the requirement for two accesses will result in the loss of up to 6 on-street parking spaces on John Street. In order to offset this impact, the number of off-street parking spaces has been maximised as discussed in Section 3.2.2.1. Three additional off-street parking spaces will be provided in addition to the minimum amount required by the Planning Scheme, meaning half of the loss will be mitigated.

It is therefore seen as reasonable to allow two accesses on the basis that the actual impact, having been halved, is effectively the same as if the development only had one access.

Furthermore, given the function of the second access being for exit only movements, it is considered that interaction between the two accesses will be minimised, maintaining the safety of road users and pedestrians.

#### 3.2.2 Internal Site Facilities

To assess the adequacy of the internal traffic facilities, reference has been made to the Access, Parking and Transport Code within the Rockhampton Region Planning Scheme, as well as the relevant Australian Standards.

Compliance with the requirements of these documents is discussed in the following sections.

#### 3.2.2.1 Car Parking

Table 9.3.1.3.2: Parking requirements of RRC's Planning Scheme stipulates that for food and drink outlets a car parking requirement of 1 space for each 15 m2 of GFA for seating areas (including outdoor seating areas), with on-site queuing for at least 10 vehicles where involving a drive through facility. Given the proposed Drive Through has approximately  $42\text{m}^2\text{GFA}$  of seating area, namely the area shown as 'outdoor seating area' on the layout plans, and no internal seating area provision, the recommended parking provisions for the development is therefore 3 parking spaces (minimum). As shown on the site plan (included in Appendix A), a total of 6 parking spaces are proposed on site, including 1 PWD Bay for Persons with Disabilities.

All parking spaces proposed for light vehicles (cars) are generally 5.4m long and 2.6m wide and are accessed by a parking aisle exceeding 6.6m width, which meets the requirements stipulated in AS2890.1 for short term, high turnover parking, while the provision of 1 PWD bay for the proposal aligns with the general PWD bay provision rate of between 1-2% of the overall parking bays on site.

#### 3.2.2.2 Queuing and Vehicle Circulation

As shown in the Site Plan (refer Appendix A) the proposed site layout nominates one-way traffic flow (clockwise) for vehicles through the drive through. Vehicle swept paths have also been undertaken which confirm the ability of a light vehicle to travel along the drive through, with a copy of the relevant swept paths for the proposal included for reference in Appendix A. As per Table 9.3.1.3.2: Parking requirements of RRC's Planning Scheme, this Coffee Drive Through meets the requirement to contain an on-site queuing space for a minimum of 10 vehicles.

#### 3.2.2.3 Service Vehicle Access, Circulation and Loading

RRC's Planning Scheme doesn't specify a design vehicle for food and drink outlets. However, based on the approximate size and nature of the proposed development its likely only to be serviced by a Medium Rigid (MRV) vehicle or smaller. Thus, a delivery/refuse zone sized for a Medium Rigid Vehicle has been proposed on the south of the building. Vehicle swept paths have also been undertaken which confirm the ability of a MRV to travel into the site for delivery/waste collection purposes, with a copy of the relevant swept paths for the proposal included for reference in Appendix A.

#### 3.2.2.4 Pedestrians

The pedestrian access to the proposed development is via dedicated pedestrian access entrances, which are separate from the driveways, along John St frontage.

AS2890.1 requires that 2.0m wide x 2.5m long pedestrian sight splays be provided on the egress side of adjacent driveways to ensure sufficient visibility between drivers exiting the site and pedestrians using the footpath. The proposed Coffee Drive Through layout complies with these requirements, with no obstructions currently present on the egress of both driveways.

#### 3.2.2.5 Cyclists

The Austroads 'Cycling Aspects of Austroads Guides' states that a bicycle parking rate for Take aways of one per 100m<sup>2</sup> GFA for staff use and 1 per 50m<sup>2</sup> per GFA for customers. It is recommended that these spaces be provided for use prior to commencement of operational works. Consequently, it is recommended that bicycle parking for the proposed Coffee Drive Through be provided as:

Staff: One space

- Customers: Two Spaces

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### 4 Development Traffic

#### 4.1 Traffic Generation

To determine the traffic generation of the proposed service development, reference has been made to Bitzios *Trip Generation Drive Through Coffee Outlets Data and Analysis Report with Appendices*, which provides recommended traffic generation rates for drive through coffee shops based on surveys conducted at a number of sites across NSW. In accordance with the recommended range of 70-130 trips in the AM peak hour, and with consideration that the proposed use is in a regional area, a revised traffic generation rate in the AM peak hour of 70 trips/hr has been adopted. Based on the surveyed PM peak hour generation rate being on average ~25% of the AM peak hour generation rate, a conservative 35 trips/hr in the PM peak has been adopted, which represents 50% of the AM peak rate.

It is also standard practice to consider undiverted trips for Coffee Drive throughs (i.e., accounting for the trips already present on the road network). To remain consistent with this, it has been assumed that 50% of the trips associated with the development would be classified as undiverted "drop-in" trips.

#### 4.2 Traffic Distribution

Given the proposed development is a Coffee Drive Through, it is anticipated that most trips generated by the proposed development (if not all) will be undiverted "drop-in" trips undertaken by vehicles travelling past on Lawrie St.

However, with a view to maintaining a conservative approach, it has been assumed that 50% of trips generated by the Coffee Drive Through during the peak hours will be destination (i.e. new) trips, with a summary of the expected distribution of traffic from the development provided in Table 5 below.

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Table 5 - Proposed development traffic distribution

AM Peak	PM Peak
Arrival/Departure Split	
<ul> <li>50% traffic inbound to development; and</li> </ul>	<ul> <li>50% traffic inbound to development; and</li> </ul>
<ul> <li>50% traffic outbound from development.</li> </ul>	<ul> <li>50% traffic outbound from development.</li> </ul>
"New" Trip Distribution (50% Overall Trips)	
Inbound	Inbound
<ul> <li>60% from Gavial Gracemere Road (South- East)</li> </ul>	<ul> <li>25% from Gavial Gracemere Road (South- East)</li> </ul>
<ul> <li>5% from Russell Street (South-West)</li> </ul>	<ul> <li>5% from Russell Street (South-West)</li> </ul>
<ul> <li>25% from Lawrie Street (North-West)</li> </ul>	<ul> <li>60% from Lawrie Street (North-West)</li> </ul>
<ul> <li>10% from John Street (North)</li> </ul>	<ul> <li>10% from John Street (North)</li> </ul>
Outbound	Outbound
<ul> <li>10% to John Street (North)</li> </ul>	<ul> <li>10% to John Street (North)</li> </ul>
<ul> <li>60% to Lawrie Street (North-West)</li> </ul>	<ul> <li>60% to Lawrie Street (North-West)</li> </ul>
<ul> <li>5% to Russell Street (South-West)</li> </ul>	<ul> <li>5% to Russell Street (South-West)</li> </ul>
<ul> <li>25% from Gavial Gracemere Road (South- East)</li> </ul>	<ul> <li>25% from Gavial Gracemere Road (South- East)</li> </ul>
"Drop-In" Trip Distribution (50% Overall Trips)	
Inbound	Inbound
<ul> <li>60% from Gavial Gracemere Road (South- East)</li> </ul>	<ul> <li>30% from Gavial Gracemere Road (South- East)</li> </ul>
<ul> <li>30% from Lawrie Street (North-West)</li> </ul>	<ul> <li>60% from Lawrie Street (North-West)</li> </ul>
<ul> <li>10% from John Street (North)</li> </ul>	<ul> <li>10% from John Street (North)</li> </ul>
Outbound	Outbound
<ul> <li>10% to John Street (North)</li> </ul>	<ul> <li>10% to John Street (North)</li> </ul>
<ul> <li>60% to Lawrie Street (North-West)</li> </ul>	<ul> <li>30% to Lawrie Street (North-West)</li> </ul>
<ul> <li>30% from Gavial Gracemere Road (South- East)</li> </ul>	<ul> <li>60% from Gavial Gracemere Road (South- East)</li> </ul>

### 4.3 Development Traffic Volumes on the Network

The distribution of the development related traffic on the current road network has been estimated based on the directional split inherent in the supplied traffic surveys and expectations regarding the origins and destinations of the proposed use given its convenience nature. The resultant distribution of the development traffic for the "new" trips and "drop-in" trips are shown in the figures below.

### ROCKHAMPTON REGIONAL COUNCIL

**APPROVED PLANS** 

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**Development Permit No.: D/182-2023** 

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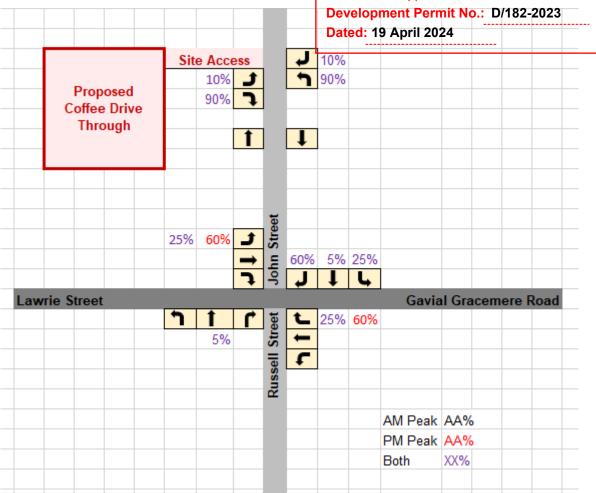


Figure 3: Development Distribution of "New" Trips

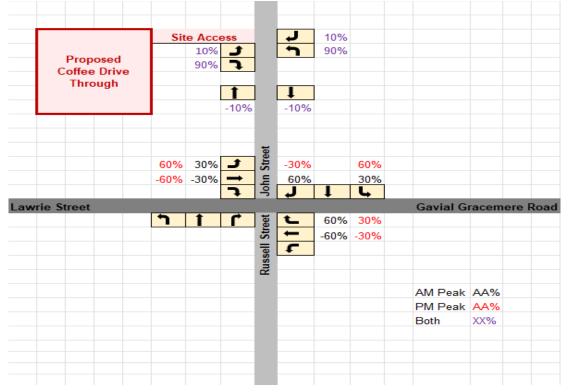


Figure 4: Development Distribution of "Drop-In" Trips

#### 4.4 Development Staging

#### 4.4.1 Timing

In the practice of analysing the future year traffic operations, it is standard to adopt a 10-year design period for the year of full operational commencement. Therefore, the subsequent development stages will be assumed:

- Traffic Counts: 2018

- Development Application: 2023

- Construction and Occupation: 2024

- Occupation Plus 10yrs: 2034

#### 4.4.2 Assessment Scenarios

Due to the location of the proposed development the site doesn't have direct access to the state-controlled road network, thus the following assessment scenarios have been adopted:

- Opening Year (2024) Pre-Development Scenario
- Opening Year (2024) Post-Development Scenario
- Occupation Plus 10yrs: 2034 (For Accesses)

#### 4.4.3 Traffic Counts Background Traffic Growth

Based on the 10-year growth in Average Annual Daily Traffic (AADT) as reported by TMR for Lawrie St, the background traffic growth for the impact assessment has been established. The background growth rate of 3% per annum has been assumed.

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Dated: 19 April 2024

### 5 Impact Assessment and Mitigation

Based on the information provided above, it was determined that the critical elements of the surrounding road network in terms of the potential impact of the proposed Coffee Drive Through development was the Lawrie/John/Russell Street intersection. Further details of the assessment of the impact of the development on the road network is provided in the following sections.

#### 5.1 With and Without Development Traffic Volumes

#### 5.1.1 Road Link Volumes

As previously discussed, given the proposed development is a Coffee Drive Through it is anticipated that most trips generated by the proposed development will be undiverted drop-in trips.

Whilst the development is predicted to generate in the order of 35 vehicle trips (entry and exit) in the AM and 18 vehicle trips (entry and exit) during the PM peak hours, at least 50% of these trips are expected to be undiverted drop-in trips by vehicles travelling past the proposed site on Lawrie St.

#### 5.1.2 Intersection Operations

The probable impact of the proposed Coffee Drive Through development on the AM/PM peak hour operations of the surrounding road network have been assessed using SIDRA. This analysis is based on the peak hour turning movement forecasts shown in Appendix B.

#### 5.1.2.1 Lawrie/John/Russell Street Intersection

The results from the SIDRA intersection analysis for Lawrie/John/Russell Street intersection as shown in Appendix C and summarised in Table 6. The results are based on the SIDRA representation of the proposed intersection shown in Figure 2. These results show that the intersection is expected to experience LOS D (or better) during the AM/PM peak hours, under the 2024 pre and post development conditions. The additional development traffic generated by the proposed Coffee Drive Through isn't expected to impose significant adverse conditions on the intersection operations.

Table 6: Lawrie/John/Russell St Intersection SIDRA Summary

		Critical		LOS	
Peak Hour	DOS	Movement Delay	95% Queue	LUS	Critical Approach
		Weekd	ay AM		
2024 Pre- Development	76%	37.6s	26.9 Veh	D	Russell St
2024 Post Development	78%	39.8s	27.8 Veh	D	Russell St
		Weekd	ay PM		
2024 Pre- Development	71%	27.9s	19.7 Veh	С	John St
2024 Post Development	73%	29.1s	20.6 Veh	С	Lawrie St

#### 5.1.3 Intersection Delay

In accordance with the procedure outlined in the Department of Transport and Main Roads' GTIA, an assessment on the impact of the proposed development on the cumulative delay at the affected intersection. The expected net change in delay has been calculated for the Lawrie/John/Russell Street signalised intersection, as indicated in Table 7 and 8.

Table 7: Cumulative Delays Assessment - 2024 AM Peak

15

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2024 AM Peak Pre Dev **Post Dev** Movement **Pre Dev Total Post Dev Total Pre Dev Vols Movement Avg Movement Avg** Delay Delay Delay Delay **Gracemere Gavial Rd** 39.3 275 293 Left 41.9 40320 Through 1050 38.4 41.3 43365 Right 40 41.4 1656 42.8 1712 John St Left 37 55.0 2035 54.9 2031 Through 9 50.4 454 50.3 453 55.0 Right 239 13145 54.8 13097 **Lawrie St** Left 54 26.6 1436 28.1 1517 500 22.1 11050 23.5 11750 Through Right 50 33.0 1650 32.9 1645 **Russell St** Left 71.1 4693 71.6 4726 66 9 66.6 599 604 Through 67.1 7 71.1 71.6 Right 498 501 Total 77811 Total 81695 % Difference Pre and Post Development 4.99%

Table 8: Cumulative Delays Assessment - 2024 PM Peak

		2024 PM Peak					
Movement	Pre Dev Vols	Pre Dev Movement Avg Delay	Pre Dev Total Delay	Post Dev Movement Avg Delay	Post Dev Total Delay		
Gracemere	Gavial Rd						
Left	18	32.8	590	33.5	603		
Through	755	28.2	21291	28.9	21820		
Right	45	33.7	1517	34.0	1530		
John St							
Left	39	61.4	2395	59.2	2309		
Through	6	56.8	341	54.6	328		
Right	127	61.3	7785	59.1	7506		
Lawrie St							
Left	64	24.5	1568	25.9	1658		
Through	1017	19.9	20238	21.5	21866		
Right	62	31.0	1922	31.8	1972		
Russell St							
Left	29	67.3	1952	67.3	1952		
Through	8	62.7	502	62.7	502		
Right	11	67.3	740	67.3	740		
		Total	60840	Total	62783		
		% Difference	ce Pre and Post De	evelopment	3.19%		

PM Right Turn

John St

172

Table 7 and 8 shows that the additional development traffic generated by the proposed Coffee Drive Through would result in a 4.99 and 3.19% increase in delay for the AM and PM Peaks, which equates to an average delay of 4% for the post-development traffic. Therefore, the presence of the additional traffic generated by the proposed development doesn't warrant mitigation works.

#### 5.2 Access and Frontage Impact Assessment and Mitigation

AM Right Turn

John St

The proposed site access ingress and egress will be provided as per Appendix A. Access visibility from both driveways requires a SISD of 114m based upon the 60km/h operational speed and other geometric parameters. Based on the SISD in Appendix A, one roadside parking space (between the driveways) will need to be removed to allow for adequate SISD for incoming vehicular movement. With this parking space removed:

- The main entry will be able to sight an oncoming vehicle comfortably with 155m from the left (northern end of John St) and 75m from the right (southern end on John St).
- The drive through exit will also be able to sight an oncoming vehicle comfortably with 120m from the left (northern end of John St) and 110m from the right (southern end on John St).

PM Left Turn

115

John St

Forecast through road and access turn volumes based on Figure 15 and 16 (Appendix B) in conjunction with a compound growth rate of 3% for through traffic are shown in Figure 5 and 6 below for the opening year of 2024 and the 10-year design horizon of 2034.

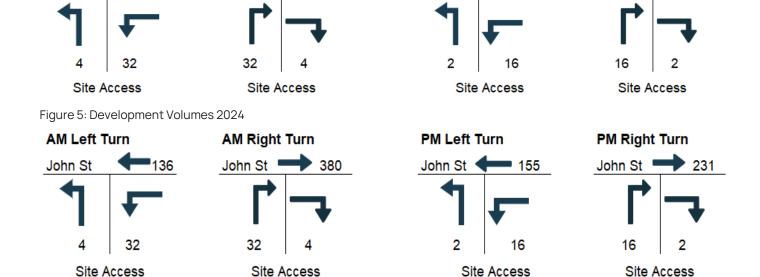


Figure 6: Development Volumes 2034

**AM Left Turn** 

John St

A turn warrants assessment was undertaken for the proposed site access intersection with John Street based on the forecast post development traffic volumes from the proposed Coffee Drive Through as identified in Figure 5 and Figure 6 above. The assessment was completed using Figure 2.26b of Austroads Guide to Traffic Management Part 6: Intersections, Interchanges and Crossings.

The resultant graphs from the assessment for the post development (2024) and the 10-year design horizon (2034) traffic conditions is provided in Figure 7 and 8 below.

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

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Dated: 19 April 2024

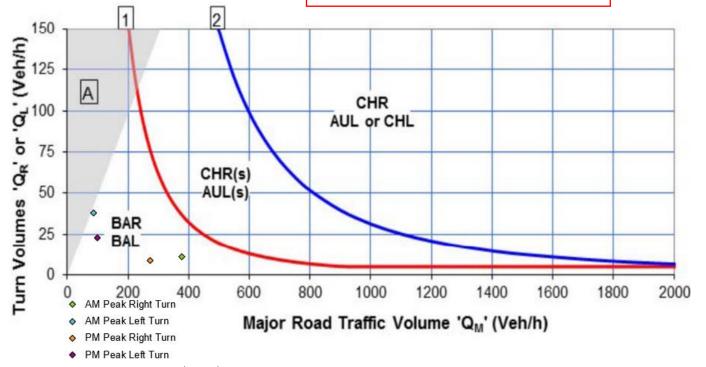


Figure 7: Post Development (2024) Warrant Graph

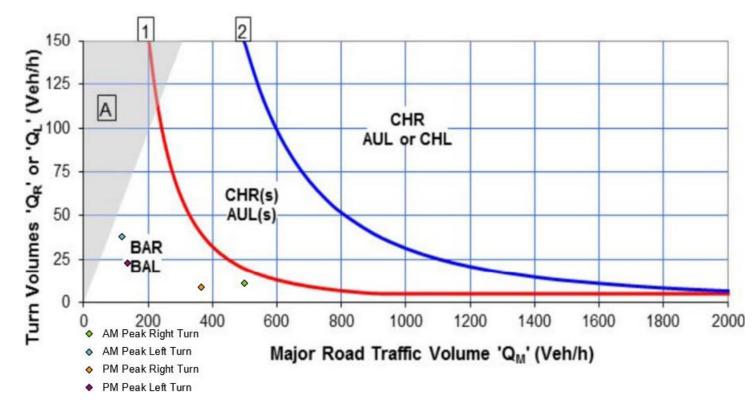


Figure 8: 10-Year Design Horizon (2034) Turn Warrant

The results of the turn warrants assessment indicate that the recommended turn treatments at the site access intersection of the John Street/site access intersection for the post development traffic volume scenario was a BAL treatment.

As a result of this, no further treatments are proposed to the existing intersection of John Street and the site access.

### 5.3 Pavement Impact Assessment and Mitigation

Given that the proposed development is a Coffee Drive Through and that the proposed development construction period will be completed in a short number of months, it is not expected to generate a significant number of new heavy vehicle movements under typical operation, no pavement mitigation works are deemed warranted or required because of the proposal.

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

Dated: 19 April 2024

PROJECT: Zarraffas Drive Through at 6 Lawrie St, Gracemere 4702 (Lot 604 on R2642)

DATE: 16/02/24 OUR REF: R002-23-24/012

### 6 Conclusions and Recommendations

### 6.1 Summary of Impacts and Mitigation Measures Proposed

#### 6.1.1 Internal Facilities

The traffic elements of the proposed plan of development have been designed generally in accordance with the requirements of AS2890 and Table 9.3.1.3.2: Parking requirements of RRC's Planning Scheme

The proposed on-site parking provision a total of 6 parking spaces, including 1 PWD Bay for Persons with Disabilities is considered adequate to cater for the parking demand expected to be generated by the development. The design of the car parking area is in accordance with the requirements outlined in the relevant standards and guidelines and is supportable from a traffic engineering perspective.

The proposed pedestrian footpath within the verge along John Street is anticipated to adequately cater for the pedestrian travel associated with the proposed development, and suitable connect to the existing pathway network in the area.

In addition, the swept paths for vehicles using the drive through and of the largest vehicle entering the site for delivery and waste removal are shown to comfortably be able to enter the site.

#### 6.1.2 Traffic Impacts

The turn warrants assessment undertaken based on the estimated post development traffic volumes (2034) indicated that the recommended turn treatments for the site access intersection of John Street/site access was a BAL treatment. As such no treatments are proposed.

The results of capacity analyses of the Lawrie/John/Russell Street intersection indicate that the proposed development will have minimal impact upon the operation of the Lawrie/John/Russell Street intersection at the proposed opening year (2024), with a minimal change in the operation between the pre and post development scenarios. Further to this, the results also indicate that the intersection is expected to operate within acceptable limits under all development scenarios assessed.

Lastly, it was also noted that the proposed development would have no impact upon the physical facilities or operation of the existing public transport and active transport facilities in the vicinity of the site.

#### 6.1.3 Recommendations

A minimum of three (3) bicycle parking spaces should be provided for the development to comply with *Austroads 'Cycling Aspects of Austroads Guides'*. Also, one (1) roadside parking space (between the driveways) will need to be removed to allow for adequate SISD.

Considering the information provided above, it is concluded that the proposed development will have a negligible impact on the adjacent road network and can therefore be recommended to be approved from a traffic engineering perspective.

#### 6.2 Certification Statement and Authorisation

A copy of the RPEQ certification and authorisation statement covering this assessment of the proposed Coffee Drive Through development located at 6 Lawrie St, Gracemere 4702, on land described as Lot 604 on R2642 is included as reference in Appendix C.

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

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## Appendix A: Site Layout Plan and Swept Paths

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

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**Dated: 19 April 2024** 

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### Appendix B: Turning Movement Forecasts

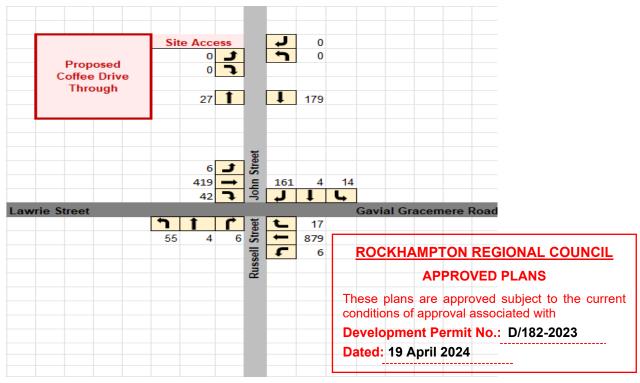


Figure 9: 2018 Existing AM Peak Hour

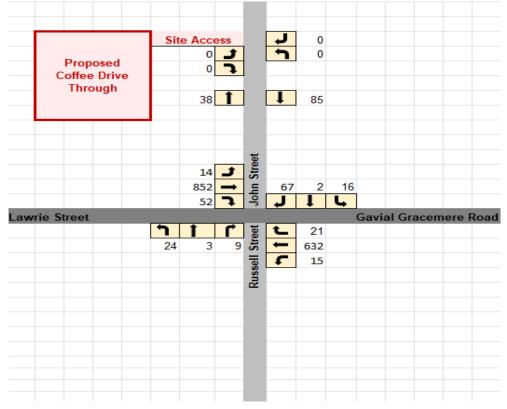


Figure 10: 2018 Existing PM Peak Hour

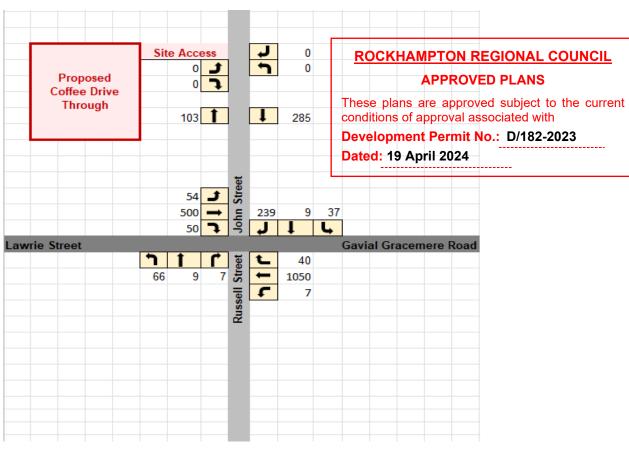


Figure 11: 2024 Pre-Development AM Peak Hour

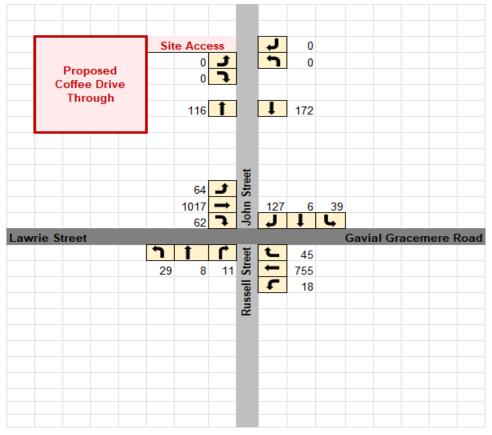


Figure 12: 2024 Pre-Development PM Peak Hour

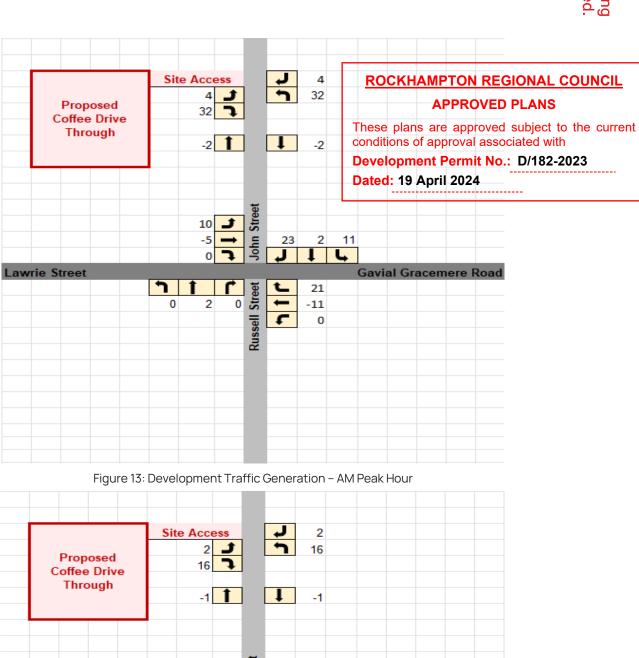


Figure 14: Development Traffic Generation - PM Peak Hour

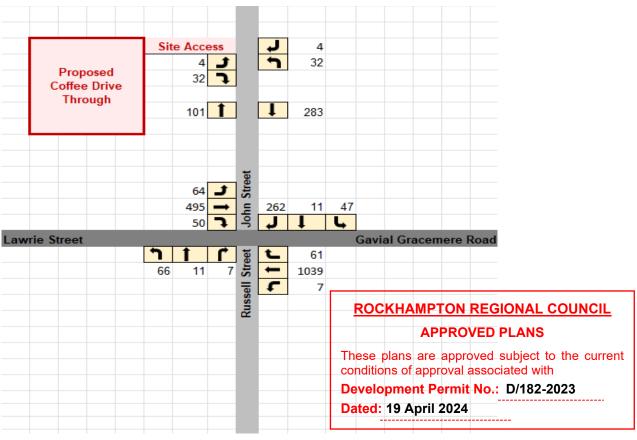


Figure 15: 2024 Post-Development AM Peak Hour

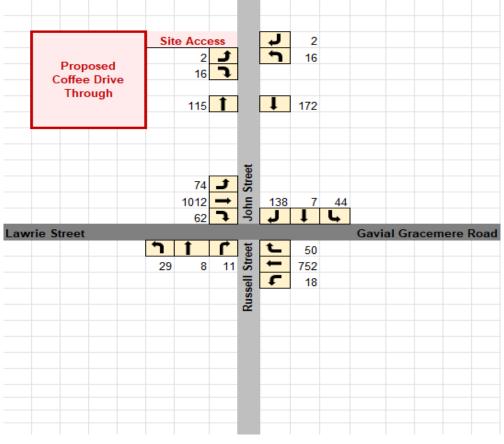


Figure 16: 2024 Post-Development PM Peak Hour

## Appendix C: Intersection Analysis

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## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

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**Development Permit No.: D/182-2023** 

**Dated: 19 April 2024** 

PROJECT: Zarraffas Drive Through at 6 Lawrie St, Gracemere 4702 (Lot 604 on R2642)

DATE: 16/02/24 OUR REF: R002-23-24/012

#### **MOVEMENT SUMMARY**

Site: 101 [2018 AM Existing (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.5.224

New Site Site Category: (None)

Delay)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Vehicle Movement Performance         Mov Turn Mov       Demand       Arrival       Deg. Aver. Level of       95% Back Of       Prop. Eff. Aver. Aver.															
Mov ID	Turn	Mov Class	FI	lows HV]		ows	Deg. Satn v/c	Aver. Delay sec		95% Ba Que [ Veh. veh		Prop. Que	Eff. Stop Rate	Aver. No. of Cycles	Aver. Speed km/h
South	n: Grac	emere G	avial Ro	oad											
1	L2	All MCs	6	2.2	6	2.2	0.658	34.2	LOS C	18.3	130.4	0.90	0.79	0.90	34.9
2	T1	All MCs	879	2.2	879	2.2	* 0.658	29.6	LOS C	18.3	130.5	0.90	0.79	0.90	35.5
3	R2	All MCs	17	2.2	17	2.2	0.077	27.9	LOS C	0.5	3.4	0.92	0.68	0.92	35.6
Appro	oach		902	2.2	902	2.2	0.658	29.6	LOS C	18.3	130.5	0.90	0.79	0.90	35.5
East:	East: John Street														
4	L2	All MCs	14	2.2	14	2.2	0.652	49.7	LOS D	8.6	61.4	0.99	0.83	1.03	29.4
5	T1	All MCs	4	2.2	4	2.2	* 0.652	45.1	LOS D	8.6	61.4	0.99	0.83	1.03	29.8
6	R2	All MCs	161	2.2	161	2.2	0.652	49.7	LOS D	8.6	61.4	0.99	0.83	1.03	29.4
Appro	oach		179	2.2	179	2.2	0.652	49.6	LOS D	8.6	61.4	0.99	0.83	1.03	29.4
North	North: Lawrie Street														
7	L2	All MCs	6	2.2	6	2.2	0.369	23.3	LOS C	6.1	43.8	0.83	0.69	0.83	38.9
8	T1	All MCs	419	2.2	419	2.2	* 0.369	18.7	LOS B	6.2	43.9	0.83	0.69	0.83	39.8
9	R2	All MCs	43	2.2	43	2.2	<b>*</b> 0.181	27.0	LOS C	1.1	7.7	0.92	0.72	0.92	35.9
Appro	oach		468	2.2	468	2.2	0.369	19.5	LOS B	6.2	43.9	0.84	0.69	0.84	39.3
West	: Russ	ell Street													
10	L2	All MCs	55	2.2	55	2.2	0.506	56.2	LOS E	3.3	23.3	1.00	0.76	1.00	27.9
11	T1	All MCs	4	2.2	4	2.2	* 0.506	51.6	LOS D	3.3	23.3	1.00	0.76	1.00	28.3
12	R2	All MCs	6	2.2	6	2.2	0.506	56.2	LOS E	3.3	23.3	1.00	0.76	1.00	28.0
Appro	oproach 65 2.2 65 2.			2.2	0.506	55.9	LOS E	3.3	23.3	1.00	0.76	1.00	28.0		
All Ve	hicles		1614	2.2	1614	2.2	0.658	30.0	LOS C	18.3	130.5	0.90	0.76	0.90	35.3

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

\* Critical Movement (Signal Timing)

Pedestrian I	Pedestrian Movement Performance													
Mov	Input	Dem.	Aver.	Level of .	AVERAGE	BACK OF	Prop.	Eff.	Travel	Travel	Aver.			
ID Crossing	Vol.	Flow	Delay	Service	QUE	UE	Que	Stop	Time	Dist. S	Speed			
					[ Ped	Dist ]		Rate						
	ped/h	ped/h	sec		ped	m			sec	m	m/sec			
South: Gracer	nere Ga	vial Road	t											
P1 Full	1	1	44.2	LOS E	0.0	0.0	0.94	0.94	198.0	200.0	1.01			
East: John Str	eet													

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P2 Full	1	1	25.6	LOS C	0.0	0.0	0.88	0.88	179.5	200.0	1.11
North: Lawrie S	Street										
P3 Full	1	1	44.2	LOS E	0.0	0.0	0.94	0.94	198.0	200.0	1.01
West: Russell S	Street										
P4 Full	3	3	44.2	LOS E	0.0	0.0	0.94	0.94	198.0	200.0	1.01
All Pedestrians	6	6	41.1	LOS E	0.0	0.0	0.93	0.93	194.9	200.0	1.03

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Project: C:\Users\Rhien\OneDrive - McMurtrie Consulting Engineers\Documents\MCM\TIA\Gracemere Zarraffas\SIDRA\Test

Variation TL 70VPH & HJ 2.sip9

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

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### **MOVEMENT SUMMARY**

Site: 101 [2018 PM Existing (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.5.224

New Site

Site Category: (None)

Delay)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Vehic	cle Mo	ovement	Perfo	rma	nce										
Mov	Turn	Mov	Dem			rival	Deg.	Aver.	Level of	95% Ba		Prop.	Eff.	Aver.	Aver.
ID		Class		OWS		OWS	Satn	Delay	Service	Que [ Veh.		Que	Stop Rate	No. of	Speed
			veh/h		[ Total I veh/h	пv ј %	v/c	sec		veh	Dist ] m		Rate	Cycles	km/h
South	: Grac	emere G				,,	., 5	555							
1	L2	All MCs	15	4.2	15	4.2	0.449	29.5	LOS C	11.8	85.4	0.80	0.69	0.80	36.5
2	T1	All MCs	632	4.2	632	4.2	0.449	24.9	LOS C	11.8	85.6	0.80	0.69	0.80	37.2
3	R2	All MCs	21	4.2	21	4.2	* 0.097	27.5	LOS C	0.6	4.0	0.92	0.69	0.92	35.7
Appro	ach		668	4.2	668	4.2	0.449	25.1	LOS C	11.8	85.6	0.80	0.69	0.80	37.2
East:	John S	Street													
4	L2	All MCs	16	4.2	16	4.2	0.589	55.8	LOS E	4.3	31.1	1.00	0.80	1.05	28.0
5	T1	All MCs	2	4.2	2	4.2	* 0.589	51.2	LOS D	4.3	31.1	1.00	0.80	1.05	28.4
6	R2	All MCs	67	4.2	67	4.2	0.589	55.8	LOS E	4.3	31.1	1.00	0.80	1.05	28.0
Appro	ach		85	4.2	85	4.2	0.589	55.7	LOS E	4.3	31.1	1.00	0.80	1.05	28.0
North	: Lawri	ie Street													
7	L2	All MCs	14	4.2	14	4.2	0.617	21.3	LOS C	12.5	90.7	0.87	0.75	0.87	39.7
8	T1	All MCs	852	4.2	852	4.2	* 0.617	16.7	LOS B	12.5	90.8	0.87	0.75	0.87	40.6
9	R2	All MCs	52	4.2	52	4.2	<b>*</b> 0.170	25.5	LOS C	1.4	9.9	0.89	0.72	0.89	36.4
Appro	ach		918	4.2	918	4.2	0.617	17.3	LOS B	12.5	90.8	0.87	0.75	0.87	40.3
West:	Russe	ell Street													
10	L2	All MCs	24	4.2	24	4.2	0.284	55.1	LOS E	1.8	12.8	0.98	0.73	0.98	28.2
11	T1	All MCs	3	4.2	3	4.2	* 0.284	50.5	LOS D	1.8	12.8	0.98	0.73	0.98	28.6
12	R2	All MCs	9	4.2	9	4.2	0.284	55.1	LOS E	1.8	12.8	0.98	0.73	0.98	28.2
Appro	ach		36	4.2	36	4.2	0.284	54.7	LOS D	1.8	12.8	0.98	0.73	0.98	28.2
All Ve	hicles		1707	4.2	1707	4.2	0.617	23.1	LOS C	12.5	90.8	0.85	0.73	0.85	37.9

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

\* Critical Movement (Signal Timing)

Pedestrian I	Pedestrian Movement Performance														
Mov ID Crossing	Input Vol.	Dem. Flow	Aver. Delay	Level of a Service	AVERAGE Que		Prop. Que	Eff. Stop	Travel Time	Travel Dist. S	Aver. Speed				
	ped/h	ped/h	sec		[ Ped ped	Dist ] m		Rate	sec	m	m/sec				
South: Gracer	mere Ga	vial Road	t												
P1 Full	1	1	44.2	LOS E	0.0	0.0	0.94	0.94	198.0	200.0	1.01				
East: John Sti	East: John Street														

#### **ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS**

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

P2 Full	1	1	23.8	LOS C	0.0	0.0	0.88	0.88	177.6	200.0	1.13
North: Lawrie	Street										
P3 Full	1	1	44.2	LOS E	0.0	0.0	0.94	0.94	198.0	200.0	1.01
West: Russell	Street										
P4 Full	18	18	44.2	LOS E	0.0	0.0	0.94	0.94	198.1	200.0	1.01
All Pedestrians	21	21	43.2	LOSE	0.0	0.0	0.94	0.94	197.1	200.0	1.01

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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Variation TL \_70VPH & HJ 2.sip9

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

Dated: 19 April 2024

Site: 101 [2024 AM Pre Dev (Site Folder: General)]
Output produced by SIDRA INTERSECTION Version: 9.1.5.224

New Site

Site Category: (None)

**MOVEMENT SUMMARY** 

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site Optimum Cycle Time - Minimum

Delay)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Vehicle Movement Performance           Mov Turn Mov         Demand         Arrival         Deg.         Aver.         Level of         95% Back Of         Prop.         Eff.         Aver.         Aver.															
Mov ID	Turn	Mov Class	FI	lows HV]		ows	Deg. Satn v/c	Aver. Delay sec		95% Ba Que [ Veh. veh		Prop. Que	Eff. Stop Rate	Aver. No. of Cycles	Aver. Speed km/h
South	n: Grad	emere G	avial Ro	oad											
1	L2	All MCs	7	2.2	7	2.2	0.740	39.3	LOS D	26.9	191.6	0.93	0.83	0.93	33.2
2	T1	All MCs	1050	2.2	1050	2.2	<b>*</b> 0.740	38.4	LOS D	26.9	191.6	0.93	0.82	0.93	33.8
3	R2	All MCs	40	2.2	40	2.2	0.219	41.4	LOS D	1.4	9.6	0.95	0.72	0.95	33.5
Appro	oach		1097	2.2	1097	2.2	0.740	38.5	LOS D	26.9	191.6	0.93	0.82	0.93	32.7
East:	East: John Street														
4	L2	All MCs	37	2.2	37	2.2	0.747	55.0	LOS D	16.3	116.4	1.00	0.88	1.06	28.2
5	T1	All MCs	9	2.2	9	2.2	<b>*</b> 0.747	50.4	LOS D	16.3	116.4	1.00	0.88	1.06	28.6
6	R2	All MCs	239	2.2	239	2.2	0.747	55.0	LOS D	16.3	116.4	1.00	0.88	1.06	28.2
Appro	oach		285	2.2	285	2.2	0.747	54.8	LOS D	16.3	116.4	1.00	0.88	1.06	28.2
North	North: Lawrie Street														
7	L2	All MCs	54	2.2	54	2.2	0.434	26.6	LOS C	9.8	69.7	0.83	0.72	0.83	37.3
8	T1	All MCs	500	2.2	500	2.2	* 0.434	22.1	LOS C	9.9	70.4	0.83	0.71	0.83	38.2
9	R2	All MCs	50	2.2	50	2.2	* 0.252	33.0	LOS C	1.5	10.9	0.95	0.73	0.95	33.9
Appro	oach		604	2.2	604	2.2	0.434	23.4	LOS C	9.9	70.4	0.84	0.71	0.84	37.7
West	: Russ	ell Street													
10	L2	All MCs	66	2.2	66	2.2	0.765	71.1	LOS E	5.2	37.2	1.00	0.90	1.24	25.1
11	T1	All MCs	9	2.2	9	2.2	* 0.765	66.6	LOS E	5.2	37.2	1.00	0.90	1.24	25.4
12	R2	All MCs	7	2.2	7	2.2	0.765	71.1	LOS E	5.2	37.2	1.00	0.90	1.24	25.1
Appro	pproach 82 2.2 82 2.			2.2	0.765	70.6	LOS E	5.2	37.2	1.00	0.90	1.24	25.2		
All Ve	hicles		2068	2.2	2068	2.2	0.765	37.6	LOS D	26.9	191.6	0.91	0.80	0.93	32.9

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

\* Critical Movement (Signal Timing)

Mov	Input	Dem.	Aver.	Level of A	VERAGE	BACK OF	Prop.	Eff.	Travel	Travel	Aver.		
ID Crossing	Vol.	Flow	Delay	Service	QUE	UE	Que	Stop	Time	Dist.	Speed		
					[ Ped	Dist ]		Rate					
	ped/h	ped/h	sec		ped	m			sec	m	m/sec		
South: Gracer	mere Ga	vial Road	i										
P1 Full	1	1	54.2	LOS E	0.0	0.0	0.95	0.95	208.0	200.0	0.96		
East: John Street													

P2 Full	1	1	34.5	LOS D	0.0	0.0	0.90	0.90	188.4	200.0	1.06
North: Lawrie S	Street										
P3 Full	1	1	54.2	LOS E	0.0	0.0	0.95	0.95	208.0	200.0	0.96
West: Russell S	Street										
P4 Full	3	3	54.2	LOS E	0.0	0.0	0.95	0.95	208.0	200.0	0.96
All Pedestrians	6	6	50.9	LOSE	0.0	0.0	0.94	0.94	204.7	200.0	0.98

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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#### **ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS**

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

#### **MOVEMENT SUMMARY**

Site: 101 [2024 PM Pre Dev (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.5.224

New Site

Site Category: (None)

Delay)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Vehic	cle Mo	ovement	Perfo	rma	nce										
Mov ID	Turn	Mov Class	[ Total	lows HV]		rival lows HV] %	Deg. Satn v/c	Aver. Delay sec	Level of Service	95% Ba Que [ Veh. veh		Prop. Que	Eff. Stop Rate	Aver. No. of Cycles	Aver. Speed km/h
South	: Grad	emere G	avial Ro	oad											
1	L2	All MCs	18	4.2	18	4.2	0.499	32.8	LOS C	16.7	120.8	0.80	0.70	0.80	35.3
2	T1	All MCs	755	4.2	755	4.2	0.499	28.2	LOS C	16.7	121.1	0.80	0.70	0.80	36.0
3	R2	All MCs	45	4.2	45	4.2	* 0.250	33.7	LOS C	1.4	10.4	0.96	0.73	0.96	33.6
Appro	ach		818	4.2	818	4.2	0.499	28.6	LOS C	16.7	121.1	0.80	0.70	0.80	35.9
East:	East: John Street														
4	L2	All MCs	39	4.2	39	4.2	0.714	61.4	LOS E	10.2	73.7	1.00	0.86	1.08	26.9
5	T1	All MCs	6	4.2	6	4.2	* 0.714	56.8	LOS E	10.2	73.7	1.00	0.86	1.08	27.3
6	R2	All MCs	127	4.2	127	4.2	0.714	61.3	LOS E	10.2	73.7	1.00	0.86	1.08	26.9
Appro	ach		172	4.2	172	4.2	0.714	61.2	LOS E	10.2	73.7	1.00	0.86	1.08	26.9
North	: Lawr	ie Street													
7	L2	All MCs	64	4.2	64	4.2	0.700	24.5	LOS C	19.6	142.0	0.89	0.79	0.89	38.3
8	T1	All MCs	1017	4.2	1017	4.2	* 0.700	19.9	LOS B	19.7	142.8	0.89	0.79	0.89	39.2
9	R2	All MCs	62	4.2	62	4.2	* 0.229	31.0	LOS C	2.0	14.4	0.92	0.74	0.92	34.5
Appro	ach		1143	4.2	1143	4.2	0.700	20.7	LOS C	19.7	142.8	0.89	0.78	0.89	38.8
West	Russ	ell Street													
10	L2	All MCs	29	4.2	29	4.2	0.453	67.3	LOS E	2.9	21.0	1.00	0.75	1.00	25.8
11	T1	All MCs	8	4.2	8	4.2	* 0.453	62.7	LOS E	2.9	21.0	1.00	0.75	1.00	26.2
12	R2	All MCs	11	4.2	11	4.2	0.453	67.3	LOS E	2.9	21.0	1.00	0.75	1.00	25.9
Appro	proach 48 4.2 48 4.2			4.2	0.453	66.6	LOS E	2.9	21.0	1.00	0.75	1.00	25.9		
All Ve	hicles		2181	4.2	2181	4.2	0.714	27.9	LOS C	19.7	142.8	0.87	0.76	0.87	36.1

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akcelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

\* Critical Movement (Signal Timing)

Pedestrian l	Pedestrian Movement Performance													
Mov ID Crossing	v Input Dem. Aver. Crossing Vol. Flow Delay				AVERAGE Que	BACK OF UE	Prop. Que	Eff. Stop	Travel Time	Travel Dist. S	Aver. Speed			
	ped/h	ped/h	sec		[ Ped ped	Dist ] m		Rate	sec	m	m/sec			
South: Gracei	mere Ga	vial Road	k											
P1 Full	1	1	54.2	LOS E	0.0	0.0	0.95	0.95	208.0	200.0	0.96			
East: John St	reet													

### **ROCKHAMPTON REGIONAL COUNCIL**

#### **APPROVED PLANS**

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

P2 Full	1	1	31.8	LOS D	0.0	0.0	0.90	0.90	185.6	200.0	1.08
North: Lawrie	Street										
P3 Full	1	1	54.2	LOS E	0.0	0.0	0.95	0.95	208.0	200.0	0.96
West: Russell	Street										
P4 Full	18	18	54.2	LOS E	0.1	0.1	0.95	0.95	208.0	200.0	0.96
All Pedestrians	21	21	53.1	LOS E	0.1	0.1	0.95	0.95	207.0	200.0	0.97

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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### **ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS**

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

### **MOVEMENT SUMMARY**

Site: 101 [2024 AM Post Dev (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.5.224

New Site

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site Optimum Cycle Time - Minimum

Delay)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Vehic	cle Mo	ovement	Perfo	rmai	nce										
Mov ID	Turn	Mov Class	FI			rival lows HV] %	Deg. Satn v/c	Aver. Delay sec	Level of Service	95% Ba Que [ Veh. veh		Prop. Que	Eff. Stop Rate	Aver. No. of Cycles	Aver. Speed km/h
South	: Grac	emere G			ven/m	/0	V/C	366		Ven	- '''				KIII/II
1	L2	All MCs	7	2.2	7	2.2	0.769	41.9	LOS D	27.8	198.0	0.95	0.86	0.97	32.5
2	T1	All MCs	1039	2.2	1039	2.2	* 0.769	41.3	LOS D	27.8	198.0	0.95	0.86	0.97	33.0
3	R2	All MCs	61	2.2	61	2.2	* 0.334	42.8	LOS D	2.2	15.4	0.97	0.74	0.97	33.2
Appro	ach		1107	2.2	1107	2.2	0.769	41.4	LOS D	27.8	198.0	0.95	0.85	0.97	31.9
East:	John S	Street													
4	L2	All MCs	47	2.2	47	2.2	0.777	54.9	LOS D	18.6	132.3	1.00	0.90	1.08	28.2
5	T1	All MCs	11	2.2	11	2.2	* 0.777	50.3	LOS D	18.6	132.3	1.00	0.90	1.08	28.7
6	R2	All MCs	262	2.2	262	2.2	0.777	54.8	LOS D	18.6	132.3	1.00	0.90	1.08	28.3
Appro	ach		320	2.2	320	2.2	0.777	54.7	LOS D	18.6	132.3	1.00	0.90	1.08	28.3
North	: Lawr	ie Street													
7	L2	All MCs	64	2.2	64	2.2	0.462	28.1	LOS C	10.2	72.8	0.85	0.73	0.85	36.7
8	T1	All MCs	495	2.2	495	2.2	* 0.462	23.5	LOS C	10.3	73.7	0.85	0.72	0.85	37.6
9	R2	All MCs	50	2.2	50	2.2	0.252	32.9	LOS C	1.5	10.5	0.95	0.73	0.95	33.9
Appro	ach		609	2.2	609	2.2	0.462	24.7	LOS C	10.3	73.7	0.86	0.73	0.86	37.2
West:	Russ	ell Street													
10	L2	All MCs	66	2.2	66	2.2	0.782	71.6	LOS E	5.4	38.3	1.00	0.91	1.27	25.0
11	T1	All MCs	11	2.2	11	2.2	* 0.782	67.1	LOS E	5.4	38.3	1.00	0.91	1.27	25.4
12	R2	All MCs	7	2.2	7	2.2	0.782	71.6	LOS E	5.4	38.3	1.00	0.91	1.27	25.1
Appro	ach		84	2.2	84	2.2	0.782	71.0	LOS E	5.4	38.3	1.00	0.91	1.27	25.1
All Ve	hicles		2120	2.2	2120	2.2	0.782	39.8	LOS D	27.8	198.0	0.93	0.82	0.97	32.2

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

\* Critical Movement (Signal Timing)

Pedestrian I	Pedestrian Movement Performance												
Mov	Input	Dem.	Aver.	Level of a	AVERAGE	BACK OF	Prop.	Eff.	Travel	Travel	Aver.		
ID Crossing	Vol.	Flow	Delay	Service	QUE	UE	Que	Stop	Time	Dist. S	Speed		
					[Ped	Dist ]		Rate					
	ped/h	ped/h	sec		ped	m			sec	m	m/sec		
South: Gracer	nere Ga	vial Road	d										
P1 Full	1	1	54.2	LOS E	0.0	0.0	0.95	0.95	208.0	200.0	0.96		
East: John Str	eet												

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

P2 Full	1	1	34.5	LOS D	0.0	0.0	0.90	0.90	188.4	200.0	1.06
North: Lawrie S	Street										
P3 Full	1	1	54.2	LOS E	0.0	0.0	0.95	0.95	208.0	200.0	0.96
West: Russell S	Street										
P4 Full	3	3	54.2	LOS E	0.0	0.0	0.95	0.95	208.0	200.0	0.96
All Pedestrians	6	6	50.9	LOSE	0.0	0.0	0.94	0.94	204.7	200.0	0.98

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay) Pedestrian movement LOS values are based on average delay per pedestrian movement. Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

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### **ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS**

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

### **MOVEMENT SUMMARY**

Site: 101 [2024 PM Post Dev (Site Folder: General)]

Output produced by SIDRA INTERSECTION Version: 9.1.5.224

New Site

Site Category: (None)

Signals - EQUISAT (Fixed-Time/SCATS) Isolated Cycle Time = 120 seconds (Site Optimum Cycle Time - Minimum

Delay)

Variable Sequence Analysis applied. The results are given for the selected output sequence.

Class	Vehic	cle Mo	ovement	Perfo	rmaı	nce										
		Turn														Aver.
Veh/h         %         veh/h         %         v/c         sec         veh/h         m           South: Gracewere Gavial Read           1         L2         All MCs         18         4.2         18         4.2         0.508         33.5         LOS C         16.8         122.0         0.81         0.71         0.81           2         T1         All MCs         752         4.2         752         4.2         0.508         28.9         LOS C         16.9         122.3         0.81         0.71         0.81           3         R2         All MCs         50         4.2         50         4.2         0.508         29.4         LOS C         16.9         122.3         0.81         0.71         0.81           Approach         820         4.2         50.508         29.4         LOS C         16.9         122.3         0.82         0.71         0.82           East: John Crace         820         4.2         0.508         29.4         LOS C         16.9         122.3         0.82         0.71         0.82           East: John Crace         820         4.2         0.697         59.2         LOS E	טו		Class					Satn	Delay	Service			Que			Speed
1 L2 All MCs 18 4.2 18 4.2 0.508 33.5 LOS C 16.8 122.0 0.81 0.71 0.81 2 T1 All MCs 752 4.2 752 4.2 0.508 28.9 LOS C 16.9 122.3 0.81 0.71 0.81 3 R2 All MCs 50 4.2 50 4.2 *0.277 34.0 LOS C 16.9 122.3 0.82 0.71 0.82  Approach 820 4.2 820 4.2 0.508 29.4 LOS C 16.9 122.3 0.82 0.71 0.82  East: John Street 4 L2 All MCs 44 4.2 44 4.2 0.697 59.2 LOS E 11.0 79.5 1.00 0.85 1.05 5 T1 All MCs 7 4.2 7 4.2 *0.697 59.1 LOS E 11.0 79.5 1.00 0.85 1.05 6 R2 All MCs 138 4.2 138 4.2 0.697 59.1 LOS E 11.0 79.5 1.00 0.85 1.05  Approach 189 4.2 189 4.2 0.697 59.0 LOS E 11.0 79.5 1.00 0.85 1.05  North: Lawrie Street 7 L2 All MCs 74 4.2 74 4.2 0.734 25.9 LOS C 20.5 148.6 0.91 0.81 0.91 8 T1 All MCs 1012 4.2 1012 4.2 *0.734 25.9 LOS C 20.6 149.4 0.91 0.81 0.91 9 R2 All MCs 62 4.2 62 4.2 0.243 31.8 LOS C 2.0 14.2 0.93 0.74 0.93  Approach 1148 4.2 1148 4.2 0.734 22.4 LOS C 20.6 149.4 0.91 0.80 0.91  West: Russell Street 10 L2 All MCs 8 4.2 8 4.2 *0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00 11 T1 All MCs 11 4.2 11 4.2 0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00								v/c	sec					rtato	Oyoloo	km/h
2         T1         All MCs         752         4.2         752         4.2         0.508         28.9         LOS C         16.9         122.3         0.81         0.71         0.81           3         R2         All MCs         50         4.2         50         4.2         *0.508         29.4         LOS C         1.6         11.8         0.96         0.73         0.96           Approach         820         4.2         820         4.2         0.508         29.4         LOS C         1.6         11.8         0.96         0.73         0.96           Approach         820         4.2         820         4.2         0.508         29.4         LOS C         16.9         122.3         0.82         0.71         0.82           East: John Street         ***********************************	South	: Grac	emere G	avial Ro	oad											
3         R2         All MCs         50         4.2         50         4.2         *0.277         34.0         LOS C         1.6         11.8         0.96         0.73         0.96           Approach         820         4.2         820         4.2         0.508         29.4         LOS C         16.9         122.3         0.82         0.71         0.82           East: John Street           4         L2         All MCs         44         4.2         0.697         59.2         LOS E         11.0         79.5         1.00         0.85         1.05           5         T1         All MCs         7         4.2         138         4.2         0.697         59.1         LOS E         11.0         79.5         1.00         0.85         1.05           6         R2         All MCs         138         4.2         138         4.2         0.697         59.1         LOS E         11.0         79.5         1.00         0.85         1.05           Approach         189         4.2         189         4.2         0.697         59.0         LOS E         11.0         79.5         1.00         0.81         0.91	1	L2	All MCs	18	4.2	18	4.2	0.508	33.5	LOS C	16.8	122.0	0.81	0.71	0.81	35.0
Approach       820       4.2       820       4.2       0.508       29.4       LOS C       16.9       122.3       0.82       0.71       0.82         East: John Street         4       L2       All MCs       44       4.2       44       4.2       0.697       59.2       LOS E       11.0       79.5       1.00       0.85       1.05         5       T1       All MCs       7       4.2       7       4.2       *0.697       59.1       LOS E       11.0       79.5       1.00       0.85       1.05         6       R2       All MCs       138       4.2       138       4.2       0.697       59.1       LOS E       11.0       79.5       1.00       0.85       1.05         Approach       189       4.2       189       4.2       0.697       59.0       LOS E       11.0       79.5       1.00       0.85       1.05         North: Lawrier Street         7       L2       All MCs       74       4.2       0.734       25.9       LOS C       20.5       148.6       0.91       0.81       0.91         8       T1       All MCs       1012	2	T1	All MCs	752	4.2	752	4.2	0.508	28.9	LOS C	16.9	122.3	0.81	0.71	0.81	35.7
East: John Street  4	3	R2	All MCs	50	4.2	50	4.2	<b>*</b> 0.277	34.0	LOS C	1.6	11.8	0.96	0.73	0.96	33.6
4 L2 All MCs 44 4.2 44 4.2 0.697 59.2 LOS E 11.0 79.5 1.00 0.85 1.05  5 T1 All MCs 7 4.2 7 4.2 *0.697 54.6 LOS D 11.0 79.5 1.00 0.85 1.05  6 R2 All MCs 138 4.2 138 4.2 0.697 59.1 LOS E 11.0 79.5 1.00 0.85 1.05  Approach 189 4.2 189 4.2 0.697 59.0 LOS E 11.0 79.5 1.00 0.85 1.05  North: Lawrie Street  7 L2 All MCs 74 4.2 74 4.2 0.734 25.9 LOS C 20.5 148.6 0.91 0.81 0.91  8 T1 All MCs 1012 4.2 1012 4.2 *0.734 21.5 LOS C 20.6 149.4 0.91 0.81 0.91  9 R2 All MCs 62 4.2 62 4.2 0.243 31.8 LOS C 20.6 149.4 0.91 0.80 0.91  West: Russell Street  10 L2 All MCs 29 4.2 148 4.2 0.734 22.4 LOS C 20.6 149.4 0.91 0.80 0.91  West: Russell Street  10 L2 All MCs 8 4.2 8 4.2 *0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00  11 T1 All MCs 11 4.2 11 4.2 0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00	Appro	ach		820	4.2	820	4.2	0.508	29.4	LOS C	16.9	122.3	0.82	0.71	0.82	35.6
5         T1         All MCs         7         4.2         7         4.2         * 0.697         54.6         LOS D         11.0         79.5         1.00         0.85         1.05           6         R2         All MCs         138         4.2         138         4.2         0.697         59.1         LOS E         11.0         79.5         1.00         0.85         1.05           Approach         189         4.2         189         4.2         0.697         59.0         LOS E         11.0         79.5         1.00         0.85         1.05           North: Lawrie Street           7         L2         All MCs         74         4.2         74         4.2         0.734         25.9         LOS C         20.5         148.6         0.91         0.81         0.91           8         T1         All MCs         1012         4.2         1012         4.2         *0.734         21.5         LOS C         20.6         149.4         0.91         0.81         0.91           9         R2         All MCs         62         4.2         62         4.2         0.243         31.8 <t>LOS C         20.6         149.4</t>	East:	John S	Street													
6 R2 All MCs 138 4.2 138 4.2 0.697 59.1 LOSE 11.0 79.5 1.00 0.85 1.05  Approach 189 4.2 189 4.2 0.697 59.0 LOSE 11.0 79.5 1.00 0.85 1.05  North: Lawrie Street  7 L2 All MCs 74 4.2 74 4.2 0.734 25.9 LOS C 20.5 148.6 0.91 0.81 0.91  8 T1 All MCs 1012 4.2 1012 4.2 *0.734 21.5 LOS C 20.6 149.4 0.91 0.81 0.91  9 R2 All MCs 62 4.2 62 4.2 0.243 31.8 LOS C 2.0 14.2 0.93 0.74 0.93  Approach 1148 4.2 1148 4.2 0.734 22.4 LOS C 20.6 149.4 0.91 0.80 0.91  West: Russell Street  10 L2 All MCs 29 4.2 29 4.2 0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00  11 T1 All MCs 8 4.2 8 4.2 *0.453 62.7 LOS E 2.9 21.0 1.00 0.75 1.00  12 R2 All MCs 11 4.2 11 4.2 0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00	4	L2	All MCs	44	4.2	44	4.2	0.697	59.2	LOS E	11.0	79.5	1.00	0.85	1.05	27.3
Approach       189       4.2       189       4.2       0.697       59.0       LOS E       11.0       79.5       1.00       0.85       1.05         North: Lawrie Street         7       L2       All MCs       74       4.2       74       4.2       0.734       25.9       LOS C       20.5       148.6       0.91       0.81       0.91         8       T1       All MCs       1012       4.2       *0.734       21.5       LOS C       20.6       149.4       0.91       0.81       0.91         9       R2       All MCs       62       4.2       62       4.2       0.243       31.8       LOS C       2.0       14.2       0.93       0.74       0.93         Approach       1148       4.2       1148       4.2       0.734       22.4       LOS C       20.6       149.4       0.91       0.80       0.91         West: Russell Street         10       L2       All MCs       29       4.2       29       4.2       0.453       67.3       LOS E       2.9       21.0       1.00       0.75       1.00         11       T1       All MCs       11       4.2       11	5	T1	All MCs	7	4.2	7	4.2	* 0.697	54.6	LOS D	11.0	79.5	1.00	0.85	1.05	27.7
North: Lawrie Street  7	6	R2	All MCs	138	4.2	138	4.2	0.697	59.1	LOS E	11.0	79.5	1.00	0.85	1.05	27.4
7 L2 All MCs 74 4.2 74 4.2 0.734 25.9 LOS C 20.5 148.6 0.91 0.81 0.91  8 T1 All MCs 1012 4.2 1012 4.2 *0.734 21.5 LOS C 20.6 149.4 0.91 0.81 0.91  9 R2 All MCs 62 4.2 62 4.2 0.243 31.8 LOS C 2.0 14.2 0.93 0.74 0.93  Approach 1148 4.2 1148 4.2 0.734 22.4 LOS C 20.6 149.4 0.91 0.80 0.91  West: Russell Street  10 L2 All MCs 29 4.2 29 4.2 0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00  11 T1 All MCs 8 4.2 8 4.2 *0.453 62.7 LOS E 2.9 21.0 1.00 0.75 1.00  12 R2 All MCs 11 4.2 11 4.2 0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00	Appro	ach		189	4.2	189	4.2	0.697	59.0	LOS E	11.0	79.5	1.00	0.85	1.05	27.4
8 T1 All MCs 1012 4.2 1012 4.2 *0.734 21.5 LOS C 20.6 149.4 0.91 0.81 0.91 9 R2 All MCs 62 4.2 62 4.2 0.243 31.8 LOS C 2.0 14.2 0.93 0.74 0.93 Approach 1148 4.2 1148 4.2 0.734 22.4 LOS C 20.6 149.4 0.91 0.80 0.91  West: Russell Street 10 L2 All MCs 29 4.2 29 4.2 0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00 11 T1 All MCs 8 4.2 8 4.2 *0.453 62.7 LOS E 2.9 21.0 1.00 0.75 1.00 12 R2 All MCs 11 4.2 11 4.2 0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00	North	: Lawr	ie Street													
9 R2 All MCs 62 4.2 62 4.2 0.243 31.8 LOS C 2.0 14.2 0.93 0.74 0.93  Approach 1148 4.2 1148 4.2 0.734 22.4 LOS C 20.6 149.4 0.91 0.80 0.91  West: Russell Street  10 L2 All MCs 29 4.2 29 4.2 0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00  11 T1 All MCs 8 4.2 8 4.2 *0.453 62.7 LOS E 2.9 21.0 1.00 0.75 1.00  12 R2 All MCs 11 4.2 11 4.2 0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00	7	L2	All MCs	74	4.2	74	4.2	0.734	25.9	LOS C	20.5	148.6	0.91	0.81	0.91	37.7
Approach 1148 4.2 1148 4.2 0.734 22.4 LOS C 20.6 149.4 0.91 0.80 0.91  West: Russell Street  10 L2 All MCs 29 4.2 29 4.2 0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00  11 T1 All MCs 8 4.2 8 4.2 *0.453 62.7 LOS E 2.9 21.0 1.00 0.75 1.00  12 R2 All MCs 11 4.2 11 4.2 0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00	8	T1	All MCs	1012	4.2	1012	4.2	* 0.734	21.5	LOS C	20.6	149.4	0.91	0.81	0.91	38.6
West: Russell Street  10  L2 All MCs	9	R2	All MCs	62	4.2	62	4.2	0.243	31.8	LOS C	2.0	14.2	0.93	0.74	0.93	34.4
10 L2 All MCs 29 4.2 29 4.2 0.453 67.3 LOSE 2.9 21.0 1.00 0.75 1.00  11 T1 All MCs 8 4.2 8 4.2 *0.453 62.7 LOSE 2.9 21.0 1.00 0.75 1.00  12 R2 All MCs 11 4.2 11 4.2 0.453 67.3 LOSE 2.9 21.0 1.00 0.75 1.00	Appro	ach		1148	4.2	1148	4.2	0.734	22.4	LOS C	20.6	149.4	0.91	0.80	0.91	38.2
11 T1 All MCs 8 4.2 8 4.2 *0.453 62.7 LOS E 2.9 21.0 1.00 0.75 1.00  12 R2 All MCs 11 4.2 11 4.2 0.453 67.3 LOS E 2.9 21.0 1.00 0.75 1.00	West:	Russ	ell Street													
12 R2 All MCs 11 4.2 11 4.2 0.453 67.3 LOSE 2.9 21.0 1.00 0.75 1.00	10	L2	All MCs	29	4.2	29	4.2	0.453	67.3	LOS E	2.9	21.0	1.00	0.75	1.00	25.8
	11	T1	All MCs	8	4.2	8	4.2	* 0.453	62.7	LOS E	2.9	21.0	1.00	0.75	1.00	26.2
Approach 48 4.2 48 4.2 0.453 66.6 LOSE 2.9 21.0 1.00 0.75 1.00	12	R2	All MCs	11	4.2	11	4.2	0.453	67.3	LOS E	2.9	21.0	1.00	0.75	1.00	25.9
	Appro	ach		48	4.2	48	4.2	0.453	66.6	LOS E	2.9	21.0	1.00	0.75	1.00	25.9
All Vehicles 2205 4.2 2205 4.2 0.734 29.1 LOS C 20.6 149.4 0.89 0.77 0.89	All Ve	hicles		2205	4.2	2205	4.2	0.734	29.1	LOS C	20.6	149.4	0.89	0.77	0.89	35.6

Site Level of Service (LOS) Method: Delay (SIDRA). Site LOS Method is specified in the Parameter Settings dialog (Options tab). Vehicle movement LOS values are based on average delay per movement.

Intersection and Approach LOS values are based on average delay for all vehicle movements.

Delay Model: SIDRA Standard (Control Delay: Geometric Delay is included).

Queue Model: SIDRA queue estimation methods are used for Back of Queue and Queue at Start of Green.

Gap-Acceptance Capacity Formula: SIDRA Standard (Akçelik M3D).

HV (%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Arrival Flows used in performance calculations are adjusted to include any Initial Queued Demand and Upstream Capacity Constraint effects.

\* Critical Movement (Signal Timing)

Pedestrian I	Pedestrian Movement Performance												
Mov ID Crossing	Input Vol.	Dem. Flow	Aver. Delay	Level of a Service	AVERAGE QUE I Ped		Prop. Que	Eff. Stop Rate	Travel Time	Travel Dist.	Aver. Speed		
South: Gracer	ped/h mere Gav	ped/h vial Road	sec		ped	m m		rate	sec	m	m/sec		
P1 Full	1	1	54.2	LOS E	0.0	0.0	0.95	0.95	208.0	200.0	0.96		
East: John Str	eet												

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

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**Development Permit No.: D/182-2023** 

P2 Full	1	1	32.3	LOS D	0.0	0.0	0.90	0.90	186.2	200.0	1.07
North: Lawrie	Street										
P3 Full	1	1	54.2	LOS E	0.0	0.0	0.95	0.95	208.0	200.0	0.96
West: Russell	Street										
P4 Full	18	18	54.2	LOS E	0.1	0.1	0.95	0.95	208.0	200.0	0.96
All Pedestrians	21	21	53.1	LOSE	0.1	0.1	0.95	0.95	207.0	200.0	0.97

Level of Service (LOS) Method: SIDRA Pedestrian LOS Method (Based on Average Delay)
Pedestrian movement LOS values are based on average delay per pedestrian movement.
Intersection LOS value for Pedestrians is based on average delay for all pedestrian movements.

SIDRA INTERSECTION 9.1 | Copyright © 2000-2023 Akcelik and Associates Pty Ltd | sidrasolutions.com
Organisation: MCMURTRIE CONSULTING ENGINEERS PTY LTD | Licence: PLUS / 1PC | Processed: Friday, 9 February 2024 11:51:02 AM
Project: C:\Users\Rhien\OneDrive - McMurtrie Consulting Engineers\Documents\MCM\TIA\Gracemere Zarraffas\SIDRA\Test
Variation TL 70VPH & HJ 2.sip9

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**Development Permit No.: D/182-2023** 

Dated: 19 April 2024

### Appendix D: RPEQ Certification

Certification of Traffic Impact Assessment Report Registered Professional Engineer Queensland

for

**Project Title:** 

Zarraffas Drive Through Gracemere

As a professional engineer registered by the Board of Professional Engineers of Queensland pursuant to the *Professional Engineers Act 2002* as competent in my areas of nominated expertise, I understand and recognise:

- the significant role of engineering as a profession, and that
- the community has a legitimate expectation that my certification affixed to this engineering work can be trusted, and that
- I am responsible for ensuring its preparation has satisfied all necessary standards, conduct and contemporary practice.

As the responsible RPEQ, I certify:

- i. I am satisfied that all submitted components comprising this traffic impact assessment, listed in the following table, have been completed in accordance with the Guide to Traffic Impact Assessment published by the Queensland Department of Transport and Main Roads and using sound engineering principles, and
- ii. where specialised areas of work have not been under my direct supervision, I have reviewed the outcomes of the work and consider the work and its outcomes as suitable for the purposes of this traffic impact assessment, and that
- iii. the outcomes of this traffic impact assessment are a true reflection of results of assessment, and that
- iv. I believe the strategies recommended for mitigating impacts by this traffic impact assessment.
- v. embrace contemporary practice initiatives and will deliver the desired outcomes.

Name:	Chris Hewitt	RPEQ No:	05141
RPEQ Competencies:	Civil	-	
Signature:	agf:#	Dated:	06/02/2024
Postal Address:	PO Box 2149 Wandal QLD 4700	-	
Email:	chris@mcmengineers.com		

PROJECT: Zarraffas Drive Through at 6 Lawrie St, Gracemere 4702 (Lot 604 on R2642)

DATE: 16/02/24 OUR REF: R002-23-24/012

# Engineering reimagined

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

Traffic impact assessment components to which this certification applies	✓
1. Introduction	
Background	✓
Scope and study area	✓
Pre-lodgement meeting notes	✓
2. Existing Conditions	
Land use and zoning	N/A
Adjacent land uses / approvals	N/A
Surrounding road network details	✓
Traffic volumes	✓
Intersection and network performance	✓
Road safety issues	✓
Site access	<b>✓</b>
Public transport (if applicable)	✓
Active transport (if applicable)	✓
Parking (if applicable)	<b>✓</b>
Pavement (if applicable)	N/A
Transport infrastructure (if applicable)	N/A
3. Proposed Development Details	1477
Development site plan	✓
Operational details (including year of opening of each stage and any relevant catchment / market analysis)	✓
Proposed access and parking	✓
4. Development Traffic	
Traffic generation (by development stage if relevant and considering light and heavy vehicle trips)	✓
Trip distribution	✓
Development traffic volumes on the network	✓
5. Impact Assessment and Mitigation	
With and without development traffic volumes	✓
Construction traffic impact assessment and mitigation (if applicable)	N/A
Road safety impact assessment and mitigation	✓
Access and frontage impact assessment and mitigation	✓
Intersection delay impact assessment and mitigation	✓
Road link capacity assessment and mitigation	N/A
Pavement impact assessment and mitigation	N/A
Transport infrastructure impact assessment and mitigation	✓
Other impacts assessment relevant to the specific development type / location (if applicable)	N/A
6. Conclusions and Recommendations	
Summary of impacts and mitigation measures proposed	✓
Certification statement and authorisation	✓

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

**Dated: 19 April 2024** 



### 6 Lawrie Street, Gracemere

## STORMWATER MANAGEMENT PLAN (SMP) (Quantity and Quality)

CLIENT: Ray Group PTY LTD

SITE ADDRESS: 6 Lawrie Street, Gracemere

MCE No: 23118

DATE: January 2024

## **ROCKHAMPTON REGIONAL COUNCIL**

### **APPROVED PLANS**



These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

Dated: 19 April 2024

DOCUMENT CONTROL

**DOCUMENT TITLE:** 

**Stormwater Management Plan (SMP)** 

MELIORA JOB No:

23118

CLIENT:

Ray Group PTY LTD

**AUTHOR:** 

SM

**AUTHORISED:** 

MB (BEng, CPEng, NER, RPEQ, MIEAust, MIPWEAQ)

SPERO MELIORA ENTERPRISES P/L T/A Meliora Engineering ABN 46153772813

21 McLeod Street Herston Queensland 4006 Australia

T: 0429970345 E: info@meliorace.com

Rev No	Date	Issue Details	Ву	Certified By RPEQ
01	21.12.23	Issued for Information	SN	No. 21258

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### **1 EXECUTIVE SUMMARY**

Meliora Engineering has been engaged by Ray Group PTY LTD to prepare a Stormwater Management Plan (SMP) suitable for submission to Rockhampton Regional Council in support of Operational Works for a site located at 6 Lawrie Street, Gracemere. The Application proposes a MCU proposes a café (Zarraffa's drive-through coffee).

The purpose of this Stormwater Management Plan (SMP) is to provide commentary and relevant calculations required to service the proposed development stormwater drainage management (quality and quality) as documented within Schematic Civil Drawings shown within Appendix B.

The assessment has been carried out in accordance with Rockhampton City Council Planning Scheme Policies and the proposed works described herein will be subject to any associated DA & OPW Approval Conditions to be provided by Council.

Meliora Engineering civil schematic sketches addressing stormwater management arrangement and catchment areas are shown within Appendix B – Schematic Civil Drawings.

A summary of civil engineering advice is as follows:

- The site is not affected by sources of flooding (including river, creek nor overland flow). No further flood study or analysis is considered necessary.
- The development proposes to capture roof water & runoff from the site in under-ground
  pit/pipe network before discharging to John Street, which is proposed as the sites lawful
  point of discharge. Catchment C1 will be detained within under-ground pipes and as shallow
  ponding within the pavement surface totalling a minimum 20kL storage to achieve nonworsening of flows in the post-development case. Further details of the detention system
  are specified in the report below.
- The proposal, featuring a lot less than 2500m² does not trigger the SPP's Post-Development Stormwater Management (Water Quality) Design Objectives and therefore no permanent treatment solutions/devices are proposed.

Information discussed in this report is inferred from several sources including authority databases, DBYD records, site survey and design documents received from the client.

All relevant standards and guidelines are addressed in this report including criteria from:

- RCC Planning Scheme Policy
- Australian Rainfall and Runoff Guideline (ARR)
- Queensland Urban Drainage Manual (QUDM) 2013
- Plumbing and Drainage Code AS3500.3
- State Planning Policy (SPP)
- International Erosion Control Association of Australasia (IECA)

This report has demonstrated that the proposed development does not present any. civil related engineering issues which would prevent the development from proceeding as proposed.

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

These plans are approved subject to the current conditions of approval associated with

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### 2 SITE CHARACTERISTICS

### 2.1 LOCATION & TITLES/EASEMENTS

Refer to below figures and tables for locality plan and specific title information for the property to be developed.





Figure 1 - Site Location (as accessed from Google Maps 8/01/2024)

Table 1 - Property Details

Lot Information	Lot 604 on RP2642
Street Address	6 Lawrie Street, Gracemere
Site Area	977m²
Existing Easements	No

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

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### 3 PROPOSED CIVIL ENGINEERING WORKS

Meliora Engineering accepts no responsibility for the accuracy of information supplied to them by second and third parties, including survey, authority mapping data and geotechnical testing information which may have been relied on to inform the civil engineering opinions and calculations presented within the advice below.

Consider that the assessment addresses the requirements for development of the subject site at the time the study was undertaken. If these conditions are known to change, the results of this assessment should be reviewed and amended as required.

The assessment has been carried out in accordance with the relevant Council Planning Scheme Policies and the proposed works described herein will be subject to the conditions attached to the Development Approval to be provided by Council and any nominated referral agencies.

### 3.1 DESCRIPTION OF WORKS

The Application proposes a MCU proposes a café (Zarraffa's drive-through coffee).

Please refer to Appendix A – Architectural Drawings for architectural layout plans.

### 3.2 SITE-BASED STORMWATER DRAINAGE MANAGEMENT - QUANTITY

Refer to Appendix F – Code Response Table for the Rockhampton Regional Council Stormwater Management Code & responses.

### 3.2.1 ON-SITE DRAINAGE & RUNOFF QUANTITY TREATMENT OBJECTIVE

the stormwater management objectives that apply to the site have been derived from QUDM, State Planning Policy (2017), BCC Planning Scheme Policy and BCC Land Development Guidelines. The key stormwater parameters and desired outcomes are:

- Minimisation of storm-related nuisance to the public.
- Minimisation of legal disputes between neighbouring landowners and communities.
- Flood control & resilience to flooding in excess of nominated design events.
- Pedestrian and vehicular safety
- Integrate stormwater management infrastructure carefully in the urban and natural landscape, promoting retention of natural drainage system and protection/restoration of environmental values.

Subsequently, the objectives of Stormwater Runoff Quantity Management for the subject site are;

- 1. Provide a stormwater conveyance system for minor (10% AEP) and major (2% AEP) storm events to discharge to the nominated Lawful Point of Discharge
- 2. Limit flooding of public and private property, both within the catchment and downstream, to acceptable levels.
- 3. To provide convenience and safety for pedestrians and traffic in frequent stormwater flows by controlling those flows within prescribed velocity/depth limits.

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### 3.2.2 EXISTING DRAINAGE REGIME

A site survey documenting existing services within and surrounding the development site was performed by CMi and is shown within Appendix C – Survey plan. The survey highlights the following existing features related to drainage:

- In-ground drainage infrastructure, notably an existing gully pit at northern corner of the property which discharges into John St corridor
- Sheet flow discharges towards the north direction
- The site grades towards the north direction at an approximate slope of 3.20%

The site is in a local high point in the surrounding land, and there are no upstream contributing catchments discharge into the site, assisted by runoff being diverted away from the site by John Street Road corridor infrastructure.

#### 3.2.2.1 EXISTING LAWFUL POINT OF DISCHARGE

The site discharges to the existing gully pit at the site's northern corner, which is the existing Lawful Point of Discharge.

Further information on existing Council Stormwater Infrastructure in the area of the site was received via a BYDA search and a Council Mapping search.

### 3.2.3 PROPOSED DRAINAGE REGIME

#### 3.2.3.1 PROPOSED LAWFUL POINT OF DISCHARGE

In the case of the proposed development, and as per further commentary in the below section, the site DOES alter the site's stormwater discharge characteristics and there is a risk of nuisance flow during the post-development case. Detention storage will be provided to ensure non-worsening, though ultimately the new on-site network will continue to discharge to the existing pit in the northern corner which is proposed as the sites lawful point of discharge in the post-development case as well.

### 3.2.3.2 TAILWATER LEVELS

The tailwater level circumstance considered within the drainage analysis assumes water levels 300mm below surface in the existing pit.

### 3.2.3.3 PROPOSED DRAINAGE NETWORK

Stormwater generated from the development will be conveyed through a pit and pipe network for minor stormwater events (10% AEP) and a combination of pits and pipes and overland flow for major storm events (1% AEP).

All stormwater drainage will be designed in accordance with the requirements of QUDM 2016.

Generally, the application proposes internal private pit and pipe infrastructure to capture all site runoff and discharge flows to the existing stormwater gully at northern corner of the site.

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### 3.2.4 <u>CATCHMENT HYDROLOGY</u>

### 3.2.4.1 FLOW ESTIMATION METHODS & MODELLING

The choice of hydrologic method must be appropriate to the type of catchment and the required degree of accuracy.

As per Council's Infrastructure PSP flow estimations using Rational method is recognised. For this small-scale development Rational method was deemed suitable for use to estimate peak flows for catchments under existing and developed conditions. The Rational Method Calculations are summarised below.

However, a DRAINS model has also been developed in order to accurately model the detention arrangement. Results can be seen in Section 3.2.5 below.

### 3.2.4.2 RAINFALL DATA

Catchment hydrology has been estimated using rainfall specific for the site at 6 Lawrie Street, Gracemere. This is derived from the Bureau of Meteorology (BOM) Design Rainfall Data System (2016) using the following Latitude, Longitude:

Latitude -23.436223, Longitude 150.456415

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### 3.2.4.3 EXISTING CATCHMENTS DESCRIPTION

The existing catchment within the site discharging to the LPOD at northern corner.

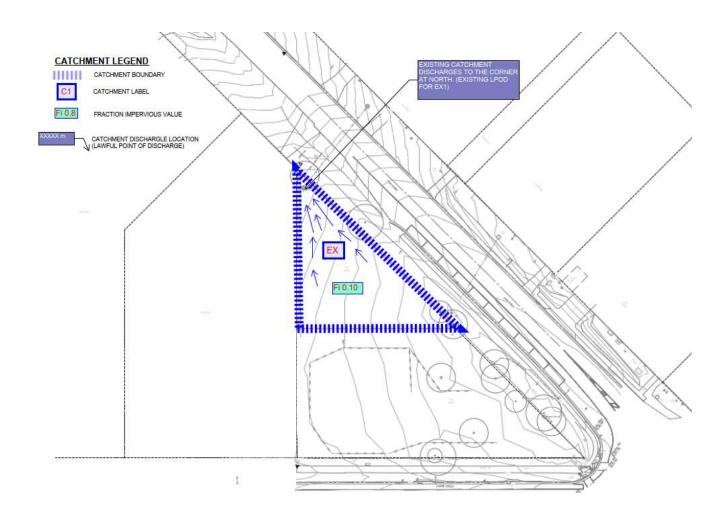


Figure 2 – Existing Catchments

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### 3.2.4.4 PROPOSED CATCHMENTS DESCRIPTION

Post—development, the run-off from proposed C2 discharges to the existing pit in northern corner before discharge to John Street. C1 discharges to pit/pipe infrastructure and allows for shallow ponding in pavement before discharge to John Street.

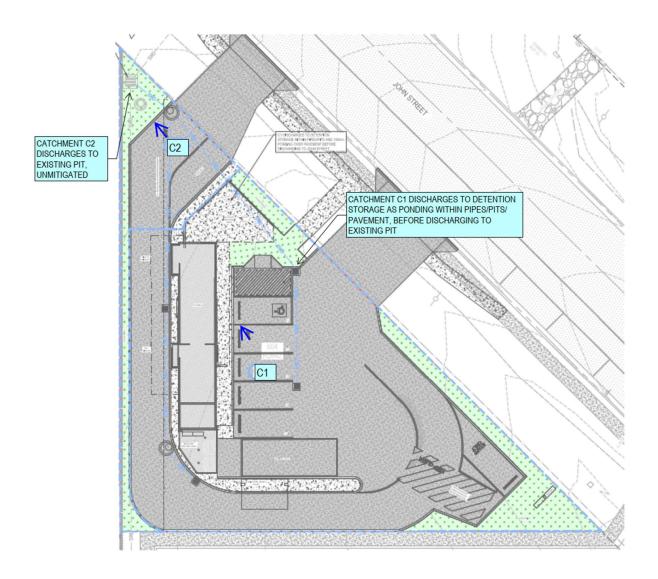


Figure 3 - Proposed Catchments

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#### 3.2.4.5 CATCHMENT HYDROLOGY - RATIONAL METHOD CALCULATIONS

### EX1 – The existing catchment within the site discharging to the LPOD at northern corner

CATCHMENT NAME	EX1			Design	Storm Event (AE	P & ARI)		
RATIONAL METHOD	(units)	63% (Q1)	38% (Q2)	18% (Q5)	10% (Q10)	5% (Q20)	2% (Q50)	1% (Q100)
Catchment Area	ha				0.098			
Time of Concentration	min				8.0			
Fraction Impervious					0.10			
Runoff Coefficient (Cy)		0.45	0.48	0.53	0.56	0.59	0.64	0.67
Rainfall Intensity (Iy)	mm/hr	86.87	112.57	145.25	165.54	192.72	229.89	259.30
Peak Flow	L/s	10.6	14.5	21.0	25.2	30.8	40.2	47.3

### Post-development, the roof water of proposed and C1 discharges to detention storage before discharge to John Street

CATCHMENT NAME	C1	Design Storm Event (AEP & ARI)						
RATIONAL METHOD	(units)	63% (Q1)	38% (Q2)	18% (Q5)	10% (Q10)	5% (Q20)	2% (Q50)	1% (Q100)
Catchment Area	ha				0.084			
Time of Concentration	min				5.0			
Fraction Impervious					0.85			
Runoff Coefficient (Cy)		0.68	0.72	0.80	0.85	0.89	0.97	1.00
Rainfall Intensity (Iy)	mm/hr	103.52	134.14	173.03	197.14	229.62	273.86	308.92
Peak Flow	L/s	16.4	22.6	32.5	39.0	47.7	62.3	72.3

### Post-development, the runoff from proposed C2 discharges to the existing pit in northern corner before discharge to John Street

CATCHMENT NAME	C2	Design Storm Event (AEP & ARI)						
DADAMETERS	(units)	63% (Q1)	38% (Q2)	18% (Q5)	10% (Q10)	5% (Q20)	2% (Q50)	1% (Q100)
Catchment Area	ha				0.013			
Time of Concentration	min				5.0			
Fraction Impervious					0.85			
Runoff Coefficient (Cy)		0.68	0.72	0.80	0.85	0.89	0.97	1.00
Rainfall Intensity (Iy)	mm/hr	103.52	134.14	173.03	197.14	229.62	273.86	308.92
Peak Flow	L/s	2.6	3.6	5.2	6.2	7.6	9.9	11.5

### 3.2.4.6 PRE vs POST DEVELOPMENT (UNMITIGATED) – RESULTS SUMMARY

The existing catchment contributes circa 47L/s (at 1% AEP event) to the existing gully pit at north corner (the LPOD).

Post—development, catchment C1 will contribute circa 72L/s (at 1% AEP event) and catchment C2 will contribute circa 12L/s (at 1% AEP event) to the nominated LPOD to achieve non-worsening.

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Total Site Cat				
AEP	Predeveloped Flow	Developed (Unmitigated) Flow	Difference	% Increase in Flow
	(m3/s)	(m3/s)	(m3/s)	
63% (Q1)	0.011	0.019	0.008	80
38% (Q2)	0.015	0.026	0.012	80
18% (Q5)	0.021	0.038	0.017	80
10% (Q10)	0.025	0.045	0.020	80
5% (Q20)	0.031	0.055	0.025	80
2% (Q50)	0.040	0.072	0.032	80
1% (Q100)	0.047	0.084	0.037	77

The above results indicate that the proposed development results in an increase in the quantity of runoff to the lawful point of discharge.

The development proposes to capture roof water & runoff from the site in under-ground pit/pipe network before discharging to John Street, which is proposed as the sites lawful point of discharge. Catchment C1 will be detained within under-ground pipes and as shallow ponding within the pavement surface totalling a minimum 20kL storage to achieve non-worsening of flows in the postdevelopment case. Further details of the detention system are specified in the report below.

#### 3.2.5 'DRAINS' MODEL RESULTS

### 3.2.5.1 DRAINS MODEL HYDROLOGICAL MODEL PARAMETERS

In order to develop a model of the site drainage in order to inform detention calculations, DRAINS software was used with an ILSAX hydrological model with the following default parameters:

- Impervious area depression storage of 1mm
- Supplementary area depression storage of 1mm
- Pervious area depression storage of 5mm

Rainfall data was sourced via BOM website for the AR&R 2019 Rainfall Ensembles, for the site locality and subsequently input into the software.

For the subject design case (and the associated site size) the following storm durations were modelled, with the 'critical storm' durations information maximum catchment flows and associated detention storage volumes:

- 5 to 45 minutes (increasing by five minute increments) storm bursts
- 1 hour storm burst
- 2 hour storm burst

For each AEP, the 'critical' storm duration informed maximum catchment flows and associated detention storage volumes.

### 3.2.5.2 DRAINS MODEL EXISTING CASE

As per figure below, the DRAINS model for the existing condition featured a catchment node discharging to the outlet (the north western boundary and ultimately John St).

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For the major event storm (1% AEP) the results (m³/s) are shown below in figure.

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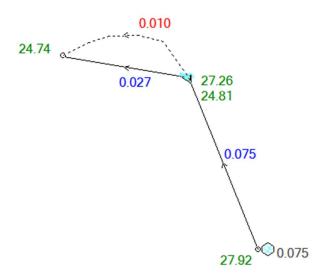


### 3.2.5.3 DRAINS MODEL DEVELOPED CASE - MITIGATED

As per figure below, the DRAINS model for the developed condition featured a network of catchment nodes, pipes and a storage basin node (as shallow ponding on the pavement surface). The sub-catchments for the roof areas, carpark areas and landscaped areas were combined into a single catchment for the purposes of detention modelling with the fraction impervious representing the breakup of surface types. The post-developed mitigated DRAINS model is shown below in figure.



The results from the DRAINS model confirm that the mitigated developed case achieves a flow rate of 37L/s during a 1% AEP storm event, which achieves non-worsening.



An 'unmitigated' DRAINs model was also developed, with storage nodes removed. The arrangement is not shown diagrammatically, however the results are shown in the section below.

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### 3.2.5.4 DRAINS MODEL DEVELOPED CASE PRE VS POST RESULTS & COMPARISON

Refer to table below for pre vs post flow results (unmitigated) and comparison.

Total Site Catchment - <b>Unmitigated</b> Discharge Summary (for Critical Storm)					
Q Event	Predeveloped Flow	Developed (Unmitigated) Flow	Difference	Increase in Flow	
	L/s	L/s	L/s	%	
63% (Q1) (1EY)	16	27	11.0	69	
38% (Q2)	21	34	13.0	62	
18% (Q5)	27	41	14.0	52	
10% (Q10)	35	49	14.0	40	
5% (Q20)	43	56	13.0	30	
2% (Q50)	52	67	15.0	29	
1% (Q100)	59	75	16.0	27	

Refer to table below for pre vs post flow results (mitigated) and comparison.

Total Site Catchment - Mitigated Discharge Summary (for Critical Storm)					
Q Event	Predeveloped Flow	Developed mitigated) Flow	Difference	Increase in Flow	
	L/s	L/s	L/s	%	
63% (Q1) (1EY)	16	18	2.0	13	
38% (Q2)	21	22	1.0	5	
18% (Q5)	27	24	-3.0	-11	
10% (Q10)	35	27	-8.0	-23	
5% (Q20)	43	27	-16.0	-37	
2% (Q50)	52	27	-25.0	-48	
1% (Q100)	59	37	-22.0	-37	

### 3.2.5.5 DRAINS MODEL - SINGLE UNDEGROUND TANK

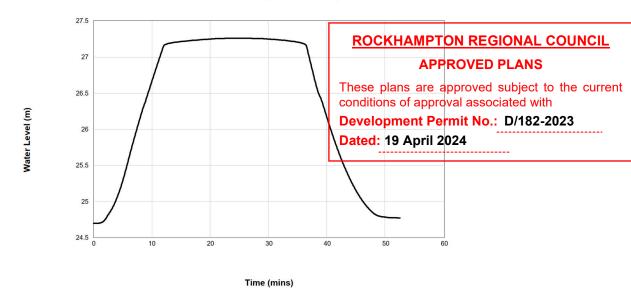
The required detention storage is proposed to be held within a shallow depth (150mm max) within the pavement surface of the drive-through and car park, to be controlled by an orifice plate in the outlet pit to ensure peak flows from the site are mitigated.

As can be seen above, the post developed flows are effectively mitigated for the 18%- 1% AEP events. The 63% and 38% AEP events does not achieve non-worsening, but the quantum of increase is no more than 2L/s for these frequent events, hence will have a negligible impact on downstream infrastructure.

At the storage node (pavement shallow depth), the water level depths are shown below.

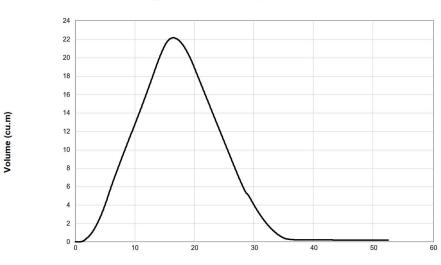


### PAVEMENT Water Level - 1% AEP, 25 min burst, Storm 4



At the storage node (pavement ponding), the storage volumes are shown below.

PAVEMENT Storage Volume - 1% AEP, 15 min burst, Storm 6



Time (mins)

The underground tank requires sharp-edged orifice plates in a staged arrangement to achieve the performance as shown in the above results. Refer to table below for tank volume, height and outlet arrangement specifications.

Detention Tank Summary			
Surface Area (m2) 300			
Internal Height (m)	100mm deep in pavement below weir,		
then 50mm deep over weir			
Volume (m3)	20		
Low Flow Outlet (Orifice 1)	120mm dia @ outlet pit (IL 24.70)		
Emergency Weir	High point in pavements @ 27.25m		

### 3.2.6 CONSTRUCTION PHASE DRAINAGE INFRASTRUCTURE

During the construction phase of the development, the stormwater management design



objectives for temporary drainage and basin spillways are to reference the Queensland Government State Planning Policy (SPP) 2017 Appendix 2 Table A (Part 1, 2 & 3).

Refer to Section 3.5 for further details on Construction Phase Erosion & Sediment Control details.

### 3.2.7 CONSTRUCTION PHASE DRAINAGE INFRASTRUCTURE

During the construction phase of the development, the stormwater management design objectives for temporary drainage and basin spillways are to reference the Queensland Government State Planning Policy (SPP) 2017 Appendix 2 Table A (Part 1, 2 & 3).

Refer to Section 3.5 for further details on Construction Phase Erosion & Sediment Control details.

### 3.3 SITE BASED STORMWATER DRAINAGE MANAGEMENT - QUALITY

Refer to Appendix F – Code Response Table for the Rockhampton Regional Council Stormwater Management Code & responses.

### 3.3.1 WATER QUALITY TREATMENT OBJECTIVE

Urban stormwater run-off potentially contributes to adverse water quality in waterways, which impact aquatic ecosystems health and limit human water uses. Unless well managed, urban stormwater can release contaminants such as nutrients, sediment and solid waste to waterways. For the post-construction phase, the SPP's stormwater management design objectives require minimum reductions in the mean annual load for key pollutants.

The SPP contains specific assessment benchmarks for the Water quality state interest. The Performance Outcomes (PO) of the SPP apply to the following applications:

- (1) a material changes of use for an urban purpose that involves premises 2500m<sup>2</sup> or greater in size and;
  - (a) will result in six or more dwellings; or
  - (b) will result in an impervious area greater than 25% of the net developable area; or
- (2) reconfiguring a lot for an urban purpose that involves premises 2500m<sup>2</sup> or greater in size and will result in six or more lots; or

The proposal, featuring a lot less than 2500m<sup>2</sup> does not trigger the SPP's Post-Development Stormwater Management (Water Quality) Design Objectives and therefore no permanent treatment solutions/devices are proposed.

3.3.2 CONSTRUCTION PHASE STORMWATER QUALITY

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During the construction phase of the development, the stormwater management design objectives for temporary water quality & ESC devices, including sediment basins, are to reference the Queensland Government State Planning Policy (SPP) 2017 Appendix 2 Table A (Part 1, 2 & 3).

### 3.4 STORMWATER DRAINAGE INFRASTRUCTURE MAINTENANCE

The landowner is responsible for the ongoing operation and maintenance of all privately-owned stormwater management assets & devices to ensure the drainage facility continues to meet its design performance and are maintained for the life of the approved development and may be liable for damages as a result of drainage system malfunction caused by lack of proper maintenance.



Roof-water drainage systems and detention arrangements/infrastructure are classified as private drains with the responsibility for maintenance lying with the property owners.

### 3.5 SEDIMENT & EROSION CONTROL

Healthy Waterways have identified that the large and increasing amount of sediment entering our waterways is one of the major issues affecting waterway health across south-east Queensland. Sediment is a contaminant that can seriously degrade water quality and starve marine life of oxygen, leading to fish kills and damage to aquatic ecosystems.

During the construction phase of the development, the stormwater management design objectives for temporary water quality & ESC devices, including sediment basins, are to reference the Queensland Government State Planning Policy (SPP) 2017 Appendix 2 Table A (Part 1, 2 & 3).

IECA 2008 Best Practice Erosion and Sediment Control (as amended) is to be referenced for details on the application of the Construction Phase requirements.

For the construction phase, the SPP's stormwater management design objectives require that developments apply best practice erosion and sediment control. These objectives are derived from International Erosion Control Association of Australasia (IECA) 2008 Best Practice Erosion and Sediment Control.

All sediment and erosion controls will be designed in the detailed design phase to meet the relevant design objectives and Council policies, and will be RPEQ'd.

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### **4 SUMMARY & CONCLUSIONS**

### 4.1 WORKS SUMMARY AND ENGINEERING RECOMMENDATION

Meliora Engineering has been engaged by Ray Group PTY LTD to prepare a Stormwater Management Plan (SMP) suitable for submission to Rockhampton Regional Council in support of Operational Works for a site located at 6 Lawrie Street, Gracemere. The Application proposes a MCU proposes a café (Zarraffa's drive-through coffee).

The purpose of this Stormwater Management Plan (SMP) is to provide commentary and relevant calculations required to service the proposed development stormwater drainage management (quality and quality) as documented within Schematic Civil Drawings shown within Appendix B.

The assessment has been carried out in accordance with Rockhampton City Council Planning Scheme Policies and the proposed works described herein will be subject to any associated DA & OPW Approval Conditions to be provided by Council.

Meliora Engineering civil schematic sketches addressing stormwater management arrangement and catchment areas are shown within Appendix B – Schematic Civil Drawings.

A summary of civil engineering advice is as follows:

- The site is not affected by sources of flooding (including river, creek nor overland flow). No further flood study or analysis is considered necessary.
- The development proposes to capture roof water & runoff from the site in under-ground
  pit/pipe network before discharging to John Street, which is proposed as the sites lawful
  point of discharge. Catchment C1 will be detained within under-ground pipes and as shallow
  ponding within the pavement surface totalling a minimum 20kL storage to achieve nonworsening of flows in the post-development case. Further details of the detention system
  are specified in the report below.
- The proposal, featuring a lot less than 2500m<sup>2</sup> does not trigger the SPP's Post-Development Stormwater Management (Water Quality) Design Objectives and therefore no permanent treatment solutions/devices are proposed.

Information discussed in this report is inferred from several sources including authority databases, DBYD records, site survey and design documents received from the client.

The assessment has been carried out in accordance with the relevant Council Planning Scheme Policies and the proposed works described herein will be subject to the conditions attached to the Development Application and Pre-Operational Works approval to be provided by Council and any nominated referral agencies.

This report has demonstrated that the proposed development does not present any stormwater management related engineering issues which would prevent the development from proceeding as proposed.

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

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### 4.2 LIMITATIONS

Meliora Engineering accept no responsibility for the accuracy of information supplied to them by second and third parties, including survey, authority mapping data and geotechnical testing information which may have been relied on to inform the civil engineering opinions and calculations presented within this report.

We consider that the study addresses the requirements for development of the subject site at the time the study was undertaken. If these conditions are known to change, the results of this study should be reviewed.

This Civil Engineering Report has been prepared under the direct supervision of a Registered Professional Engineer of Queensland generally in accordance relevant guidelines and standards.

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

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### 5 APPENDIX

### 5.1 APPENDIX A – ARCHITECTURAL DRAWINGS

## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

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## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

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## PROPOSED ZARRAFFA'S DRIVE-THROUGH 6 LAWRIE ST, GRACEMERE, QLD

### DA CIVIL ENGINEERING PACKAGE FOR FOR RAY GROUP PTY LTD



### LOCALITY PLAN

EXTRACTED FROM GOOGLE MAPS © 2023 NOT TO SCALE

LC	OT DATA
604	RP 2642

MELIORA ENGINEERING ACCEPTS NO RESPONSIBILITY FOR THE ACCURACY OF EXISTING UNDERGROUND SERVICES WHICH ARE PLOTTED FROM AUTHORITY RECORDS BY THE SURVEYOR, DOCUMENTED DESIGNS MAY BE SUBJECT TO WHICH ARE PLOT TEE PROMIND THE REVIEWS BY THE SOURCE FOR, DOCUMENTED DESIGNS MAY BE SOBJECT ON GOODING CHANGES UNTIL RECEIPT AND REVIEW OF MINIMUM QUALITY LEVEL A: EXISTING SERVICE LOCATION RESULTS ALONG FULL LENGTH OF PROPOSED MAIN ALIGNMENTS. MELIORA WILL NOT BE HELD LIABLE FOR COST INCREASES OR TIME EXTENSION RESULTING FROM NECESSARY DESIGN CHANGES TO ACHIEVE AUTHORITY CODE COMPLIANCE.

DRAWING SCHEDULE			
DRAWING No.	DRAWING TITLE		
SK00	COVER, LOCALITY, SCHEDULE & GENERAL NOTES		
SK05	PRELIMINARY STORMWATER DRAINAGE LAYOUT PLAN		
SK07	PRELIMINARY CIVIL DRAINAGE CATCHMENT PLAN		

### MANDATORY REFERENCE DOCUMENTATION

ALL WORKS TO BE CARRIED OUT IN ACCORDANCE WITH THE CURRENT COUNCIL (LOCAL AUTHORITY) DEVELOPMENT (DA) CONDITIONS), AS WELL AS THE WATER AUTHORITY CONDITIONS, ALL RELEVANT AUTHORITY APPROVALS AND CONDITIONS ARE TO BE REVIEWED (AND REQUESTED IF NOT ALREADY RECEIVED) BY CONTRACTOR PRIOR TO CONSTRUCTION.

READ THESE DRAWINGS IN CONJUNCTION WITH ARCHITECTURAL AND OTHER ENGINEERING DRAWING SPECIFICATIONS AND WITH ALL OTHER WRITTEN INSTRUCTIONS ISSUED. REFER TO ARCHITECTURAL DRAWINGS FOR SETTING OUT AND DETAIL DIMENSIONS. IN CASE OF DISCREPANCY, PRECEDENCE IS GIVEN TO DRAWINGS, THEN NOTES, THEN SPECIFICATION. REFER DISCREPANCIES TO SUPERINTENDENT BEFORE PROCEEDING WITH WORK.

- FURTHER, ALL WORKS TO BE CARRIED OUT IN ACCORDANCE WITH

  1. COUNCIL (LOCAL AUTHORITY) GUIDELINES, PLANNING SCHEME POLICIES (PSPs), SPECIFICATIONS AND STANDARD DRAWINGS
- RELEVANT LEGISLATION INCLUDING (BUT NOT LIMITED TO):
- RELEVANT LEGISLATION INCLUDING (BUT NOT LIMITED TO):

  1. WORK HEALTH & SAFETY ACT 2011

  2. ENVIRONMENTAL PROTECTION & BIODIVERSITY ACT 1999

  3.3 BIOSECURITY ACT 2015, REFER TO WWW.DAF.QLD.GOV.AU

  2.4 SUSTAINABLE PLANNING ACT 1999

  RELEVANT AUSTRALIAN STANDARDS INCLUDING (BUT NOT LIMITED TO):
- AS3500.3-2018 (PLUMBING & DRAINAGE)
- AS2865-2009 (CONFINED SPACES)

- 2. AS2865-2009 (CONFINED SPACES)
  3. AS378-2007 (EARTHWORKS)
  4. ASINZS 2890 1-2004 (PARKING FACILITIES)
  5. AS1742-3-2019 (SIGNAGE & LINE MARKING) SS BY MUTCD
  6. AS4049.2-2005 (PAVEMENT MARKING MATERIALS)
  INTERNATIONAL EROSION CONTROL AUTHORITY (IECA) & STANDARD DRAWINGS
  AUSTROADS DESIGN MANUALS & STANDARD DRAWINGS
  AUSTROADS DESIGN MANUALS & STANDARD DRAWINGS
- MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES (MUTCD) SOUTH EAST QUEENSLAND WATER SUPPLY AND SEWERAGE DESIGN AND
- CONSTRUCTION CODE (OR THE SEQ CODE)

PRELIMINARY! ALL CIVIL WORKS AS SHOWN ON MELIORA DA PLANS IS PRELIMINARY AND IS SUBJECT TO FURTHER

#### **CONTOURS LEGEND**

EXISTING SURFACE CONTOURS

PROPOSED LOT BOUNDARIES PROPOSED EASEMENT

EARTHWORKS EXISTING BATTER TOE EARTHWORKS EXISTING BATTER TOP BUILDING EXISTING BUILDING EXISTING ROOF/EAVE

MISC FENCE / GATE EXISTING ROAD EXISTING KERB

COMMUNICATIONS EXISTING DRAINAGE EXISTING CENTERLINE

ELECTRICAL EXISTING OVERHEAD FLECTRICAL EXISTING UNDERGROUND

ELECTRICAL EXISTING CENTERLINE DBYD GAS EXISTING

GAS EXISTING CENTERLINE DBYD SEWER EXISTING CENTERLINE SEWER EXISTING RISING MAIN

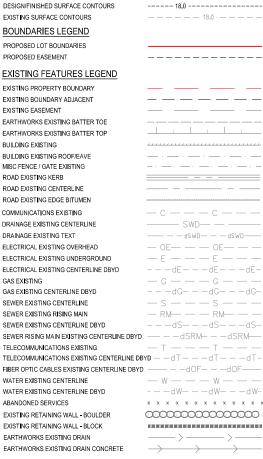
SEWER EXISTING CENTERLINE DBYD

WATER EXISTING CENTERLINE

ABANDONED SERVICES EXISTING RETAINING WALL - BOULDER

EARTHWORKS EXISTING DRAIN

EXISTING VEGETATION





These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

Dated: 19 April 2024

YOU DIG Zero Damage - Zero Harm

01 ISSUE FOR APPROVAL

ALL PLANS TO BE READ IN CONJUNCTION WITH ALL INFORMATION AND NOTES ON DRG. No. C01 AND ALL RELEVANT SPECIFICATIONS

18.12.23 SD MB

DRAWN: DECEMBER 2023

RAY GROUP PTY LTD

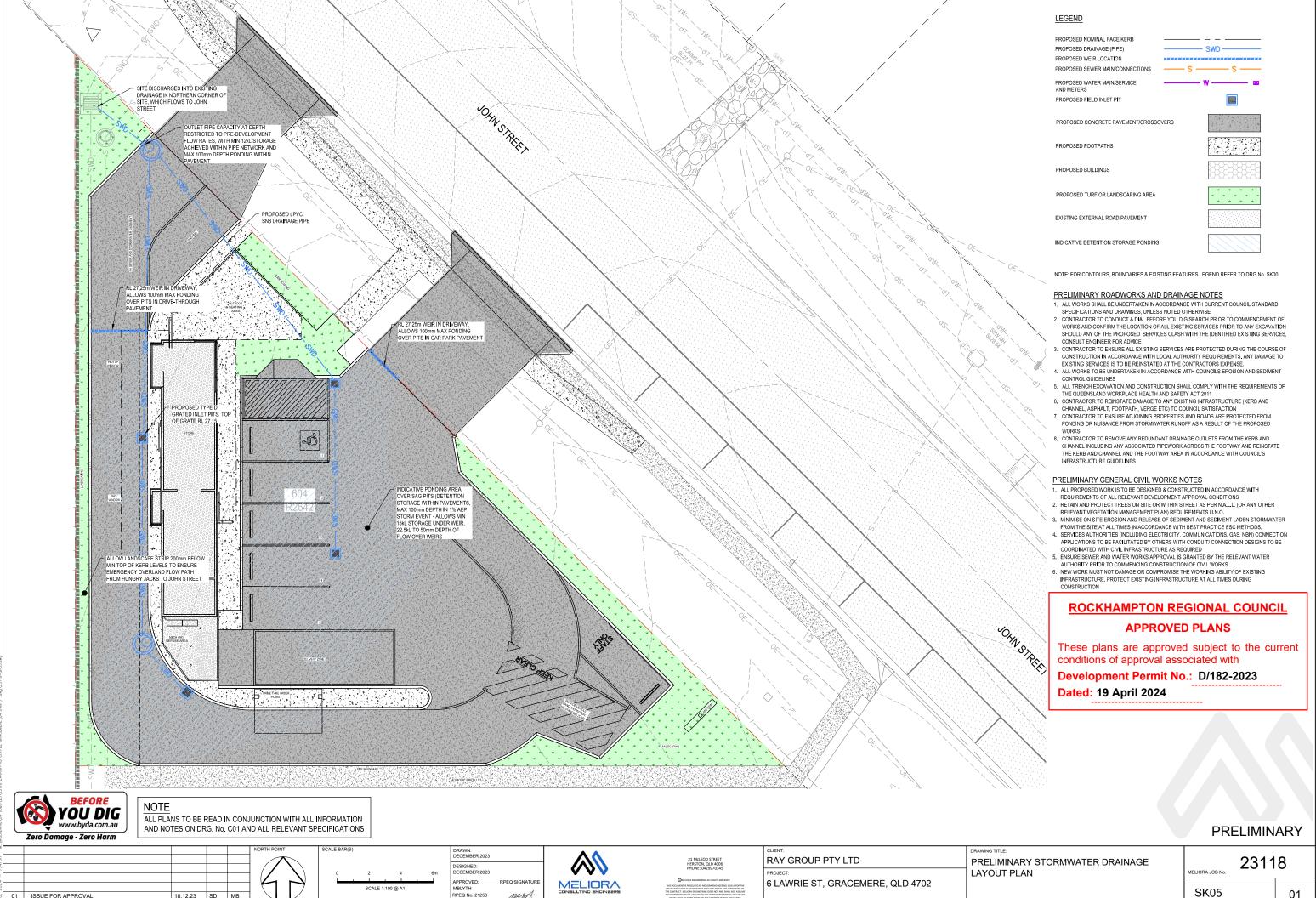
LOCALITY, SCHEDULE & GENERAL NOTES

23118

**PRELIMINARY** 

SK00 01

EXISTING FEATURES LEGEND 6 LAWRIE ST, GRACEMERE, QLD 4702 MELIORA



01 ISSUE FOR APPROVAL

18.12.23 SD MB

01



**LEGEND** 



POST DEVELOPMENT CATCHMENT BOUNDARY PROPOSED CATCHMENT FLOW DIRECTION

CATCHMENT LABEL

NOTE: FOR CONTOURS, BOUNDARIES & EXISTING FEATURES LEGEND REFER TO DRG No. SK00

### **ROCKHAMPTON REGIONAL COUNCIL**

### **APPROVED PLANS**

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

**Dated: 19 April 2024** 

**PRELIMINARY** 

01 ISSUE FOR APPROVAL 18.12.23 SD MB

MELIORA CONSULTING ENGINEERS

6 LAWRIE ST, GRACEMERE, QLD 4702

PRELIMINARY CIVIL DRAINAGE CATCHMENT PLAN

23118

SK07

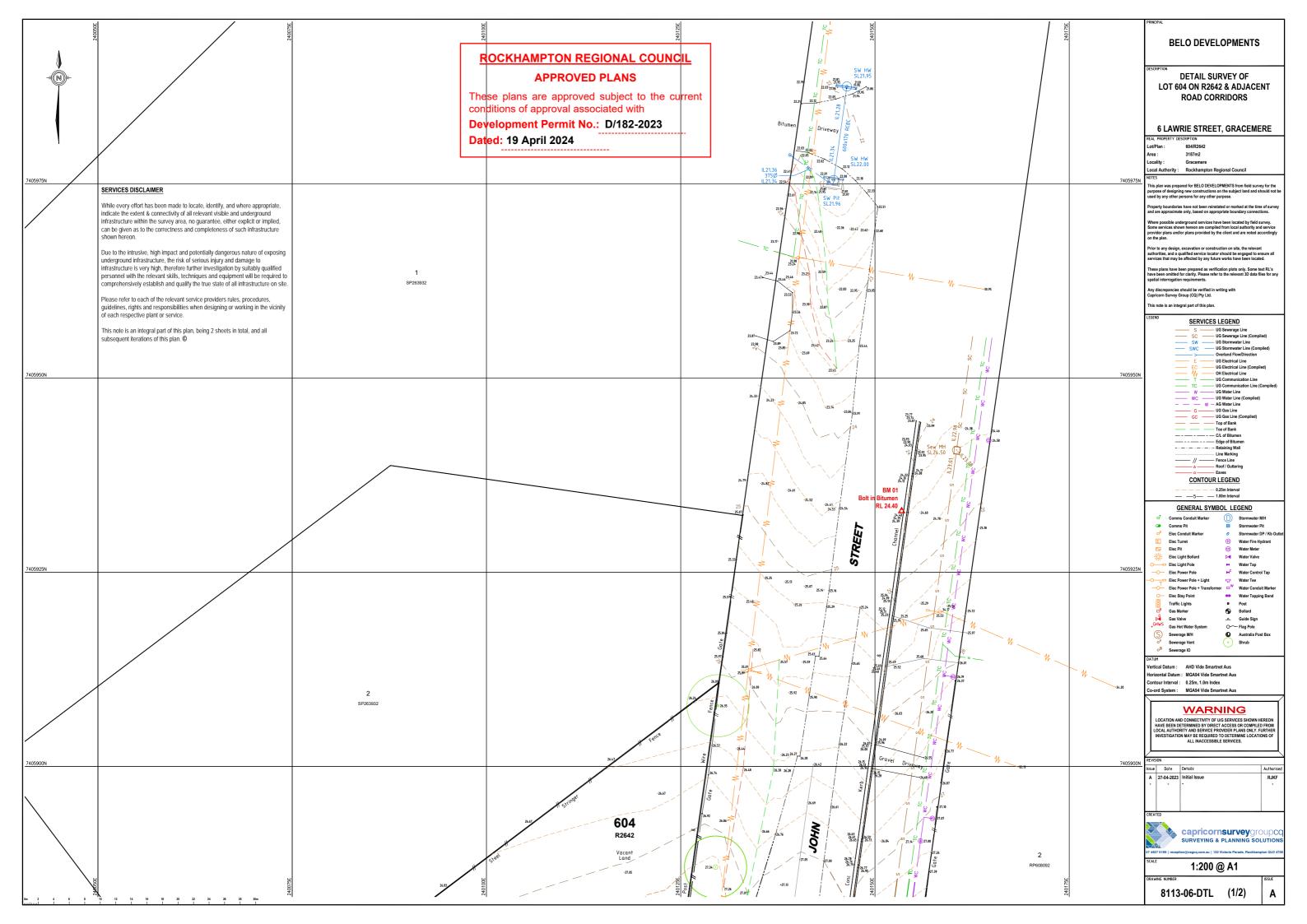
01 REVISION

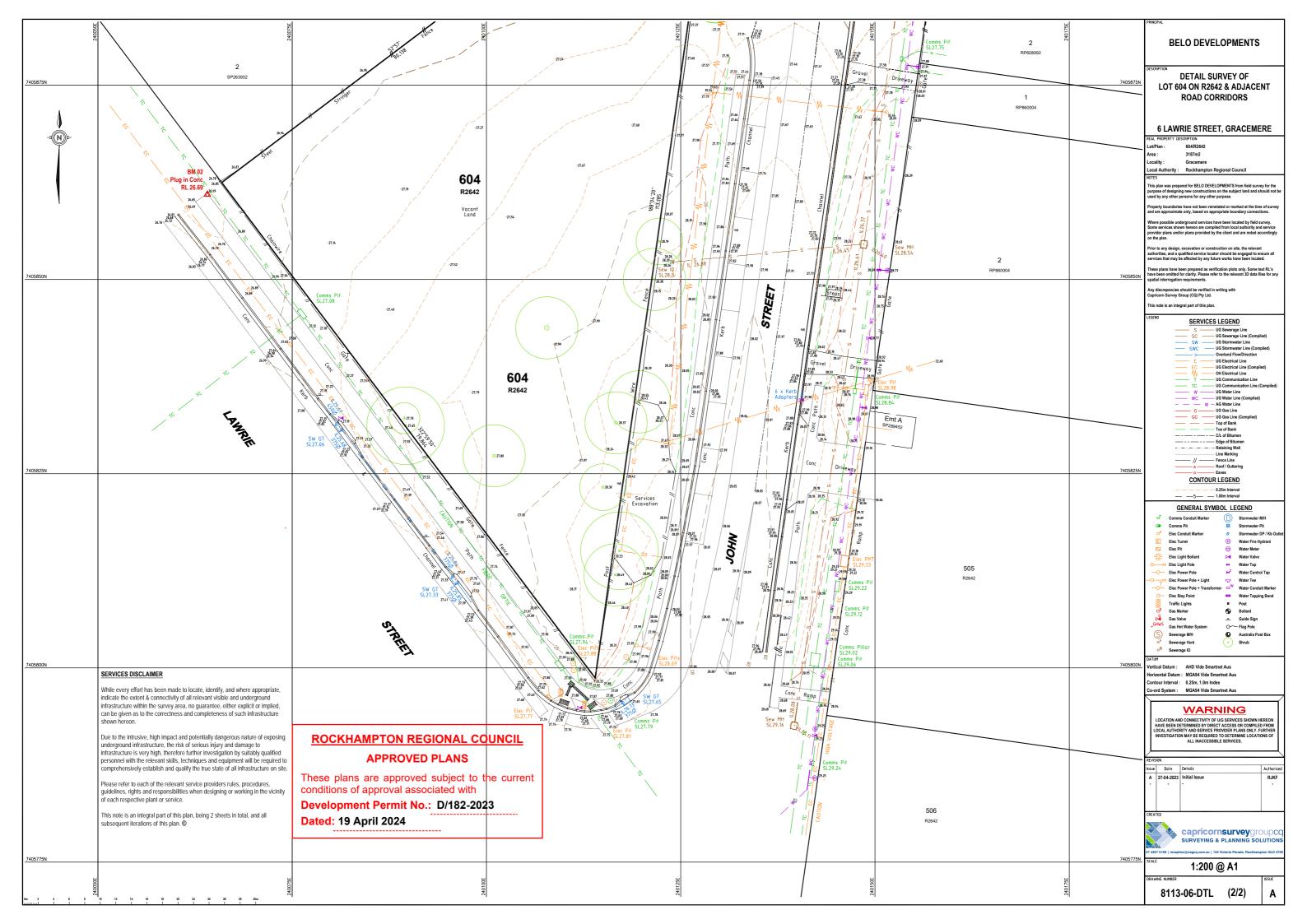


## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 





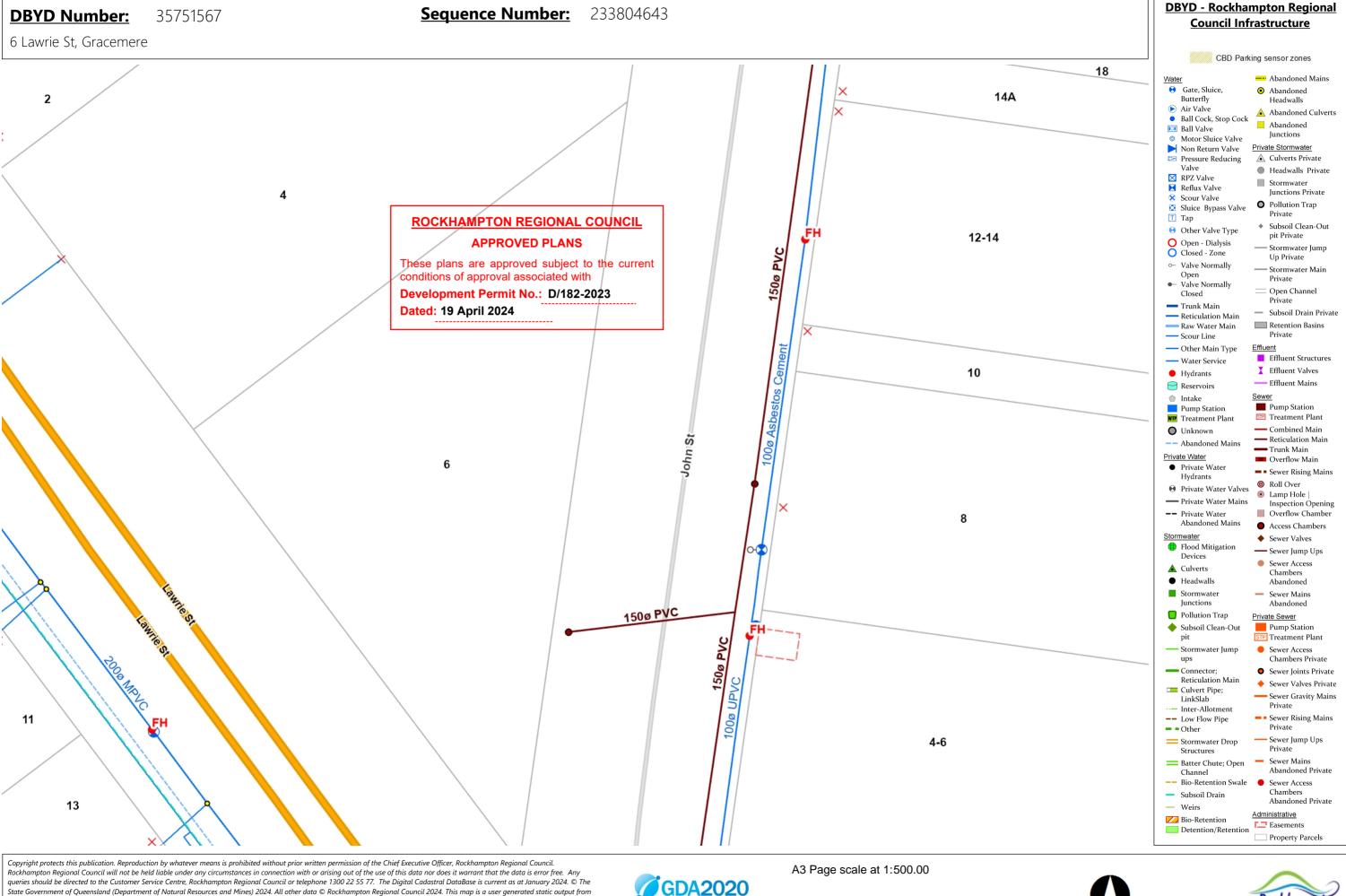


## ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

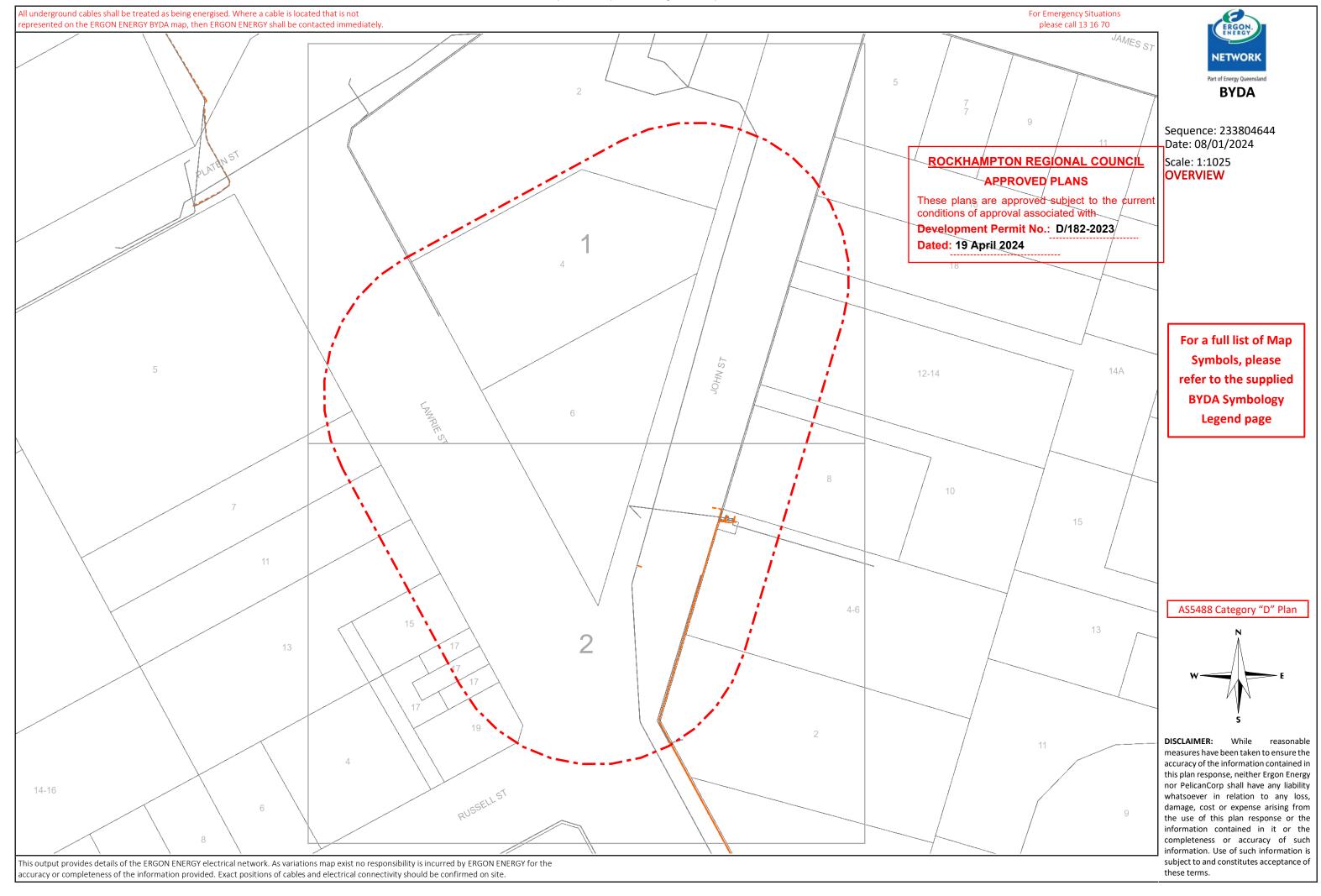
Dated: 19 April 2024

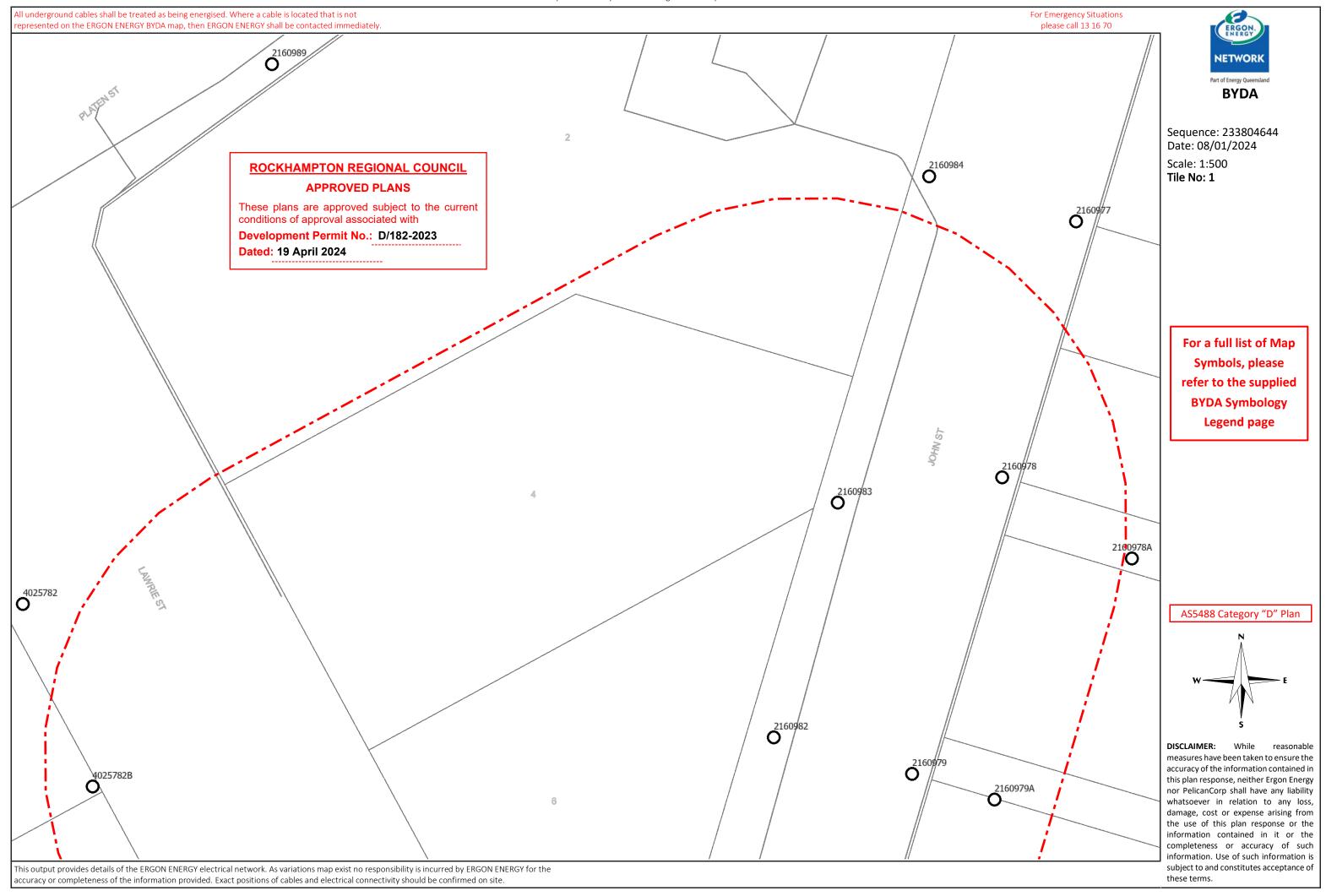


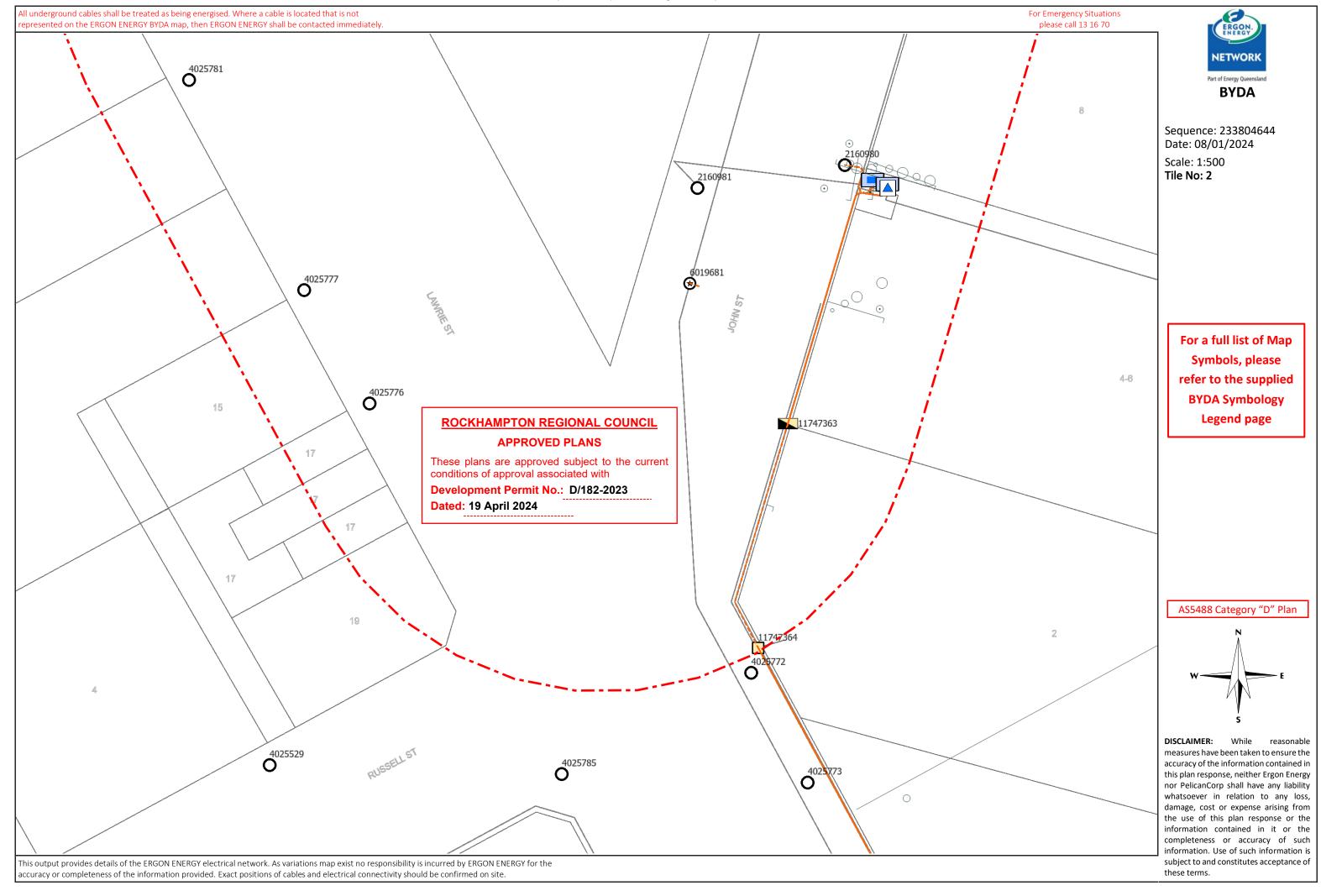


an Internet mapping site and is for reference only. Data layers that appear on this map may or may not be accurate, current, or otherwise reliable









# ROCKHAMPTON REGIONAL COUNCIL

### **APPROVED PLANS**

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

Dated: 19 April 2024

To: Kousik De
Phone: Not Supplied
Fax: Not Supplied

**Email:** admin@meliorace.com

Dial before you dig Job #:	35751567	DIAL BEFORE
Sequence #	233804645	YOU DIG
Issue Date:	07/01/2024	www.1100.com.au
Location:	6 Lawrie St , Gracemere , QLD , 4702	

# Indicative Plans 1

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

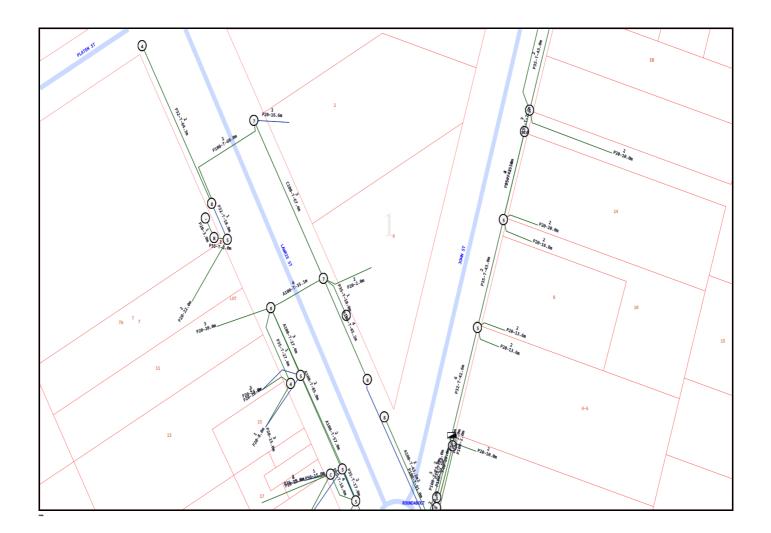
Dated: 19 April 2024

<del>-</del>	LEGEND nbn (i)	
34	Parcel and the location	
3	Pit with size "5"	
<b>(2E)</b>	Power Pit with size "2E".  Valid PIT Size: e.g. 2E, 5E, 6E, 8E, 9E, E, null.	
	Manhole	
$\otimes$	Pillar	
PO - T- 25.0m P40 - 20.0m	Cable count of trench is 2.  One "Other size" PVC conduit (PO) owned by Telstra (-T-), between pits of sizes, "5" and "9" are 25.0m apart.  One 40mm PVC conduit (P40) owned by NBN, between pits of sizes, "5" and "9" are 20.0m apart.	
-0 1 0	2 Direct buried cables between pits of sizes ,"5" and "9" are 10.0m apart.	
<del>-</del> 9 <del>-</del> -9-	Trench containing any INSERVICE/CONSTRUCTED (Copper/RF/Fibre) cables.	
<del>-</del> 99-	Trench containing only DESIGNED/PLANNED (Copper/RF/Fibre/Power) cables.	
<del>-</del> 9 <del></del> 9-	Trench containing any INSERVICE/CONSTRUCTED (Power) cables.	
BROADWAY ST	Road and the street name "Broadway ST"	
Scale	0 20 40 60 Meters 1:2000 1 cm equals 20 m	

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

Dated: 19 April 2024



# **Emergency Contacts**

You must immediately report any damage to the **nbn**™ network that you are/become aware of. Notification may be by telephone - 1800 626 329.

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

**Dated:** 19 April 2024

To: Kousik De
Phone: Not Supplied
Fax: Not Supplied

**Email:** admin@meliorace.com

Dial before you dig Job #:	35751567	DIAL BEFORE
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Issue Date:	07/01/2024	www.1100.com.au
Location:	6 Lawrie St , Gracemere , QLD , 4702	

# Indicative Plans 1

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

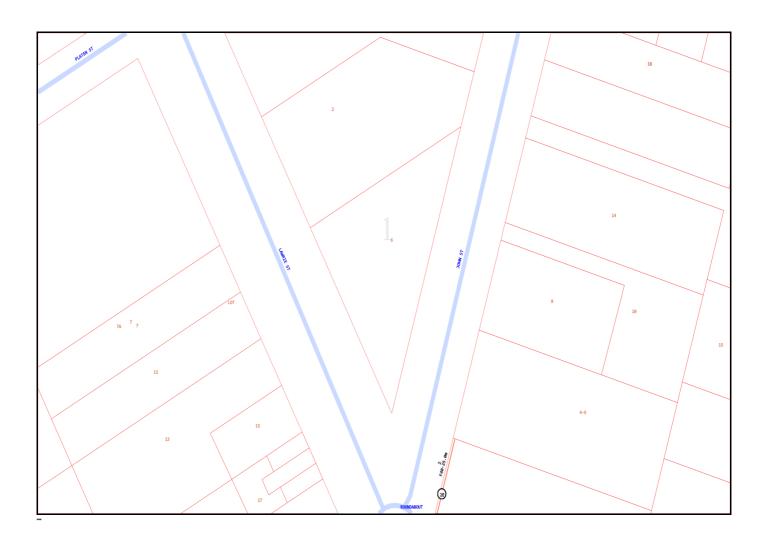
Dated: 19 April 2024

<del>-</del>	LEGEND nbn (i)	
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3	Pit with size "5"	
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PO - T- 25.0m P40 - 20.0m	Cable count of trench is 2.  One "Other size" PVC conduit (PO) owned by Telstra (-T-), between pits of sizes, "5" and "9" are 25.0m apart.  One 40mm PVC conduit (P40) owned by NBN, between pits of sizes, "5" and "9" are 20.0m apart.	
-0 1 0	2 Direct buried cables between pits of sizes ,"5" and "9" are 10.0m apart.	
<del>-</del> 9 <del>-</del> -9-	Trench containing any INSERVICE/CONSTRUCTED (Copper/RF/Fibre) cables.	
<del>-</del> 99-	Trench containing only DESIGNED/PLANNED (Copper/RF/Fibre/Power) cables.	
<del>-</del> 9 <del></del> 9-	Trench containing any INSERVICE/CONSTRUCTED (Power) cables.	
BROADWAY ST	Road and the street name "Broadway ST"	
Scale	0 20 40 60 Meters 1:2000 1 cm equals 20 m	

These plans are approved subject to the current conditions of approval associated with

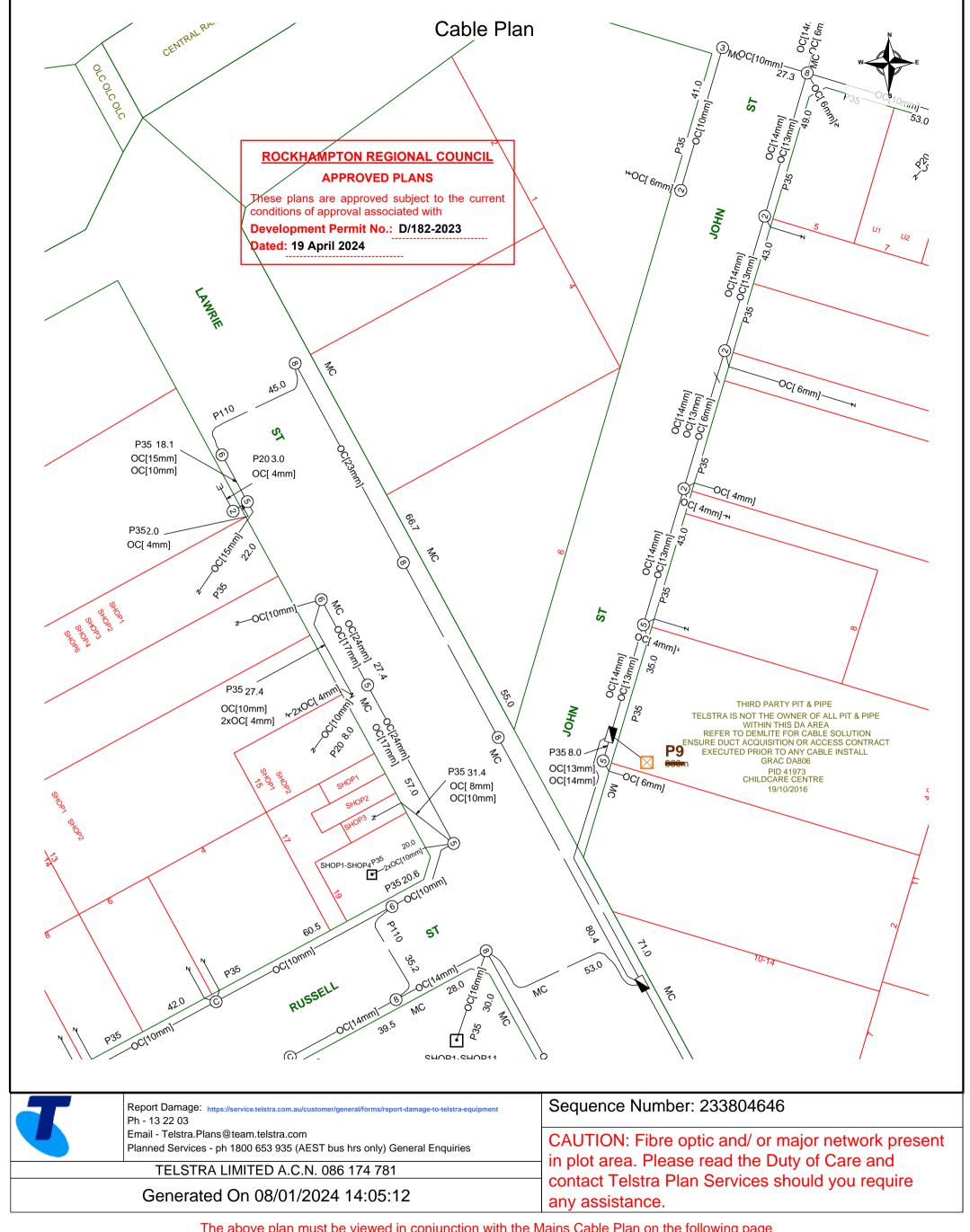
**Development Permit No.: D/182-2023** 

Dated: 19 April 2024



# **Emergency Contacts**

You must immediately report any damage to the **nbn**™ network that you are/become aware of. Notification may be by telephone - 1800 626 329.



### The above plan must be viewed in conjunction with the Mains Cable Plan on the following page

### **WARNING**

Telstra plans and location information conform to Quality Level "D" of the Australian Standard AS 5488-Classification of Subsurface Utility Information.

As such, Telstra supplied location information is indicative only. Spatial accuracy is not applicable to Quality Level D.

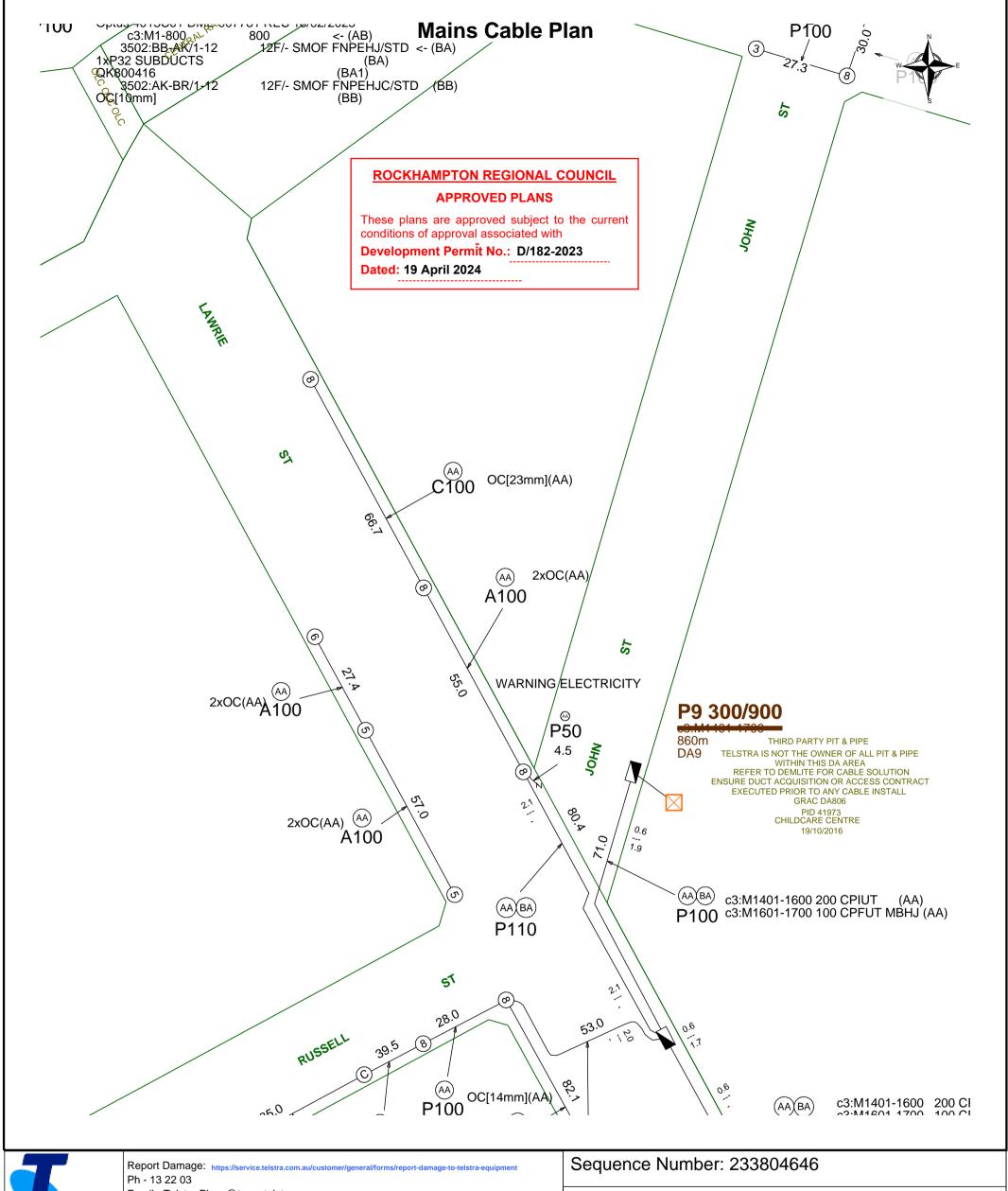
Refer to AS 5488 for further details. The exact position of Telstra assets can only be validated by physically exposing it.

Telstra does not warrant or hold out that its plans are accurate and accepts no responsibility for any inaccuracy.

Further on site investigation is required to validate the exact location of Telstra plant prior to commencing construction work.

A Certified Locating Organisation is an essential part of the process to validate the exact location of Telstra assets and to ensure the asset is protected during construction works.

See the Steps- Telstra Duty of Care that was provided in the email response.



Email - Telstra.Plans@team.telstra.com

Planned Services - ph 1800 653 935 (AEST bus hrs only) General Enquiries

TELSTRA LIMITED A.C.N. 086 174 781

Generated On 08/01/2024 14:05:13

CAUTION: Fibre optic and/ or major network present in plot area. Please read the Duty of Care and contact Telstra Plan Services should you require any assistance.

### **WARNING**

Telstra plans and location information conform to Quality Level "D" of the Australian Standard AS 5488-Classification of Subsurface Utility Information.

As such, Telstra supplied location information is indicative only. Spatial accuracy is not applicable to Quality Level D.

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See the Steps- Telstra Duty of Care that was provided in the email response.





E: <u>info@meliorace.com</u>
W: www.meliorace.com

**21 McLeod Street** 

Herston QLD 4006 Australia

# ZARRAFFA'S COFFEE GRACEMERE

6 LAWRIE STREET, GRACEMERE, QLD, 4702

# DEVELOPMENT APPLICATION

### DRAWING REGISTER

2023051-DA-A000 COVER SHEET

2023051-DA-A110 EXISTING SITE PLAN

2023051-DA-A111 EXISTING STREET VIEW ELEVATIONS

2023051-DA-A120 PROPOSED SITE PLAN

2023051-DA-A180 MRV SERVICE VEHICLE PATH PLAN

2023051-DA-A220 PROPOSED FLOOR PLAN

2023051-DA-A300 PROPOSED BUILDING ELEVATIONS SHEET 1 OF 2 2023051-DA-A301 PROPOSED BUILDING ELEVATIONS SHEET 2 OF 2

2023051-DA-L100 PROPOSED LANDSCAPE SITE PLAN

### **ROCKHAMPTON REGIONAL COUNCIL**

### **APPROVED PLANS**

These plans are approved subject to the current conditions of approval associated with

**Development Permit No.: D/182-2023** 

**Dated: 19 April 2024** 

### **REAL PROPERTY DESCRIPTION**

LOT 604 ON R2642 PARISH OF GRACEMERE COUNTY OF LIVINGSTONE LGA: ROCKHAMPTON REGIONAL COUNCIL SITE: 977.00 m<sup>2</sup>





### NOT FOR CONSTRUCTION

**DEVELOPMENT APPLICATION** 

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A 21/11/23 PRELIMINAR all dimensions and levels on site prior to commencement of construction

21/11/23 PRELIMINARY ISSUE 01/12/23 DEVELOPMENT APPROVAL

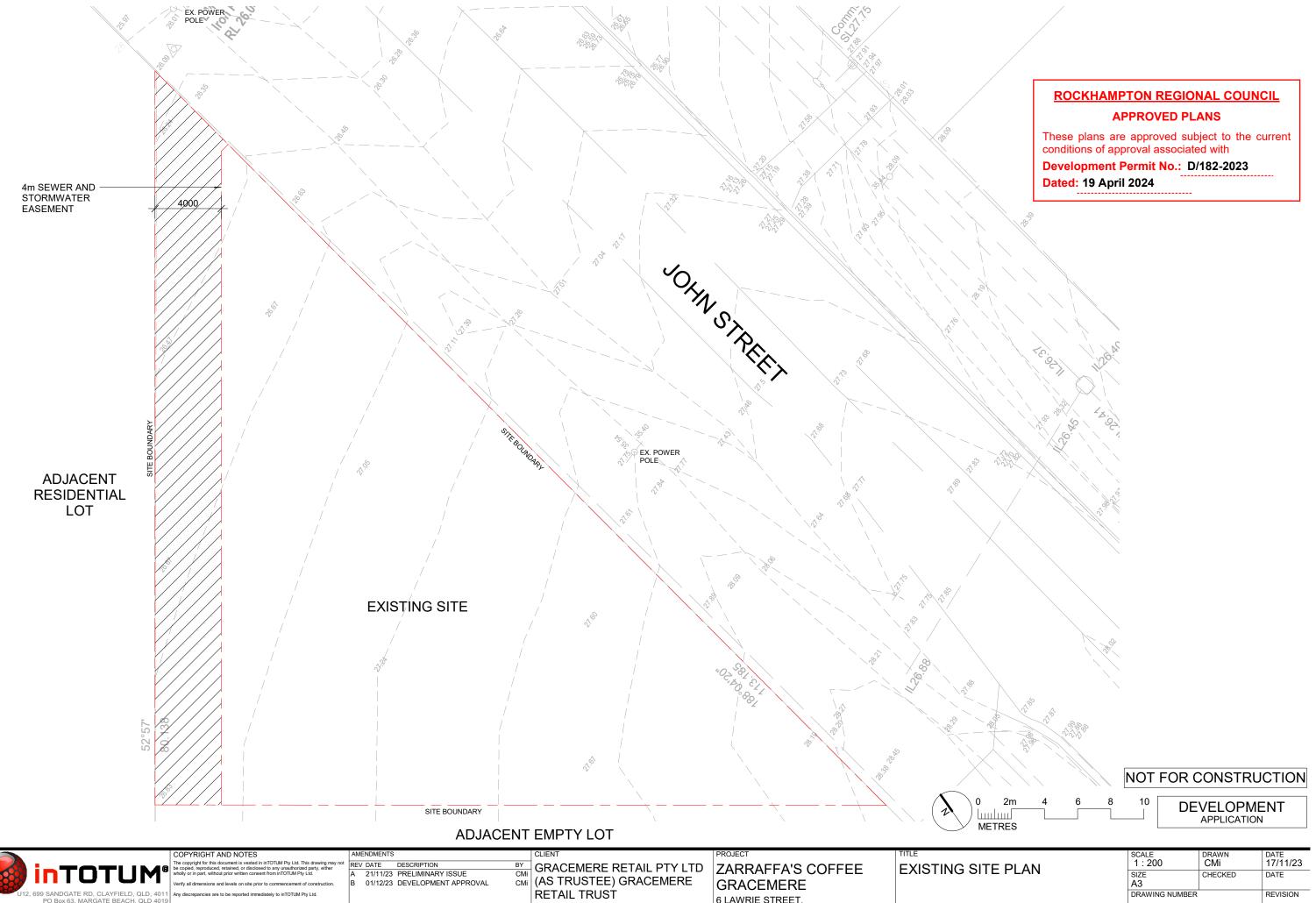
GRACEMERE RETAIL PTY LTD CMI (AS TRUSTEE) GRACEMERE **RETAIL TRUST** 

ZARRAFFA'S COFFEE GRACEMERE 6 LAWRIE STREET,

GRACEMERE, QLD, 4702

**COVER SHEET** 

NTS 17/11/23 SIZE A3 CHECKED DATE DRAWING NUMBER REVISION 2023051-DA-A000



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6 LAWRIE STREET, GRACEMERE, QLD, 4702

SIZE A3 DRAWING NUMBER REVISION 2023051-DA-A110



EXISTING SITE LOOKING NORTH ALONG JOHN STREET SCALE 1: NTS



EXISTING SITE FROM JOHN STREET SCALE 1: NTS



EXISTING SITE LOOKING SOUTH ALONG JOHN STREET SCALE 1: NTS

NOT FOR CONSTRUCTION

**ROCKHAMPTON REGIONAL COUNCIL APPROVED PLANS** These plans are approved subject to the current

conditions of approval associated with **Development Permit No.: D/182-2023** 

**Dated: 19 April 2024** 

DEVELOPMENT APPLICATION



REV DATE DESCRIPTION 21/11/23 PRELIMINARY ISSUE

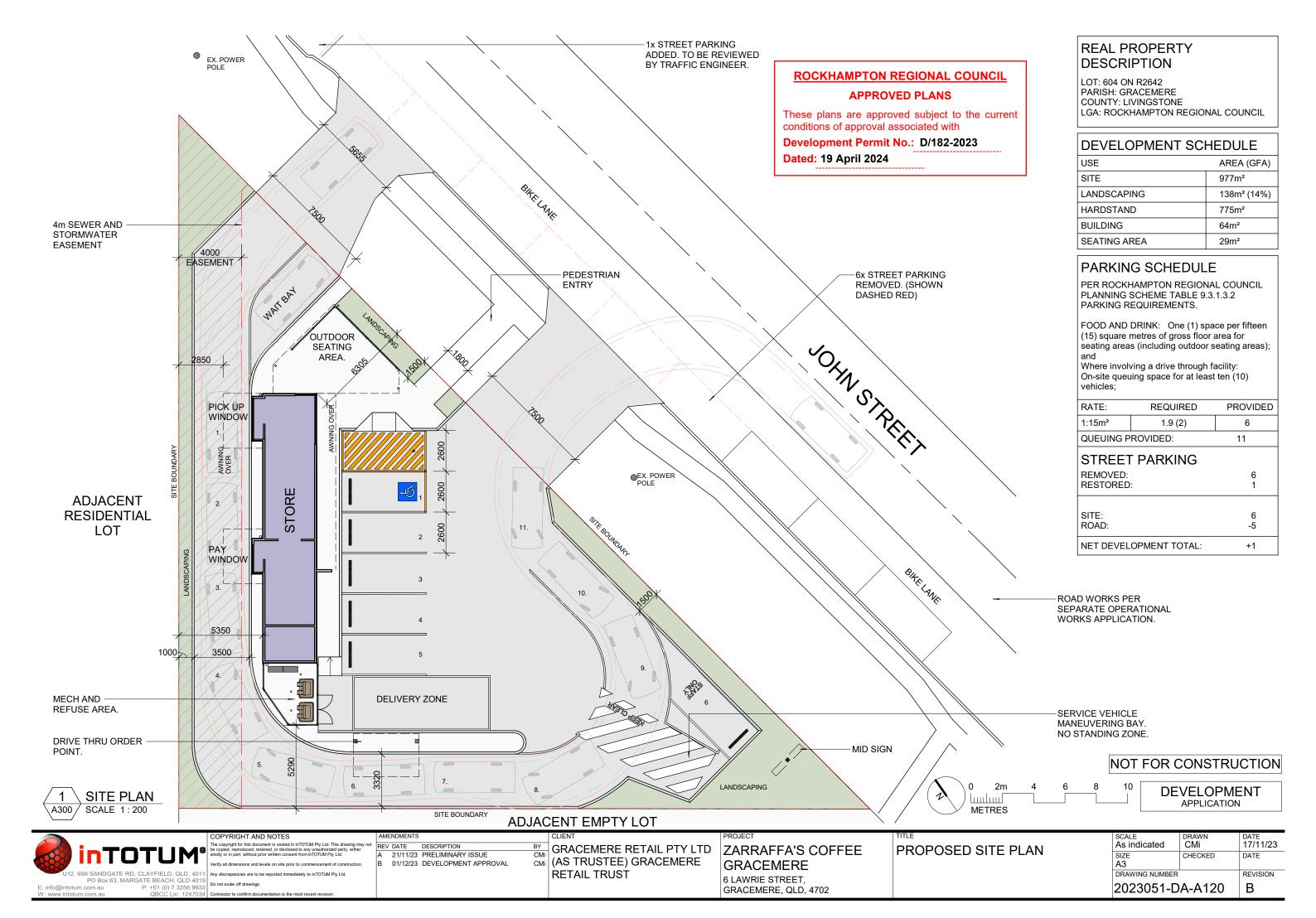
01/12/23 DEVELOPMENT APPROVAL

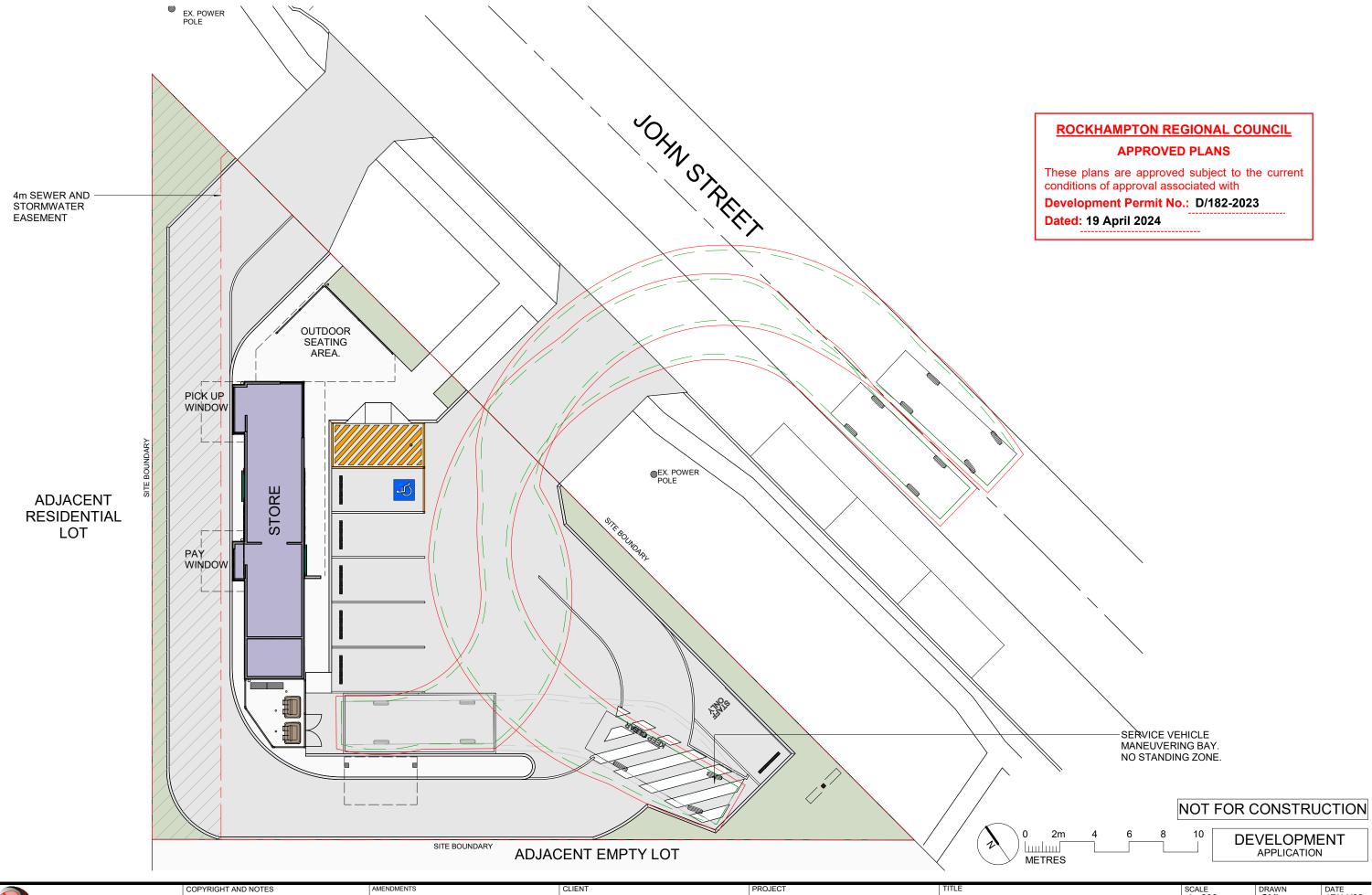
GRACEMERE RETAIL PTY LTD CMI (AS TRUSTEE) GRACEMERE RETAIL TRUST

ZARRAFFA'S COFFEE GRACEMERE 6 LAWRIE STREET, GRACEMERE, QLD, 4702

**EXISTING STREET VIEW ELEVATIONS** 

DRAWN CMi SCALE 1: NTS DATE 17/11/23 CHECKED DRAWING NUMBER REVISION 2023051-DA-A111







REV DATE DESCRIPTION 21/11/23 PRELIMINARY ISSUE 01/12/23 DEVELOPMENT APPROVAL

GRACEMERE RETAIL PTY LTD CMI (AS TRUSTEE) GRACEMERE RETAIL TRUST

ZARRAFFA'S COFFEE **GRACEMERE** 6 LAWRIE STREET, GRACEMERE, QLD, 4702

MRV SERVICE VEHICLE PATH PLAN

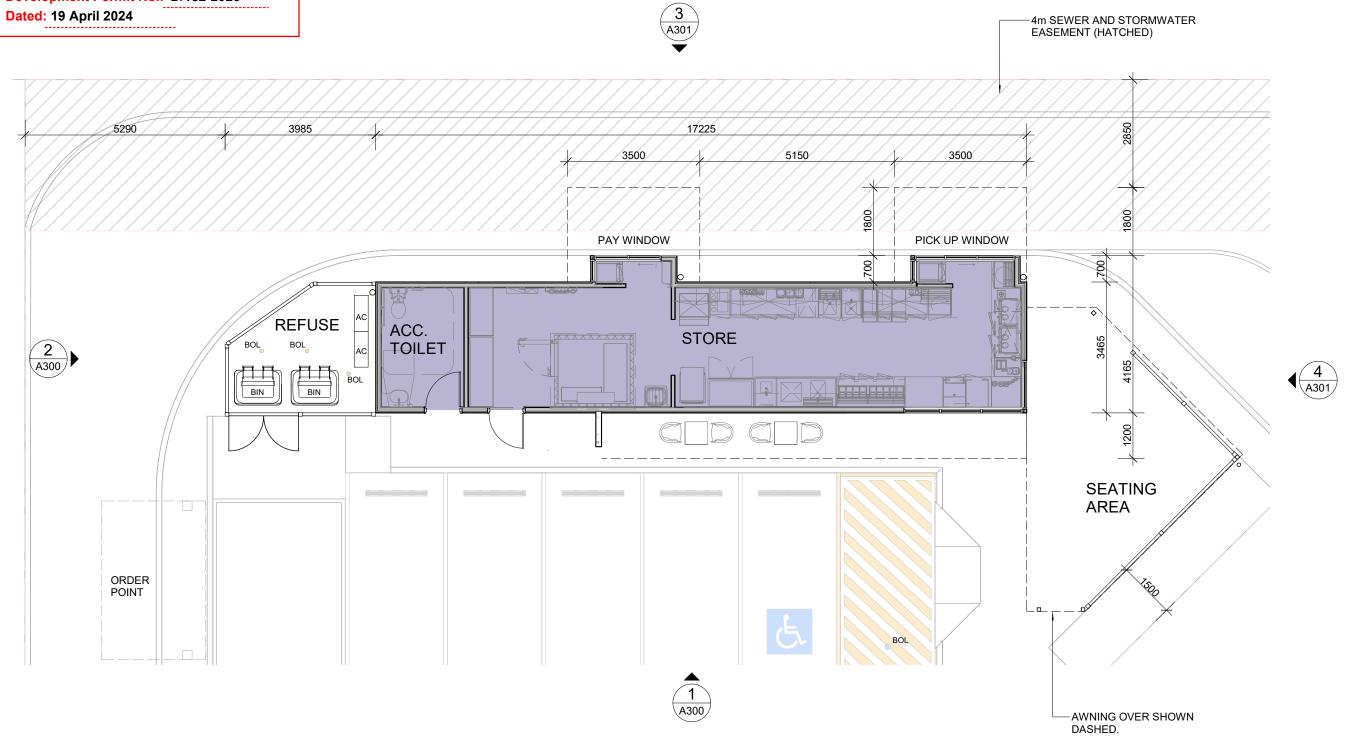
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## **ROCKHAMPTON REGIONAL COUNCIL**

### **APPROVED PLANS**

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**Development Permit No.: D/182-2023** 







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	Verify all dimensions and levels on site prior to commencement of construction.

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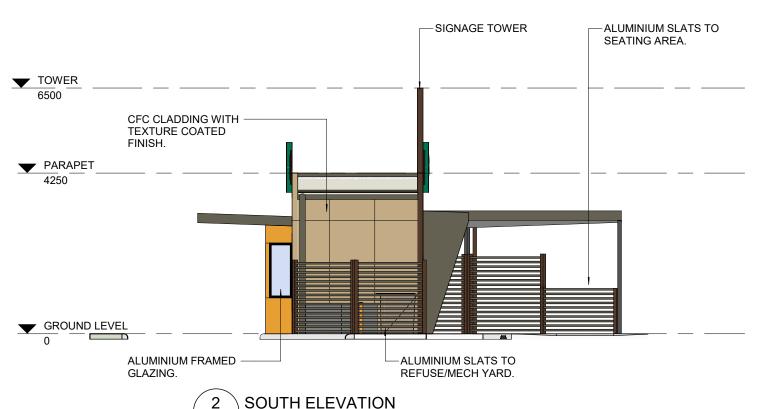
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PROJECT
ZARRAFFA'S COFFEE GRACEMERE
GRACEMERE
6 LAWRIE STREET, GRACEMERE, QLD, 4702
GRACEMERE, QLD, 4702

PROPOSED FLOOR PLAN	

SCALE 1:100	DRAWN CMi	DATE 17/11/23	
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SCALE 1:100

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21/11/23 PRELIMINARY ISSUE 01/12/23 DEVELOPMENT APPROVAL

GRACEMERE RETAIL PTY LTD CMI (AS TRUSTEE) GRACEMERE **RETAIL TRUST** 

ZARRAFFA'S COFFEE GRACEMERE 6 LAWRIE STREET,

GRACEMERE, QLD, 4702

PROPOSED BUILDING **ELEVATIONS SHEET 1 OF 2** 

SCALE 1:100	DRAWN CMi	DATE 17/11/23
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